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# Materials Testing Manual





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#### **DEFINITIONS**

Admixtures - Materials other than cement, aggregate and water in concrete used to entrain air, retard setting, or accelerate setting.

Anchorage - That portion of a reinforcing bar and any attachment thereto, designed to resist pulling out or slipping of the bar when subjected to stress.

Asphalt Cement (AC), Asphalt Binder, PGAB, etc – Asphalt Binder is considered to be practically pure bitumen which is in a semi-solid state at ordinary temperatures. Selection of the asphalt binder to be used in the HPM is based on environmental and traffic loadings.

**Base, Base Course (CB, CTB, PMB)** - Intermediate layer between subgrade and surfacing (concrete pavement or plant mix pavement) and contributes to the load bearing capacity of the surfacing section. This material is usually a granular material with the material above the No. 4 being at least partially crushed and may be stabilized using Portland cement, asphalt, emulsion, lime, etc. In the case of a gravel road, the base material will be the top layer and has similar material properties, although retain the natural cohesiveness to deter wash-boarding and rutting, which may mean higher PI.

**Batch (Concrete)** - The quantity of mix discharged from the mixer in one complete operation of the plant before additional materials are introduced.

**Bedrock/Pit Floor** - Unusable material, such as shale or native consolidate rock, that underlies the construction material and delineates the depth of rock deposit or vertical limit.

**Bleeding (HPM & Chip Seals)** - Characterized by the presence of an excessive amount of asphalt on the surface. Typically due to either an excessive amount of prime coat or tack coat or excessive asphalt in the mix.

**Bleeding (Concrete)** - The escape of water from freshly placed concrete commonly observed as an accumulation upon a horizontal surface.

**Blow-Up (Concrete)** - Localized buckling or shattering of rigid pavement caused by excessive longitudinal pressure.

**Borrow Special Excavation (BSE)** - This may be the same material as used in the sub-base, but is usually considered to be subgrade material that replaces inferior or problematic soil. This material may be of the same type as the sub-base, however a non-granular soil may be specified. This layer is not to be included as part of the surfacing section as determined during the pavement structural design; it is included as subgrade if the depth is 24 inches or greater.

**California Bearing Ratio (CBR)** - A test to determine the bearing capacity of a soil compared to a standard, well-graded, crushed stone.

Carry-over - Deposition of finer material into a bin that should contain larger size aggregate.

**Cement Treated Base (CTB)** - Crushed aggregate that incorporates pit run material meeting a specified gradation treated with cement and placed above the subgrade, sub-base, or fill as a foundation for the pavement or surface course. The strength capacity of the CTB is greater than CB, so a thinner surfacing section is the result.

**Cementation Value (CV)** - This test is used primarily for gravel roads with typically Crushed Base as the surfacing material. It is a test of the fines, minus No. 4 material, and is an indication of the cohesiveness of the material. The test consists of loading a 1 inch square compacted sample and recording the maximum strength achieved. A low strength is an indicator of a loss of cohesiveness that may result in wash-boarding and an extremely high strength is an indicator of excess clay and may result in rutting and slickness.

**Coarse Material** - Crushed rock retained on a No. 4 sieve. This material is crushed after all the undersize pit run material or fines are removed, so all of the rock is crushed.

**Consistency (Concrete)** - Designates the relative mobility of freshly mixed concrete commonly defined as slump.

Construction Joint - Vertical or notched plane of separation in pavement.

**Contraction Joint** - Joint of either full depth or weakened plane-type designed to establish position of any crack caused by contraction while providing no space for expansion of pavement beyond original length.

**Corrugations** - Regular transverse undulations in surface of pavement consisting of alternate valleys and crests.

Crack(s) - Vertical cleavage due to natural causes or traffic action.

**Crazing (Concrete)** - Pattern cracking. Extending only through surface layer: A result of more drying shrinkage in surface than interior of plastic concrete.

**Crushed Base (CB)** - Crushed aggregate that incorporates pit run material meeting a specified gradation placed above the subgrade, sub-base, or fill as a foundation for the pavement or surface course.

**Crusher Run Material** - The natural granular material run through a crusher to a specified maximum top size. Some of this material would not be subjected to any crushing so pit run fines are still present.

**Curing Period** - A period provided to prevent formation of surface cracks due to rapid loss of water while concrete is plastic and to assure attainment of specified strength.

**Cutback Asphalt** - Asphalt cement which has been rendered liquid by fluxing with a petroleum distillate. (Includes: RC's - rapid curing; MC's - medium curing; SC's - slow curing)

**"D" lines** - Disintegration characterized by successive formation of series of fine cracks at rather close intervals paralleling edges, joints, and cracks and usually curving across slab corners, initial cracks forming very close to slab edge and additional cracks progressively developing, ordinarily filled with calcareous deposit.

**Density** - The mass of a material per unit volume. Commonly called "unit weight". In other words, the "weight" of a unit volume of material. Usually expressed in terms of lbs/ft<sup>3</sup>. Refer to AASHTO M 132 for additional information.

**a. Apparent** - The weight in air of a unit volume of a material at a specified temperature and pressure. If the material is a solid, the volume will be that of the impermeable portion.

**b.** Bulk - The weight in air of a unit volume of a permeable material (including both permeable and impermeable voids normal to the material) at a specified temperature and pressure.

#### **Directional Bias** –

Gradation- "Directional bias" is considered to exist when all five tests are higher for one laboratory than for the other and the average difference on at least one sieve exceeds the Allowable Gradation Difference in Table 3 of WYDOT 126.0

Density- "Directional bias" is considered to exist when all, or all but one of the tests are higher for one laboratory than the other and the average difference exceeds  $0.5 \text{ lb/ft}^3$ .

**Disintegration** - Deterioration into small fragments from any cause.

**Distortion** - Any deviation of pavement surface from original shape.

**Emulsion** - Asphalt mixed with water with the aid of a small amount of emulsifying agent (usually a detergent). The object is to make a stable dispersion of the asphalt cement in water; stable enough for pumping, prolonged storage, and mixing. Further, the emulsion should "break" quickly after contact with aggregate in a mixer or after spraying on the roadbed. "Breaking" is the separation of the water from the asphalt.

**Expansion Joint** - Joint designed to allow for the pavement to expand in length.

Faulting - Differential vertical displacement of slabs adjacent to joint or crack.

Filler - Natural material passing a No. 4 sieve that may be either granular (sand) or dirt.

**Fine Material** - Crushed rock passing a No. 4 sieve. Generally, when specified as a Type I plant mix pavement aggregate, no pit run material is allowed unless a filler is specified and the fine material is crushed. In a Type III plant mix pavement aggregate, pit run material is allowed and the fines are usually a combination of crushed and pit run.

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**Fineness Modulus** - An index of the fineness or coarseness of an aggregate. It is the summation of the cumulative percentages of the material retained on the standard sieves divided by 100; the size opening in consecutive sieves being related by a constant ratio. Coarse aggregate sieves: 6 inch, 3 inch,  $1\frac{1}{2}$  inch,  $\frac{3}{4}$  inch,  $\frac{3}{8}$  inch, and No. 4. Fine aggregate sieves: No. 4, No. 8, No. 16, No. 30, No. 50, and No. 100.

**Flecking** - Dislodgement of thin mortar film from outermost portion of occasional particles of coarse aggregate on concrete surface, generally attributable to lack of bond between mortar and aggregate.

**Flexible Base and Pavements** - The term flexible indicates Hot Plant Mix Pavement (PMP, HPM, PMB, etc.), also referred to as asphalt pavement or asphalt base, which is granular material, at least partially crushed, with added Asphalt Cement and lime. Mix design testing is completed on material from a specified source to determine the properties required, including component rates, to provide the necessary structural strength. A flexible course is intended to provide adequate aggregate interlock to provide vertical strength and also "flexibility" to allow adequate elasticity to accommodate the seasonal effects.

Frost Heave - Differential upward displacement due to frost; seasonal displacement.

**Gradation** - A term used to describe the range and the relative distribution of particle sizes in a material.

Example: Well graded soils: Soils that having an even distribution of particle sizes but usually have a low percentage of fines (material passing the No. 4 sieve).

Poorly graded soils: Soils that have the majority of particles retained on a certain sieve and may be either fine or coarse.

**Grizzly** - Instead of the square or round openings used in a screen, a grizzly has parallel bars spaced at a fixed distance and set at angles of  $20^{\circ}$  to  $50^{\circ}$  of horizontal.

Hair Checking - Small irregular cracks extending to appreciable depth and occurring before concrete takes final set.

**Honeycomb** - A surface or interior defect in a concrete mass characterized by the lack of mortar between the coarse aggregate particles.

**Joint(s)** - Constructed junctions between adjacent sections of pavement or between pavement and structures.

**Laitance** - Extremely fine material of little or no hardness which may collect on the surface of freshly placed concrete resulting from the use of excess mixing water.

Leveling Course (Hot Plant Mix Leveling, Microsurfacing) - Course of variable thickness constructed immediately on top of base or existing pavement to remove large irregularities prior to overlying treatment or construction. This treatment restores the existing pavement surface and will have a variable thickness when placed.

**Liquid Limit** - That moisture content which is the boundary between the liquid and plastic states for the minus No. 40 fraction of a soil. For laboratory-purposes, it may be defined as the moisture content as which that soil fraction will close a standard groove for a length of  $\frac{1}{2}$  inch when subjected to 25 blows in a liquid limit device.

**Longitudinal Joint** - Joint of either full-depth or weakened-plane type constructed parallel to or along center line to control longitudinal cracking.

**Map Cracking** - Disintegration in which cracking of slab surface develops in random pattern; may develop over entire surface or localized areas; may or may not be associated with abnormal growth of concrete.

**Marshall Mix Design** - A test procedure that determines the optimum asphalt content for a specified PMP aggregate gradation that optimizes the properties required. The objective is to provide sufficient asphalt for a durable pavement, sufficient mix stability, sufficient voids to allow for a slight amount of additional compaction yet low enough to keep out air and moisture, and sufficient workability to permit efficient placement without segregation. On high traffic roads, try to minimize the asphalt content so the mix resists rutting, but keep enough to provide a durable surface that is still flexible and resists cracking. On lower traffic roads, try to allow enough asphalt to provide a flexible and durable pavement, yet not so high that rutting or shoving results. Compaction in this procedure utilizes a drop-hammer.

**Maximum Size** – The smallest sieve listed in the applicable specification through which 100 percent of the aggregate sample particles pass.

**Superpave Maximum Size** – One sieve larger than the nominal maximum size.

**Mechanical Analysis** - The mechanical analysis of a soil/aggregate is the determination of the percentage of individual grain sizes present in the sample. The results of the tests are of value when used for classification purposes. The analysis consists of two parts, the determination of the amount of coarse material using a nest of sieves or screens and the analysis for the fine grained fraction using a hydrometer analysis.

**Moisture Content** - The weight of water in a given soil mass divided by the oven dry weight of the soil; is expressed in percent.

**Nominal Maximum Size** – One size larger than the first specification sieve to retain more than 10 percent.

**Optimum Moisture** - Moisture content which will permit maximum dry density to be obtained for a given compactive effort.

**Overburden** - Surface soil or granular material which may or may not be suitable for construction purposes and overlies material that may be suitable for road or bridge construction.

**Oversize Material** - Particles that exceed the maximum size specified for a material type. For example, a <sup>3</sup>/<sub>4</sub> inch nominal maximum size plant mix pavement has a top size of <sup>3</sup>/<sub>4</sub> inch, so any material retained on a 1 inch screen or larger is considered to be oversize.

**Pavement Course or Surfacing Course (HPM or RHPM or Concrete Pavement)** - This is the uppermost layer of the surfacing section that may have a surface treatment, PMWC, and is placed on the base course. This layer is comprised of a treated granular material that is either flexible or rigid.

**Permeability** - A measure of the facility of a soil mass to transmit liquids largely dependent upon grain size distribution.

**PG Binders** - As part of the SHRP recommendations, the asphalt cement testing and classification system were developed to better characterize the design environmental conditions to improve performance by controlling rutting, low temperature cracking and fatigue cracking. Typically use PG 58-28, PG 64-22, PG 64-28. Also PG 70-28 and PG 76-28.

**Pit Run Filler** - The natural granular material passing a No. 4 screen before processing, such as crushing.

**Pitting** - Displacement of particles of aggregates from pavement surface due to action of traffic or disintegration, without major displacement of cementing material.

**Plant Mix Base (PMB)** - Crushed aggregate that may incorporate pit run material meeting a specified gradation treated with asphalt cement and placed above the subgrade, sub-base, or fill as a foundation for the pavement or surface course. The strength capacity of the PMB is greater than CB and CTB so a thinner surfacing section is the result.

**Plant Mix Pavement (PMP or HPM)** - Crushed aggregate that may incorporate pit run fines, minus No. 4 material, mixed with lime and asphalt cement meeting specified material requirements that is placed above the base course.

**Plastic Index** - The numerical difference between the liquid limit and the plastic limit. In other words, the difference between the percent of moisture at the liquid limit and the percent of moisture at the plastic limit (LL-PL).

**Plastic Limit** - The moisture content which is the boundary between the plastic and semi-solid states for the minus No. 40 fraction of a soil. For laboratory purposes, it may be defined as the minimum moisture content at which the soil fraction can be rolled into a thread <sup>1</sup>/<sub>8</sub> inch in diameter without crumbling.

**Prime Coat** - The initial application of low viscosity liquid asphalt to an absorbent base prior to placing an asphalt concrete.

**Progressive Scale** - Concrete disintegration which at first appears as surface scaling but gradually progresses deeper.

**Pumping** - Displacement and ejection of water and suspended fine particles at joint, cracks and edges.

**R-Value** - The R-Value is determined on a soil sample using the stabilometer test. R-Value is a ratio of the lateral force and the vertical pressure. The stabilometer test also is an indicator of the moisture sensitivity of the soil that may affect the strength.

**Raveling** - Progressive disintegration from surface downward or edges inward by dislodgement of aggregate particles.

**Resilient Modulus (M\_R)** - Resilient Modulus is another method of classifying the bearing capacity of a soil. This test procedure allows varying moisture and lateral forces to mimic confined and unconfined conditions.

**Resurfacing** - Supplemental surface placed on existing pavement to improve surface conformation or increase strength.

**Rigid Base and Rigid Pavement (Concrete Pavement, PCCP, or CTB)** – The term rigid indicates concrete, which is granular material, at least partially crushed, that has added Portland cement, such as concrete pavement or Cement Treated Base (CTB). Mix design testing is completed on material from a specified source to determine the mixture properties required to provide the necessary structural strength.

**Rutting** - Formation of longitudinal depressions by wheel tracking.

**Sand Equivalent (SE)** - A ratio representing the sand to fines and is used to indicate the quality of granular materials for surfacing.

**Saturated Surface Dry** - A term used to describe the condition of an aggregate in which the pores of all the particles are completely filled with water, but their surfaces are free from moisture.

Scaling - Peeling away of surface of concrete pavement.

**Screened Material** - Pit run or crusher run material that is separated into two or more size fractions and is often referred to as scalped on a certain sieve size.

Screenings or Chats - Screened material passing a linch screen.

**Seal Coat** - An application of liquid asphalt to an existing or new pavement to secure the necessary bond between the bituminous pavement and the plant mix wearing course to be placed over it.

Settlement - Reduction in elevation of short sections of pavement or structures.

Shaker - A vibratory or rotational device used to sieve undersize material out of the crushed material.

**Shoving** - Displacement of bituminous paving material due to action of traffic, generally resulting in bulging of surface.

Strategic Highway Research Program, SHRP. Due to the high costs of surfacing materials, SHRP was established by Congress to improve the performance and durability of US roads. All aspects of highway construction were considered for study and recommendations and many areas were considered including traffic control, rigid and flexible surfacing, maintenance and all aspects such as testing, field correlation and specifications.

**Slump** - A measure of the consistency of concrete.

**Soil Classification** - A soil classification system is an arrangement of different soils into groups having similar properties. The purpose is to make it possible to estimate the soil properties or strength capabilities by association with soils of the same class whose properties are known, and to provide the engineer with an accurate method of soil description.

**Spalling** - Breaking or chipping of pavement at joints, cracks or edges usually resulting in fragments with feather edges.

#### Specific Gravity -

**a.** Absolute - The ratio of the density of a solid to the density of water at a stated temperature and pressure. In other words, the ratio of the weight of a unit volume of a solid to the weight of an equal volume of water at a stated temperature.

**b. Apparent** - The ratio of the density of a permeable or impermeable material to the density of water at a stated temperature and pressure. In other words, the ratio of the weight in air of a unit volume of a material at a stated temperature to the weight in air of equal density of an equal volume of gas-free distilled water at a stated temperature. If the material is a solid, the volume shall be that of the impermeable portion.

**c.** Bulk - The ratio of the density of a permeable material to the density of water at a stated temperature and pressure. In other words, the ratio of the weight in air of a unit volume of a permeable material (including both permeable and impermeable voids normal to the material) at a stated temperature to the weight in air of equal density of an equal volume of gas-free distilled water at a stated temperature.

Stripping - Separation of bituminous films from aggregate particles due to presence of moisture.

Sub-base - Specified surfacing material of planned thickness placed as foundation for a pavement.

**Sub-base (SB or PRSB or CRSB)** - A specified surfacing course, usually granular, that overlies the subgrade and acts as the foundation for the overlying base and surface courses. The sub-base may be pit run or crusher run material from a designated source, borrow, pit, or quarry, or reused surfacing, and has a specified or implied minimum R-Value strength. This layer is typically included as part of the surfacing section as determined during the pavement structural design, but may be included as a drainage layer.

**Subgrade (Basement Soil)** - The upper limits of embankments or in-place soils upon which the pavement structure is built. Material in cuts, fills, and fill foundations immediately below the first layer of sub-base. For design purposes, the subgrade is the top two feet of soil below the dirt grade.

**Sub-sealing or Under-sealing** - Placing of waterproof material under existing pavement to arrest vertical flow of water or suspended solids and fill voids under pavement.

**Superpave (Superior Performing Asphalt Pavements)** - A test procedure developed under SHRP to replace the Marshall mix design to determine the optimum asphalt content and aggregate gradation based on the traffic level. This procedure utilizes a gyratory compactor that is intended to more closely mimic field compaction.

**Surface Scale** - Peeling away of surface mortar of Portland Cement Concrete exposing sound concrete, even though scale extends into mortar surrounding coarse aggregate.

**Surface Texture** - Character of surface of pavement which depends on size, shape, arrangement and distribution of aggregates and cement or binder.

**Surface Treatment or Surface Seal (PMWC or Chip Seal)** - This is the uppermost surfacing course that is not considered to provide structural strength, but does provide a friction layer to prevent skidding and also to seal the surface to prevent the infiltration of water. This layer is usually a chip seal or plant mix wearing course (PMWC) but could be microsurfacing or similar product.

**Tack Coat** - An application of liquid asphalt to an existing or new pavement or primed surface to secure the necessary bond between the concrete or plant mix pavement and the plant mix pavement to be placed over it.

Thrust - Pressure exerted by rigid pavement against other pavements or bridges.

Topsoil - Surface soil suitable for germination of seeds and the support of vegetative growth.

**Undersize Material (Reject)** - Material passing a specified screen size are considered to be undersized. Usually this term is used to describe the rejects or material passing the maximum size to produce the crushed material.

**Unit Weight** - The commonly used term for <u>*DENSITY*</u>. Even though its usage has been widespread over the years, it is <u>not</u> standardized nor desirable terminology. For more detailed information, <u>see AASHTO M 132</u>, <u>Appendix paragraph X1.5</u>.

**Warping** - Deviation of pavement surface from original shape caused by temperature and moisture differentials within slab.

**Warping Joint** - Joint permitting warping of pavement slabs when moisture and temperature differentials occur in pavement, i.e., longitudinal or transverse joints with bonded steel or tie bars passing through them.

**Washing** - Method utilized to remove the soils that are attached to the rock that would otherwise be knocked off the rock during crushing resulting in a high No. 200 fraction.

Water to Cement Ratio (W/C or W/(CM)) - Ratio of the weight of water to the weight of cement used in a concrete mix design; an indicator of quality. (CM) indicates the total cementicious material in the mix including portland cement, silica fume, fly ash and slag.

Water Table – Temperature/Density of Water referenced in WYDOT 213.0 and WYDOT 479.0

| Temperature<br>°F | Calibration of Measure |  |  |  |  |
|-------------------|------------------------|--|--|--|--|
| 45                | lb/ft <sup>3</sup>     |  |  |  |  |
|                   | 62.421                 |  |  |  |  |
| 46                | 62.419                 |  |  |  |  |
| 47                | 62.417                 |  |  |  |  |
| 48                | 62.415                 |  |  |  |  |
| 49                | 62.412                 |  |  |  |  |
| 50                | 62.409                 |  |  |  |  |
| 51                | 62.406                 |  |  |  |  |
| 52                | 62.402                 |  |  |  |  |
| 53                | 62.399                 |  |  |  |  |
| 54                | 62.395                 |  |  |  |  |
| 55                | 62.391                 |  |  |  |  |
| 56                | 62.387                 |  |  |  |  |
| 57                | 62.382                 |  |  |  |  |
| 58                | 62.377                 |  |  |  |  |
| 59                | 62.372                 |  |  |  |  |
| 60                | 62.367                 |  |  |  |  |
| 61                | 62.361                 |  |  |  |  |
| 62                | 62.355                 |  |  |  |  |
| 63                | 62.349                 |  |  |  |  |
| 64                | 62.343                 |  |  |  |  |
| 65                | 62.337                 |  |  |  |  |
| 66                | 62.330                 |  |  |  |  |
| 67                | 62.323                 |  |  |  |  |
| 68                | 62.316                 |  |  |  |  |
| 69                | 62.309                 |  |  |  |  |
| 70                | 62.301                 |  |  |  |  |
| 71                | 62.294                 |  |  |  |  |
| 72                | 62.286                 |  |  |  |  |
| 73                | 62.278                 |  |  |  |  |
| 73                | 62.270                 |  |  |  |  |
| 75                | 62.261                 |  |  |  |  |
| 76                | 62.252                 |  |  |  |  |
| 70                | 62.244                 |  |  |  |  |
| 77                | 62.235                 |  |  |  |  |
| 78                | 62.226                 |  |  |  |  |
| 80                | 62.216                 |  |  |  |  |
| 80                | 62.207                 |  |  |  |  |
| 81                | 62.197                 |  |  |  |  |
| 82                |                        |  |  |  |  |
|                   | 62.187                 |  |  |  |  |
| 84                | 62.177                 |  |  |  |  |
| 85                | 62.167                 |  |  |  |  |

#### SOILS TESTS AND THEIR INDICATIONS

#### Reference

Documents: AASHTO T 99

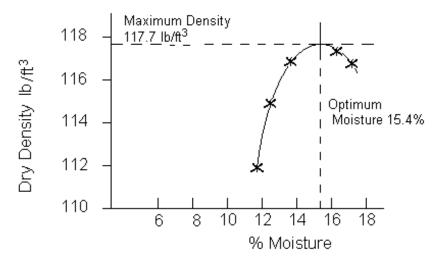
Standard Method of Test for Moisture-Density Relations of Soils Using a 2.5-kg (5.5-lb) Rammer and a 305-mm (12in.) Drop

#### Field Density Test

- 1. Purpose of the field density test:
  - a. A test procedure for assuring compliance with the density specification and moisture.
  - b. Preliminary investigation to obtain the natural density of the soil in place.
    - 1. As an indication of its bearing value as foundation.
    - 2. To aid in computing the shrinkage or swell of a soil.
- 2. WYDOT methods for determining field density:
  - a. Sand cone method.
  - b. Nuclear density method.

#### Soil Compaction Test

- 1. Purpose of the test:
  - a. To determine the density to which a soil can be compacted at various moisture contents.
  - b. To determine the maximum dry density.
  - c. To determine the optimum moisture.
  - d. To determine the minimum moisture.



#### 2. Theory of compaction:

The theory of compaction is every soil has an optimum moisture content at which it reaches a maximum density when compacted by a given compactive effort. In other words, unless a soil is compacted at its optimum moisture content, the maximum density cannot be obtained with this compactive effort. Experience has shown it is necessary to compact sub-grades, sub-bases and bases to high densities to obtain a foundation which will stand the effects of the traffic. Compaction increases the bearing value of soils and decreases compressibility minimizing settlements. Furthermore, it reduces the ability of some soils to absorb water; thus eliminating excessive expansion and softening of the subgrade lift. Since it influences so many properties of a road, it is necessary to control the compaction.

a. Density - Optimum Moisture Content:

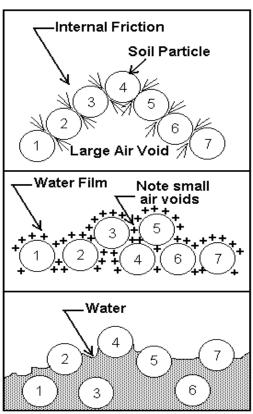
The optimum moisture content for a soil may be defined as that amount of water which will, either partially or totally, fill the voids between the soil particles. This moisture will act as a lubricant which will allow the soil particles to slide over each other and form a denser mass. Since the water content at which the soil reaches its maximum density for any given compactive effort must completely or partially fill the voids between the particles, gradation of the soil is one of the major considerations. The finer the grains of the soil, the greater the surface area of the particles and therefore, more water must be added to reach its maximum density.

Consequently, using a specified compactive effort, the density of a soil increases with an incremental increase in moisture content until the optimum moisture content is reached. At this point the soil contains sufficient moisture to lubricate its particles as well as partially satisfy its affinity for water. If the moisture content is increased beyond this point, the soil particles will be displaced by water resulting in a decrease in the density.

Regarding the tolerances in the control of moisture content, it can be stated that granular soils have a sharp peak in their compaction (moisture-density) curves; hence the tolerance in moisture content cannot be as large as in a case of a clayey soil that has a considerably flatter curve. Generally, 4 percentage points under or 2 percentage points over optimum moisture content are accepted as to produce the M - D curve.

In the laboratory or on-site, the density and the optimum moisture content of soils are determined by use of "Standard Method of Test for Moisture-Density Relations of Soils Using a 2.5-kg (5.5-lb) Rammer and a 305-mm (12- in.) Drop", AASHTO Designation T 99. In this method, the soil is compacted in a  $\frac{1}{30}$  ft<sup>3</sup> mold which is 4 inches in diameter. The soil is placed in three equal layers and compacted by 25 blows of a standard rammer on each of the three layers. The rammer has a striking face 2 inches in diameter, a weight of 5.5 lb, and a free fall of 12 inches. The density and the optimum moisture content are greatly affected by the amount of compaction and method used. Whenever the compactive effort is increased, it will result in a decrease in the optimum moisture content and an increase in the density of the soil. This, of course, can easily be explained. A higher compactive effort will require less lubricant, namely water, to facilitate the movement of the particles and at the same time will have a tendency to yield higher densities due to the increased pressure. Therefore, it is absolutely necessary to follow the standard method in every detail.

- 1. Dry soil density compaction is lower due to internal friction.
- 2. Soil at about optimum moisture. Water has overcome internal friction (lubricated soil particles).
- 3. Soil over optimum moisture replaces air voids. Soil is very unstable. (soil particles are being displaced by water).



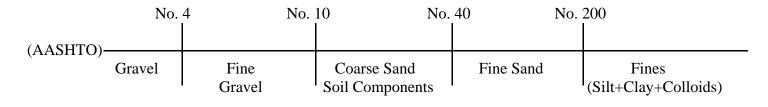
- 3. Rock Correction:
  - a. Rock is material larger than No. 4 screens that will not break down in water within 24 hours.
  - b. Rock Correction will be used when rock does not exceed 15 percent. If rock is over 15 percent, AASHTO Designation T 99 Method "C" will be used.
  - c. Rock correction, (to the nearest whole number) is equal to:

$$Rock\ Corr = \frac{Percent\ of\ Rock}{3}$$

#### Mechanical Analysis

- 1. Purpose:
  - a. Helps to analyze soils (soil classification).
  - b. Determine frost heave potentialities (10 percent or less minus No. 200 material generally resists frost).
  - c. Determine percent of soil components (gravel, sand, etc.).

#### **Screen Sizes**



#### Atterberg Limit Tests (Liquid Limit & Plastic Index)

- 1. Purpose:
  - a. Determine the 'stickiness' and cohesiveness of a soil.
  - b. Calculate the plasticity index.
- 2. Liquid Limit (LL):
  - a. Definition:
    - 1. The moisture content at which a soil passes from a plastic to a liquid state.
  - b. Indications:
    - 1. Since cohesion of a soil retards the flow, this test is an index of cohesion. Cohesion will be over-come at the liquid limit.
    - 2. Sandy soils, being low in cohesion, have low liquid limits.
    - 3. Clays have high liquid limits.
    - 4. Generally a LL of 25 or less minimizes frost action.
- 3. Plastic Limit (PL):
  - a. Definition:
    - 1. The moisture content at which a soil changes from a semi-solid to a plastic state. This is determined by rolling the soil until by loss of moisture, the soil begins to crumble when at a  $\frac{1}{8}$  inch diameter thread.
- 4. Plasticity Index (PI):
  - a. Definition:
    - 1. The numerical difference between the liquid limit and the plastic limit:

$$PI = LL - PL$$

- b. If the LL and PL are the same or if the soil cannot be rolled at the LL moisture, it is non-plastic (NP).
- c. Generally, a PI of 6 or less is required for frost prevention.

Hydrometer Analysis (typically not performed in field labs)

- 1. Purpose:
  - a. To determine percent of sand, silt, clay & colloids in a given material. (Test is performed on minus No. 10 material).
- 2. Theory:
  - b. (Stokes Law) "Particles of equal specific gravity settle in water at a rate proportional to the size of the particle."

#### Sand Equivalent (SE)

- 1. Purpose:
  - a. To determine the ratio between the sand and the fines.
  - b. Performed on processed aggregates, such as surfacing materials.
  - c. Low sand equivalent indicates a poor material.

Cementing Value (typically not performed in field labs)

- 1. Definition:
  - a. A 1 inch compacted cube of minus No. 10 material is oven dried and tested under increasing loads until failure.
- 2. Use:
  - a. An indication of the binding qualities of a surfacing material.
  - b. Generally a cementing value of 150 lb/inch<sup>2</sup> or less indicates whether the addition of a binder is required.

California Bearing Ratio (CBR) (typically not performed in field labs)

- 1. Purpose:
  - a. To determine the load supporting capacity of a soil as compared to a standard, well graded, crushed stone.

Stabilometer Test, R-Value (typically not performed in field labs)

- 1. Definition:
  - a. The resistance value (R-Value) test is a stiffness test.
  - b. The stabilometer test is a triaxial compression test and is an indication of the material's resistance to plastic flow. R-Value is calculated from the ratio of the applied vertical pressure to the developed lateral pressure.
- 2. Use:
  - a. The R-Value thickness design considers this value to determine a minimum amount of cover (surfacing).

Specific Gravity, G<sub>s</sub>

1. Definition:

#### WYDOT 101.0 (Rev. 10-17)

a. The ratio of the density of a material to the density of water at the same temperature:

$$G_S = \frac{A}{B-E}$$

A = weight of oven dry sample in air

B = weight of saturated, surface dry sample in air

E = weight of saturated sample in water

Note: Use the same unit of weight for A, B & E. (G<sub>S</sub> is unitless)

#### SOIL CLASSIFICATION SYSTEM

- Scope: This practice describes classifying soils into seven groups based on laboratory determination of particle size distribution, liquid limit, and plasticity index. Evaluation of soils within each group is made by means of a "group index," which is a value calculated from an empirical formula.
- Use: The group classification, including group index, is useful in determining the relative quality of the soil material for use in earthwork structures, particularly embankments, subgrades, subbases, and bases. However, for the detailed design of important structures, additional data concerning strength or performance characteristics of the soil under field conditions will usually be required.

#### Reference Documents: AASHTO M 145 Standard Specification for Classification of Soils and Soil -Aggregate Mixtures for Highway Construction Purposes

Procedure: With required test data available, proceed from left to right on chart; the correct group will be found by process of elimination. The first group from the left into which the test data will fit is the correct classification.

| General<br>Classification                                   |                            | Granular Materials<br>35% or less of total sample passing |                      |                  |                  | 00               |                  |                  | More than        | y Materials<br>35% of total<br>sing No. 200 |                  |
|---|----------------------------|---|----------------------|------------------|------------------|------------------|------------------|------------------|------------------|---|------------------|
|   | A                          | <b>-</b> -1   |                      |                  | А                | -2               |                  |                  |                  |   | A-7*             |
| Group<br>Classification                                     | A-1-a                      | A-1-b   | A-3                  | A-2-4            | A-2-5            | A-2-6            | A-2-7            | A-4              | A-5              | A-6   | A-7-5<br>A-7-6   |
| Sieve analysis,<br>% passing<br>No. 10<br>No. 40<br>No. 200 | 50 max<br>30 max<br>15 max | <br>50 max<br>25 max                                      | <br>51 min<br>10 max | <br><br>35 max   | <br><br>35 max   | <br><br>35 max   | <br><br>35 max   | <br><br>36 min   | <br><br>36 min   | <br><br>36 min                              | <br><br>36 min   |
| Liquid Limit<br>Plasticity Index                            | 6 max                      | 6 max   | NP                   | 40 max<br>10 max | 41 min<br>10 max | 40 max<br>11 min | 41 min<br>11 min | 40 max<br>10 max | 41 min<br>10 max | 40 max<br>11 min                            | 41 min<br>11 min |
| General Rating as<br>Subgrade                               |                            |   | Excellent            | to               | Good             |                  |                  | Fair             | to               | Poor  |                  |

#### AASHTO SOIL CLASSIFICATION CHART

\* For A-7 Soils:

A-7-5 when  $PI \le (LL - 30)$ A-7-6 when PI > (LL - 30)

Group Index,  $GI = GI_{LL} + GI_{PI}$  except for A-2-6 and A-2-7 soils in which  $GI = GI_{PI}$ 

| $GI_{LL}$ | = | (F - 35) x (0.2 + (0.005 x (LL - 40))) | F  | = | percent passing No. 200 sieve |
|-----------|---|--|----|---|-------------------------------|
| $GI_{PI}$ | = | 0.01 x (F - 15) x (PI - 10)            |    |   | Liquid Limit                  |
|           |   |  | PI | = | Plasticity Index              |

Group Index values should always be shown in parenthesis after the group classification, such as, A-2-6(3), A-4(5), A-6(12), A-7-5(17), etc. Under average conditions of good drainage and thorough compaction, a group index of 0 indicates a good subgrade material and a group index of 20 or more indicates a poor subgrade material.

Example: Assume A-7 material with 80 percent passing the No. 200 sieve, LL = 90, & PI = 50.

 $\begin{array}{l} GI_{LL} = (80 - 35) \; x \; (0.2 + (0.005 \; x \; (90 - 40) \; ) \; = 45 \; x \; (0.2 + (0.005 \; x \; 50)) = 45 \; x \; 0.45 = 20.3 \\ GI_{PI} = 0.01 \; x \; (80 - 15) \; x \; (50 - 10) = 0.01 \; x \; 65 \; x \; 40 = 26.0 \\ GI = 20.3 + 26 = \underline{46.3} \end{array}$ 

PI = 50, LL - 30 = 60, therefore group classification is A-7-5 since  $PI \le (LL - 30)$ 

Classification: A-7-5(46)

Description of Classification Groups:

| A-1 Soils | Well graded sands and gravels. Satisfactory treated surface. Good base, with thin pavement. Excellent fill.   |
|-----------|---|
| A-2 Soils | Poorly graded sands and gravels. Good base for moderate, thickness flexible or relatively thin, thickness rigid pavement. Good fill. Frost detrimental if plastic. Softens when wet if plastic. Not to be used for base if PI is greater than three or for subbase if PI is greater than six. |
| A-3 Soils | Mostly clean sands. Good base for moderate flexible or thin rigid pavement. Good fill. No frost conditions.   |
| A-4 Soils | Silty soils. Poor base. Absorbs water. Unstable when wet. Frost very detrimental. Use sub-drainage with flexible pavement.  |
| A-5 Soils | Elastic silts. Absorbs water. Frost very detrimental. Use sub-drainage with good granular base. Not suited for base.  |
| A-6 Soils | Clays. Stable and impermeable when dry or undisturbed. Plastic and absorbent when disturbed. Bad pumping into porous base. Shrinks and cracks when dry. Use tight granular base. Frost heave is slight when well compacted. Thick, strong flexible pavement design is indicated.              |
| A-7 Soils | Expansive, plastic clays. Excessive volume change. Frost very detrimental.<br>Sub-drainage is not effective. Thick dense flexible pavement is indicated.<br>Sometimes excavation and waste or stabilization is indicated.   |

Muck & Peat Excavate to solid stratum and replace with selected fill. In some cases, this may be used in lower limits of fill when blended with other materials.

|   |  | Iviaj  | OI DIVISIONS OI   | 30118  |   |
|---|--|--|---|--|---|
| Sieve Analysis<br>Coarse Grained (Granular) |  | Hydromet   | er Analysis   |  |   |
|   |  | Fine C   | Grained   | Organic                                      |   |
| Gravel                                      | Sand                                       | Silt   | Clay  | Muck   | Peat  |
| No plasticity,<br>gritty,<br>granular       | No plasticity,<br>grains easily<br>visible | No plasticity,<br>fine, grains<br>barely visible,<br>no cohesion | Highly plastic,<br>cohesive, can<br>be rolled into<br>ribbon when<br>wet, remains<br>suspended in<br>water 3+ hours | Thoroughly<br>decomposed<br>organic material | Partly decayed<br>plant material,<br>mostly organic,<br>fibrous |
|   | N  | lo. 200  |   |  |   |
|   |  | Minus  | No. 200   |  |   |

#### Major Divisions of Soils

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#### MATERIALS ACCEPTANCE

#### CONSTRUCTION TEST AND CERTIFICATION REQUIREMENTS

- Scope: WYDOT uses a combination of sampling, testing, manufactured product documentation (certification), and inspection to establish conformance of materials to project plans and specifications. Generally, three forms are developed for each construction project by the WYDOT Materials Program to provide guidelines for materials acceptance testing and documentation requirements. They are WYDOT Forms: T-128 *Construction Test Requirements*, T-131 *Manufactured Products Received*, and T-132 *Engineer's Verification of Specification Compliance*.
- Use: Form T-128 *Construction Test Requirements*, lists the specified sampling and testing frequencies for construction materials. Included in Form T-128 are sections for each construction material, identified from the project plans and specifications, where testing by the contractor or WYDOT is required to determine compliance to the applicable specification. A Form T-128 is generated and sent to the Resident Engineer for each project.

Form T-131 *Manufactured Products Received*, lists the documentation requirements (Acceptance Criteria) for manufactured goods and products where documentation provided by the manufacturer or supplier is required to verify compliance to the applicable specification. Included in Form T-131 are sections for each manufactured product identified from the project plans and specifications. Within each section are fields containing the material / product name, acceptance criteria, bid item number(s), and, if available, the plan quantity. Field identification, quantity, and comment fields are provided for field personnel to list certification documents received and the quantity being certified or received. Fields are provided for the total quantity documented, final quantity and the identification of the person preparing the final. Manufactured products added to the project must be documented as well. Form T-131 is generated and sent to the Resident Engineer and Prime Contractor for each project. This form is available in MS Excel in the Falcon project directory.

Form T-132 *Engineer's Verification of Specification Compliance*, may be used to document acceptance of certain construction materials and manufactured goods when exceptions exist to verify specification compliance. This method of acceptance may be used only when specifically noted in Forms T-128 or T-131.

Reference Documents

| cuments: | WYDOT T-128 | Construction Test Requirements                      |
|----------|-------------|---|
|          | WYDOT T-131 | Manufactured Products Received                      |
|          | WYDOT T-132 | Engineer's Verification of Specification Compliance |

Form T-128 11/12

|    | 1   | 0     | 2     |    |
|----|-----|-------|-------|----|
| 1  | 12  | +     | 1     |    |
| 17 | 1   |       |       | A  |
| 10 | TRA | 10.10 | THE O | ~) |

#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY

CONSTRUCTION TEST REQUIREMENTS

2010 Specifications

| PROJECT NUMBER  | PART     |                         | STATION   |
|---|----------|-------------------------|---|
| NHPPI-1806205   | <b>I</b> |                         | 21+10.22 TO 570+75.61   |
|   |          |                         | R.M.  |
|   |          |                         | 362.040 TO 372,400  |
| LOCATION  |          | DISTRICT                | LENGTH  |
| Cheyenne-Pine Bluffs (Central Ave - Archer EBL Section) |          | 1                       | 10.48 MI  |
| COUNTY  |          | DATE LET                |   |
| Laramie   | ľ        | 9/8/2016                |   |
| ENGINEER  |          | CONTRACTOR              | A CONTRACT OF A |
| Wayne Shenefelt, Cheyenne, WY                           |          | Mountain Construction C | Company, Lovell, WY   |

#### MILLING PLANT MIX

| Bid Item Number(s): 202.03305                |             |              |          |            |  |
|--|-------------|--------------|----------|------------|--|
|  | DESIGNATION | FREQUENCY    | QUANTITY | # REQUIRED |  |
| Acceptance - Macrotexture Analysis (SS-200D) | A - MACRO   | 1 / mile min | 20.84 MI | 21 min     |  |

#### FLOWABLE BACKFILL Rid Item Number(s): 206 03400

|                                    | DESIGNATION | FREQUENCY      | QUANTITY | # REQUIRED |
|------------------------------------|-------------|----------------|----------|------------|
| Acceptance - Aggregate Gradation   | W-A-FB      | 1 ea. 500 CY   | 20 CY    | 1 min *    |
| Check Sample - Aggregate Gradation | CS-A-FB     | 1 ea. 2,500 CY | 20 CY    | 1 min *    |

HOT PLANT MIX (RECYCLE) QC/QA LEVEL OF CONTROL 2 (Type II, Class II-S, 1/2" Nom. Max., w/PG 76-28)

#### Bid Item Number(s): 401.03310

| Pavement Smoothness Analysis                                    | Per SS-400B (Report On Form T-515) |                               |          |                  |  |  |
|---|------------------------------------|-------------------------------|----------|------------------|--|--|
| Quality Acceptance - Mix Production <sup>(6)</sup> (Contractor) | DESIGNATION                        | FREQUENCY (1)                 | QUANTITY | # REQUIRED       |  |  |
| Mix Volumetrics   | QA - HPMR - MV                     | See Specifications *          | 45,550 T | 12 min           |  |  |
| Virgin Aggregate Gradation                                      | QA-HPMR-G                          | 1 lot / 5,000 ton             | 45,550 T | 10 lots          |  |  |
| Asphalt Binder Content (Volume Analysis)                        | QA - HPMR - BC                     | 1 lot ea. day                 | ? Day    | ? lot(s).        |  |  |
| Virgin Aggregate Liquid Limit (7)                               | QA - HPMR - LL                     | 1 / 1,000 ton min             | 45,550 T | 46 or 0          |  |  |
| Virgin Aggregate Plasticity Index (7)                           | QA - HPMR - PI                     | 1 / 1,000 ton min             | 45,550 T | 46 or 0          |  |  |
| Virgin Aggregate Coarse Aggregate Angularity (7)                | QA - HPMR - CAA                    | 1 / 1,000 ton min             | 45,550 T | 46 or 0          |  |  |
| Virgin Aggregate Fine Aggregate Angularity (7)                  | QA - HPMR - FAA                    | 1 / 1,000 ton min             | 45,550 T | 46 or 0          |  |  |
| Virgin Aggregate Flat & Elongated (7)                           | QA - HPMR - F&E                    | 1 / 1,000 ton min             | 45,550 T | 46 or 0          |  |  |
| Moisture Content of Virgin Aggregate/Hydrated Lime              | QA-HPMR-MVA                        | 1 ea. day min                 | ? Day    | 1 / day.         |  |  |
| Moisture Content of Mix   | QA-HPMR-MM                         | 1 ea. day min                 | ? Day    | 1 / day.         |  |  |
| /erification Testing - Mix Production (WYDOT/Contractor)        | DESIGNATION                        | FREQUENCY                     | QUANTITY | # REQUIRED       |  |  |
| Mix Volumetrics   | V-HPMR-MV                          | See Specifications * *        | 45,550 T | ?                |  |  |
| Virgin Aggregate Gradation                                      | V-HPMR-G                           | 1/ lot                        | 10 lots  | 10               |  |  |
| Asphalt Binder Content (Volume Analysis)                        | V-HPMR-BC                          | No tests required             | 45,550 T | No tests require |  |  |
| Virgin Aggregate Liquid Limit                                   | V - HPMR - LL                      | 1 / mix design <sup>(8)</sup> | 45,550 T | 1 min            |  |  |
| Virgin Aggregate Plasticity Index                               | V - HPMR - PI                      | 1 / mix design <sup>(8)</sup> | 45,550 T | 1 min            |  |  |
| Virgin Aggregate Coarse Aggregate Angularity                    | V - HPMR - PI                      | 1 / mix design <sup>(8)</sup> | 45,550 T | 1 min            |  |  |
| Virgin Aggregate Fine Aggregate Angularity                      | V - HPMR - PI                      | 1 / mix design <sup>(8)</sup> | 45,550 T | 1 min            |  |  |
| Flat & Elongated  | V-HPMR-F&E                         | 1 / mix design <sup>(8)</sup> | 45,550 T | 1 min            |  |  |
| Moisture Content of Virgin Aggregate/Hydrated Lime              | V - HPMR - MCVA                    | 1 / mix design <sup>(6)</sup> | 45,550 T | 1 min            |  |  |
| Moisture Content of Mix   | V- HPMR - MCMIX                    | 1 / mix design <sup>(8)</sup> | 45,550 T | 1 min            |  |  |
| Quality Acceptance - In-Place Density (Contractor)              | DESIGNATION                        | FREQUENCY                     | QUANTITY | # REQUIRED       |  |  |
| Designation I   | QA - HPMR - D - I                  | 1 lot / 1500 ton              | 45,550 T | 31 lots          |  |  |
| /erification Testing - In-Place Density (WYDOT/Contractor)      | DESIGNATION                        | FREQUENCY                     | QUANTITY | # REQUIRED       |  |  |
| Designation I   | V-HPMR-D-I                         | 1/ lot                        | 31 lots  | 31               |  |  |

\*\* Split sample required but no test frequency specifically required
 (1) Testing frequencies shown are minimum quantities. Example: 1 min/1000 ton [1 min/1000 to] (5). Acceptance-tests may be used for quality control purposes.
 (6) Perform acceptance testing.
 (7) If, during aggregate production, the test results for LL, PI, coarse aggregate angularity, fine aggregate angularity, and flat & elongated were within specification, the department will not require retaining.
 (8) LL, PI, and coarse and fine aggregate angularity only.

#### (CONTINUED NEXT PAGE)

#### Page 1 OF 4

NHPPI-1806205

9/23/2016

FORM T-131 REV 3/00

## Wyoming Department of Transportation Materials Laboratory

Manufactured Products Received

Project No(s). NHPPI-1806205

Location Cheyenne-Pine Bluffs (Central Ave - Archer EBL Section) Engineer Wayne Shenefelt, Cheyenne, WY Contractor Mountain Construction Company, Lovell, WY

#### Product Documentation Guidelines

#### Any product documentation must include:

the name and address of the business or person certifying the product(s)

the name of the manufacturer(s) of the product(s)

common names(s) of the product(s) being certified

the quantity of the product(s) being certified

the specification(s) to which the product(s) was manufactured

a statement of certification

the signature of a person having legal authority for the manufacturer/supplier

date of the signature

mill test reports or manufacturer's certification that all manufacturing and coating processes of steel and iron products occurred in the United States of America

Reference the Manufactured Product Acceptance Procedure for additional information and explanation.

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| Item/Description:            | PORTLAND CEMENT, ASTM C 150, TYPE II, LOW ALKALI  |                            |   |  |
|------------------------------|---|----------------------------|---|--|
| Acceptance Criteria:         | Certification & Chemical Analysis or Engineer's Verification (if < \$1500 w/ Specification Label) |                            |   |  |
| Bid Item #: 206.031, 507.01, | 508.01101, 513.00005, 513.000   | 15, 515.028"               |   |  |
| Plan Quantity                | <i>I</i> ;  | Final Quantity:            |   |  |
| Field I.D.                   | Quantity  | Comments                   |   |  |
|                              |   |                            |   |  |
|                              |   |                            | _ |  |
|                              |   |                            |   |  |
|                              | Buy America C   | Compliant 🗆 Yes 🖾 No 🗔 N/A |   |  |
| Verified By:                 |   | Quantity Documented:       |   |  |
|                              |   |                            | - |  |
| Item/Description:            | AIR ENTRAINING ADMIXTURE, AASHTO M 154  |                            |   |  |
| Acceptance Criteria:         | Certification or Engineer's Verification if Pre-Certified (See Field Testing Manual)              |                            |   |  |

| Plan Quantity: |                      | Final Quantity:          |  |
|----------------|----------------------|--------------------------|--|
| Field I.D. G   | Quantity             | Comments                 |  |
| 2 - 2 2        |                      |                          |  |
|                |                      |                          |  |
|                |                      |                          |  |
|                |                      |                          |  |
|                | Buy America Com      | ipliant 🗆 Yes 🛛 No 🗆 N/A |  |
| Verified By:   | Quantity Documented: |                          |  |

## Wyoming Department of Transportation

|   | A          |
|---|------------|
|   | AMA        |
| 1 | 7 A A      |
| 5 | massemilas |

#### Materials Laboratory

Verification of Specification Compliance

(Use to document accepting products and materials without certification and/or testing)

Project No(s): NHPPI-1806205

Location: Cheyenne - Pine Bluffs (Central Ave - Archer EBL Section)

Resident Engineer: Wayne Shenefelt, Cheyenne, WY

Contractor: Mountain Construction Company, Lovell, WY

| By:       Date:         Item/Description:  |           |
|--|-----------|
| Quantity Accepted:         By:       Date:         Item/Description:         Acceptance Criteria       Bidge Program Approval         Commercial Products List (QPL)       Materials Program Approval         Commercial Products       Commercial Product         Catagorithm       State Traffic Engineer Approval         Catagorithm       Other (Documentation         Brand Name:       Date:         Quantity Accepted:       Bridge Program Approval         By:       Date:         Item/Description:       Acceptance Criteria         Acceptance Criteria       Bridge Program Approval         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval         Commercial Product       Commercial Product         By:       Date:         Item/Description:       Contractor Reained O         Catagorithm       State Traffic Engineer Approval         Contractor Reained O       State Traffic Engineer Approval         By:       Date:         Quantity Accepted:       By:         By:  | Ownership |
| Item/Description:       Bidge Program Approval       Engineer Approval (Ins         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Specification Label  |           |
| Item/Description:       Bidge Program Approval       Engineer Approval (Ins         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Specification Label  |           |
| Acceptance Criteria       Bidge Program Approval       Engineer Approval (Ins         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Name Brand in Contract   |           |
| Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product:         Contractor Retained O       State Traffic Engineer Approval       Other (Documentation         Brand Name:       Date:       Item/Description:         Acceptance Criteria       Bridge Program Approval       Commercial Product         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Engineer Approval (Instance Approval)         Contractor Retained O       State Traffic Engineer Approval       Commercial Product         Item/Description:       Item/Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Specification Label  |           |
| Quantity Accepted:         By:       Date:         Item/Description:         Acceptance Criteria       Bridge Program Approval         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval         Commercial Product       Commercial Product         State Traffic Engineer Approval       Contractor Retained O         \$1500 w/ Specification Label       ITS Program Approval         \$1500 w/ Name Brand in Contract       State Traffic Engineer Approval         Brand Name:       Outer         Quantity Accepted:       Date:         By:       Date:         Item/Description:       Bridge Program Approval         Acceptance Criteria       Bridge Program Approval         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval         Contractor Retained O       Contractor Retained O         State Traffic Engineer Approval       Other (Documentation         Brand Name:       Outantity Accepted:         By:       Date:         State Traffic Engineer Approval       Other (Documentation  | Ownership |
| By:       Date:         Item/Description:       Bridge Program Approval       Engineer Approval (Instantiation of the second of                                    |           |
| Item/Description:       Bridge Program Approval       Engineer Approval (Instead of the commercial Product |           |
| Acceptance Criteria       Bridge Program Approval       Engineer Approval (Instead of the products List (QPL)         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Name Brand in Contract   |           |
| Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Specification Label  |           |
| Quantity Accepted:       Date:         By:       Date:         Item/Description:   | Ownership |
| By:     Date:       Item/Description:  |           |
| Item/Description:  |           |
| Acceptance Criteria       Bridge Program Approval       Engineer Approval (Ins         Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Specification Label   |           |
| Pre-Certified / Qualified Products List (QPL)       Materials Program Approval       Commercial Product         < \$1500 w/ Specification Label  |           |
| Quantity Accepted:<br>By: Date:<br>Statement of Acceptance   | Ownership |
| By: Date:  |           |
| itatement of Acceptance  |           |
|  |           |
| I hereby certify that the above listed items meet the requirements as set forth in the plans<br>and/or specifications and have been accepted using the above mentioned criteria.   |           |
| By: Date:  |           |

#### MATERIALS ACCEPTANCE - MANUFACTURED PRODUCTS

#### MATERIALS CERTIFICATIONS FORM T-168, Certification of Materials

- Scope: To ensure manufactured products meet the applicable specification WYDOT requires products delivered to the project site be accompanied by certification documents stating the specification the items were manufactured to meet.
- Use: Generally, the materials certification for manufactured products on WYDOT projects is the Form T-168, *Certification of Materials*. The Materials Program provides one blank Form T-168, *Certification of Materials*, for each item identified from the plans and specifications that will be accepted by certification. The contractor, in turn, is to provide these forms to sub-contractors and eventually to the material suppliers and manufacturers. The manufacturer or supplier can then complete the Form T-168, *Certification of Materials*, and return it with the product to the project site.

WYDOT accepts forms of certification other than Form T-168, *Certification of Materials*, including statements of compliance on test reports, letters-of-certification, etc., although in order to be considered valid, all certification documents must provide the information shown below:

#### PRODUCT DOCUMENTATION GUIDELINES

Product documentation must include:

WYDOT PROJECT NUMBER

Name and address of the business or person certifying the product Name of the manufacturer of the product Common (trade) name of the product Quantity of the product Specifications to which the product was manufactured Statement of certification Signature of a person having legal authority for the supplier or manufacturer Printed or typed name corresponding to the signature Date of signature

#### SUPPORTING DOCUMENTS

For many products, supporting documentation must also accompany the certification in order for the certification to be complete and valid. In most cases, the required supporting documents are listed in the "Acceptance Criteria" field on Form T-131, *Manufactured Products Received*. Examples of supporting documents include Seed Analysis Reports for each lot of seed, Transit Certificates for Dry Mulch, Typical Chemical Analysis Reports for Portland Cement & Fly Ash, and Mill Test Reports for Steel products.

#### INSPECTION

It is important for the WYDOT inspector to verify that material delivered to the project site is undamaged and that the certification documents represent the materials delivered to the project. Compare the description and quantity to the product delivered and verify that the specification designation, lot, batch and heat number match up with the markings on the product and the specification listed in the project contract documents.

Reference Documents:

WYDOT T-131 WYDOT T-168 Manufactured Products Received Certification of Materials



T-168 (Rev. 09-16)

## **CERTIFICATION OF MATERIALS**

| WYDOT Project No. ERP Project Number |               |                      |                 | WYDOT Field Identification                     |
|--------------------------------------|---------------|----------------------|-----------------|--|
| Location As                          | per plans     |                      |                 | (Date - Sequence Rec'd - Inspector's Initials) |
| The                                  | Supplier      | Company Name         | Supplier        | Supplier                                       |
| 3                                    | (Name of Manu | facturer/Supplier)   | (Address)       | (City, State)                                  |
| has furn                             | ished to      | Company Name         | Company address | Company City                                   |
|                                      | <u> </u>      | (Name of Contractor) | (Address)       | (City, State)                                  |

the following materials for use in the construction of the above referenced project.

| WYDOT<br>Bid Item Number | Product Description<br>or Use | Quantity | Unit<br>LF, YD², m,<br>m², etc. | Manufacturer | Applicable Specification<br>(AASHTO, ASTM, WYDOT, etc.) |
|--------------------------|-------------------------------|----------|---------------------------------|--------------|---|
| Per Plans                | Per Plans                     | Plans    | Plans                           | Company Name | Per plans   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |
|                          |                               |          |                                 |              |   |

(Mill Test Reports, Heat Numbers, Chemical Analysis Reports, Coating Thickness Reports, Seed Analysis Reports, Transit Certificates, etc. must accompany this form where applicable.)

|     | State   | ement of Certification  |
|-----|---|---|
|     | I hereby certify that the above listed items of n | naterials do meet the requirements as set forth in the plans and/or specifications. |
| By: |   | Title:  |
|     | (Name Typed or Printed)                           |   |
|     |   | Date:   |
|     | (Signature)                                       |   |
|     |   | n triplicate to the contractor who, in turn, must submit two copies<br>his project. |

Distribution:

White : Materials Laboratory Yellow: Resident Engineer Pink: Contractor Gold: Manufacturer/Supplier Copies of this form are available from: WYDOT Purchasing Program Attn: Storeroom Manager P.O. Box 1708 Cheyenne, WY 82003-1708

REORDER # FR-6140

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#### FIELD LABORATORY TESTING EQUIPMENT: STANDARD SOILS KIT

- 1. Chisel and hammer
- 2. Moisture tins, 3 oz
- 3. Moisture tins, 8 oz
- 4. Moisture tins, 16 oz
- 5. Graduated cylinder, 100 ml
- 6. Straightedge, 15 inch
- 7. Measure,  $0.1 \text{ ft}^3$
- 8. Compaction mold,  $0.03 \text{ ft}^3$  (base plate optional)
- 9. Compaction rammer and guide,  $5\frac{1}{2}$  lb
- 10. No. 4 Screen, round, 16 inch diameter (WYDOT Catalog # FT6440)
- 11. Pan, 16 inch diameter (WYDOT Catalog # FT5420)
- 12. Compaction block, 300 lb minimum (Standard Plan 106-1A)
- 13. Removal press and plug for samples
- 14. Stove for drying or infra-red heater
- 15. Balance (high capacity), sensitive to 0.1 lb [50 g]
- 16. Balance (low capacity), sensitive to 0.0002 lb [0.1 g]
- 17. Trowel, 5 inch
- 18. Wood block, 2 inch x 4 inch
- 19. Sample splitter: one large mechanical splitter
- 20. Sand cone apparatus, 1 gal [4 L] (jar and funnel)
- 21. Standard calibration sand (not less than 100 lb)
- 22. Containers with lids; suggest concrete cylinder cans and lids
- 23. Rammer with guide, 5 <sup>1</sup>/<sub>2</sub> lb
- 24. Spoon (large)
- 25. Shovel (and pick, if required)
- 26. Brass brush
- 27. Canvas sample bags
- 28. Mortar
- 29. Pestle (rubber tipped)
- 30. Liquid limit device
- 31. Grooving tool
- 32. Porcelain casserole
- 33. Spatula
- 34. Ground glass plate
- 35. Suitable pans
- 36. U.S. Standard Sieves, 8 inch diameter:

| 2 inch                           | [50 mm]   |
|----------------------------------|-----------|
| <sup>3</sup> / <sub>4</sub> inch | [19 mm]   |
| No. 4                            | [4.75 mm] |
| No. 10                           | [2.00 mm] |
| No. 20                           | [850 µm]  |
| No. 40                           | [425 µm]  |
| No. 200                          | [75 µm]   |

WYDOT 120.0 (Rev. 09-16)

37. Kit box

- 38. Shipping envelopes
- 39. WYDOT Forms:

T-112 Soil Compaction Worksheet \*T-113 Weekly Report for Compaction of Embankment/Crushed Base/Other T-140 Plotting Worksheet

\*Weekly report no longer mandatory but optional

#### FIELD LABORATORY TESTING EQUIPMENT: STANDARD SURFACING KIT

- 1. Moisture tins, 3 oz
- 2. Moisture tins, 16 oz
- 3. Graduated cylinder, 100 ml
- 4. Straightedge, 15 inch
- 5. Measure,  $0.1 \text{ ft}^3$
- 6. Compaction mold,  $0.03 \text{ ft}^3$  (base plate optional)
- 7. Compaction rammer and guide, 5<sup>1</sup>/<sub>2</sub> lb
- 8. No. 4 screen, round, 16 inch diameter (WYDOT Catalog # FT6440)
- 9. Pan, 16 inch diameter (WYDOT Catalog # FT5420)
- 10. Compaction block, 300 lb minimum (Standard Plan 106-1A)
- 11. Removal press and plug for samples
- 12. Stove for drying or infra-red heater
- 13. Balance, high capacity, sensitive to 0.1 lb [5 g]
- 14. Balance, low capacity, sensitive to 0.0002 lb [0.1 g]
- 15. Trowel, 5 inch
- 16. Sample splitter: one large mechanical splitter
- 17. Sand cone apparatus, 1 gal [4 l] (jar and funnel)
- 18. Standard calibration sand (not less than 100 lb)
- 19. Chisel and hammer
- 20. Containers with lids; suggest concrete cylinder cans and lids
- 21. Rammer with guide, 5 <sup>1</sup>/<sub>2</sub> lb
- 22. Spoon (large)
- 23. Shovel (flat square nose)
- 24. Wood block, 2 inch x 4 inch
- 25. Canvas sample bags
- 26. Container, 5 gal for sampling
- 27. Mortar
- 28. Pestle (rubber tipped)
- 29. Liquid limit device
- 30. Grooving tool
- 31. Porcelain casserole
- 32. Spatula, 4 inch long x 1 inch wide (with straight edge)
- 33. Ground glass plate
- 34. Suitable wash pans
- 35. Scoop (flat square nose)
- 36. Thermometers, 50 °F to 500 °F and 0 °F to 120 °F
- 37. Coring machine
- 38. Wire basket and chain
- 39. Container, 5 gal (with overflow)
- 40. Asbestos gloves
- 41. Brush sweeping
- 42. Brush brass
- 43. Large mechanical shaker with screens
- 44. Sieve shaker for 8 inch diameter sieves

WYDOT 121.0 (Rev. 09-16)

- 45. No. 8 sieve for washing
- 46. No. 200 sieve for washing

47. U.S. Standard Sieves, 8 inch diameter and / or large shaker:

| 2 ½ inch                         | [53 mm]   | C                  |
|----------------------------------|-----------|--------------------|
| 2 inch                           | [50 mm]   |                    |
| 1 ½ inch                         | [37.5 mm] |                    |
| 1 inch                           | [25.0 mm] |                    |
| <sup>3</sup> ⁄ <sub>4</sub> inch | [19.0 mm] |                    |
| <sup>1</sup> / <sub>2</sub> inch | [12.5 mm] |                    |
| <sup>3</sup> / <sub>8</sub> inch | [9.5 mm]  |                    |
| No. 4                            | [4.75 mm] | (for large shaker) |
| Pan                              |           | (for large shaker) |

48. U.S. Standard Sieves, 8 inch diameter:

| No. 4          |      | [4.75 mm] |
|----------------|------|-----------|
| No. 8          |      | [2.36 mm] |
| No. 10         |      | [2.00 mm] |
| No. 20         |      | [850 µm]  |
| No. 30         |      | [600 µm]  |
| No. 40         |      | [425 µm]  |
| No. 50         |      | [300 µm]  |
| No. 100        |      | [150 µm]  |
| No. 200        |      | [75 µm]   |
| Pan            |      |           |
| <b>T</b> • 1 / | C* * | ``        |

Lid (snug fitting)

- 49. Funnel stand with funnel,  $1\frac{1}{4}$  inch  $\pm$ , above cylinder
- 50. Jar (cylinder) and funnel bottom opening of  $\frac{1}{2}$  inch  $\pm \frac{1}{8}$  diameter
- 51. Proportional caliper device
- 52. WYDOT Forms:

\*T-102 Report of Field Tests on Surfacing Materials

- T-120 Sample Transmittal
- T-166 Aggregate Analysis

\*Weekly report no longer mandatory but optional

### FIELD LABORATORY TESTING EQUIPMENT: STANDARD CONCRETE KIT

- 1. Rubber tired wheel borrow
- 2. Balance, high capacity (sensitive to 0.1 lb [50 g])
- 3. Balance, low capacity (sensitive to 0.0002 lb [0.1 g])
- 4. Slump cone
- 5. Pan, 15 inch x 15 inch
- 6. Tamping rod (bullet-point), <sup>5</sup>/<sub>8</sub> inch
- 7. Tamping rod (bullet-point), <sup>3</sup>/<sub>8</sub> inch
- 7. Rubber or rawhide mallet,  $1.25 \pm 0.50$  lb
- 8. Trowel, 5 inch
- 9. Scoop (large)
- 10. Straightedge, 15 inch
- 11. Stove for drying or infra-red heater
- 12. Ruler, incremented in millimeters and inches
- 13. Air meter apparatus: including 12 inch x 12 inch x 0.5 inch plexiglass plate and water bulbs
- 14. Shovel
- 15. Concrete cylinder cans with lids (cases available, any number of cylinders can be taken)
- 16. Suitable wash pans
- 17. Sample splitters, one large field splitter or quartering canvas
- 18. Beam molds, 6 inch x 6 inch x 20 inch
- 19. Wood float
- 20. Brass brush
- 21. Large mechanical shaker with screens
- 22. Sieve shaker for 8 inch diameter sieves
- 23. No. 8 sieve for washing
- 24. No. 200 sieve for washing
- 25. U.S. Standard Sieves 8 inch diameter and / or large shaker:

| 2 <sup>1</sup> / <sub>2</sub> inch | [53 mm]   |                    |
|------------------------------------|-----------|--------------------|
| 2 inch                             | [50 mm]   |                    |
| 1 ½ inch                           | [37.5 mm] |                    |
| 1 inch                             | [25.0 mm] |                    |
| <sup>3</sup> / <sub>4</sub> inch   | [19.0 mm] |                    |
| <sup>1</sup> / <sub>2</sub> inch   | [12.5 mm] |                    |
| <sup>3</sup> / <sub>8</sub> inch   | [9.5 mm]  |                    |
| No. 4                              | [4.75 mm] | (for large shaker) |
| Pan                                |           | (for large shaker) |
|                                    |           |                    |

26. U.S. Standard Sieves 8 inch diameter:

| No. 4           | [4.75 mm] |
|-----------------|-----------|
| No. 8           | [2.36 mm] |
| No. 16          | [1.18 mm] |
| No. 30          | [600 µm]  |
| No. 50          | [300 µm]  |
| No. 100         | [150 µm]  |
| No. 200         | [75µm]    |
| Pan             |           |
| Lid (snug fitti | ng)       |
|                 |           |

WYDOT 122.0 (Rev. 09-16)

27. Kit box
28. Transmittal envelopes
29. WYDOT Forms:

\*T-101 Report of Field Tests on Concrete Aggregate
T-109 Concrete Placing Report
T-120 Sample Transmittal
T-166 Aggregate Analysis

\*Weekly report no longer mandatory but optional

### **INVESTIGATION OF GRAVEL DEPOSITS**

- Scope: The intent of a preliminary investigation is to assess the available quantity of suitable material available and determine whether the material meets the minimum aggregate requirements for the products to be produced; reference Section 106.3.3.3.
- Apparatus: 1. Backhoe capable of digging a minimum of 15 feet
  - 2. Shovel with a flat square nose
  - 3. Clean canvas sample sacks
  - 4. Form T-120, *Sample Transmittal* with transmittal envelopes
  - 5. Log forms for recording test hole information
    - (Geology Program will provide forms upon request)
  - 6. Stakes / lathe for marking the test holes
  - 7. Weighted tape for measuring test hole depth / thicknesses

### Reference

| Documents: | WYDOT 106.3.3.3   | WYDOT Standard Specifications |
|------------|-------------------|-------------------------------|
|            | WYDOT 106.3.3.3.1 | WYDOT Standard Specifications |
|            | WYDOT T-120       | Sample Transmittal            |

Use: This procedure is intended to facilitate the requirements of 106.3.3.3.1, and intended to assist with the preparation of a sampling layout and the associated field investigation.

### Procedure:

### **Preliminary Work**

Prior to field work, several preparatory steps are recommended to ensure an efficient and thorough preliminary investigation of the proposed pit site.

- 1. Obtain an estimate of the desired quantities of material for the proposed project including what the material will be used for, for example hot plant mix (HPM), crushed base, subbase, borrow special excavation, etc.
- 2. Prepare a preliminary site map along with planned field test holes for the investigation. Any information collected regarding the geology of the area, landmarks, etc., should be included on the site map.

### **Field Investigation**

1. Conduct a surface inspection of the area to be investigated prior to any physical digging. This allows for an approximation of the total surface area and will also aid in determining the location, number of holes, and spacing between test holes. The number of test holes required will vary depending on the size of the area investigated and the amount of product to be produced.

As a guideline, between five and fifteen holes with spacing between 250 and 500 feet is adequate for a preliminary investigation. If possible, the

holes should be evenly spaced along the dimensions (length by width) of the site. However, if the thickness and quality of the gravel varies significantly, additional holes may be necessary.

- 2. There are several important factors to consider while digging and sampling the test hole:
  - a. Every effort should be made to keep the topsoil and overburden separate from the gravel in order to avoid contamination of the gravel. This is accomplished by placing the topsoil and overburden on one side of the backhoe hole while placing the gravel on the other. It is not necessary to collect topsoil, overburden or pit floor samples during the preliminary investigation. It is good practice to note the depth of these layers.
  - b. When the gravel layer is reached and sampling begins, it is important to obtain a sample(s) that is as representative as possible of the material being dug. Do not collect the sample from one specific depth of the hole but instead, obtain a sample representing the entire thickness of the gravel layer. The sample should include, if present, a representative percentage of any deleterious material present within the gravel layer such as silt/sand seams, caliche-coated rock, clay balls, etc. At least one gravel sample per hole, or 8-10 samples minimum for the entire investigation, is required to obtain an adequate amount of material for wear grade testing by the consultant. Referencing of gravel samples from one hole to the next is not recommended. A Sample Transmittal, Form T-120 and envelope, or similar, for the consultant should be filled out completely. Test hole and sample number along with vertical limits and proposed use for the material, should be considered as required minimums for submittal to consultant.
  - c. While digging and sampling the test hole, it is important to keep an accurate record or log of the material being dug. Precisely record the thickness of the topsoil, overburden, sand and gravel, and if encountered, depth to the pit floor. A brief description of topsoil, overburden and pit floor (for example sandy topsoil, clayey silt overburden, red shale pit floor) should be recorded, however a more complete description of the gravel layer is recommended. Information to be noted would include:
    - 1. Lenses or coatings of sand, silt, caliche, or clay within the gravel, and their thickness.
    - 2. The durability of the rock; is it a soft sandstone, or hard competent rock?
    - 3. Any cemented layers and the degree of cementation (slight, moderate, well).
    - 4. Depth to groundwater, if present.

- 5. Maximum size of rock and visual estimation of the percentages of plus 3 inch (oversize) and plus 1 inch rock.
- d. If and when the pit floor is reached, its depth should be recorded. At this point the test hole should be abandoned and backfilling begun.
- 3. Backfilling of the hole should be accomplished only after all the necessary samples have been collected and material thicknesses recorded. It is important to backfill the hole with the gravel first, and the topsoil and overburden last, to help reestablish vegetation. After backfilling is complete, the test hole should be marked with a lathe or stake (preferably both) labeled with the appropriate test hole number for surveying purposes, if necessary.
- 4. As the test holes are being dug, a rough sketch map should be drawn indicating approximate test hole locations and other prominent features of the site such as terrace edges, fence lines, roads, old depleted pit limits, utilities, etc. A hand held GPS unit is useful in creating these field maps, test holes and other recorded features can be easily transferred to topographic maps to create fairly accurate map of a pit site.
- 5. When the preliminary investigation has been completed, check to ensure that all of the samples have been completely and accurately identified and labeled, and then submit them to the Consultant for analysis with the suggested Form T-120. Estimate the total quantity of aggregate based on the dimensions of the pit and average gravel thickness to determine if adequate quantities are available for the project.

| $\sim$    |   | WYOMIN        | G DEPARTN    |   |                    |                       | Form T-120<br>(Rev. 09-16) |
|-----------|---|---------------|--------------|---|--------------------|-----------------------|----------------------------|
|           |   |               |              |   | ng Laboratory      |                       | (1207. 03-16)              |
|           | - And |               | SAMPL        | E IRA                                     | ANSIMITTAL         | -                     |                            |
| TRANSPOR  |   | Preliminar    | y 🔽 Ge       | ology                                     | 🔽 Con              | struction             | 🗖 QC/QA                    |
|           |   |               |              |   |                    |                       |                            |
| Projec    | t Number:                                 | ERP Number    | Ĩ            | <u></u> 8                                 | Lab                | #: <u>###</u>         |                            |
|           | Engineer:                                 | Resident En   | gineer       |   | А                  | t: Engineer's Tow     | n                          |
|           | Soils:                                    |               |              |   | Road Section       | n: As Per Plans       |                            |
| Pit       | or Source:                                | Name of Pit   | or Source    | or Source County: County of Pit or Source |                    | r Source              |                            |
| Date      | e Sampled:                                | ## / ## /     | ####         |   | Date Receive       | d: <u>## / ## /##</u> |                            |
|           |   |               | Sam          | ple Distri                                | bution             |                       |                            |
| F         | Aggregate                                 | 9             | Concrete     |   | 🗌 Chemistry        | Г                     | Geology                    |
|           |   |               |              |   |                    |                       | Multiple Samples           |
| Sample N  | Number(s):                                | -             |              |   | <b>S #:</b> 14     | TH #: 7               | of                         |
| Location  | (Belt, Stocl                              | kpile, etc.): |              | At  | :: (Sta., kp., M.P | ., etc.):             |                            |
| Verti     | cal Limits:                               | 6'            | ~            |   | То : 10            | ' 6"                  |                            |
| Horizor   | ntal Limits:                              |               |              |   | То :               |                       |                            |
| Qty. Re   | presented:                                |               |              |   |                    |                       |                            |
|           |   |               | F            | For Use A                                 | s:                 |                       |                            |
|           | Profile                                   |               | BSE          | PMP                                       | Type<br>, Grd.     | Conc. Coarse          | e Aggregate                |
|           | Borrow                                    | ~             | CB, Grd.     | RPM                                       | P                  | Conc. Med. A          | ggregate                   |
|           | Topping                                   |               | PMB          | PMW                                       | /С, Туре           | Conc. Fine A          | ggregate                   |
|           | Alkali                                    |               | СТВ          | ССА                                       | , Туре             | Conc. Cylind          | ers                        |
|           | Check Curve                               |               | Filler       | Main                                      | t. Туре            | Conc. Beams           | ;                          |
|           | Final Emb.                                |               | Drain Gra∨el | Chec                                      | k Design           | Port. Cement          | , Туре                     |
|           | Other                                     | c             |              |   |                    | Туре                  |                            |
|           |   |               | Geosynthetic | s (Geod                                   | arid/Geotexti      | le)                   |                            |
| Pro       | duct Name                                 | 2             |              |   | nufacturer         | ,                     |                            |
|           | Sand & Gr                                 |               |              | 3   | 1.                 |                       | 1                          |
| ixemarks. |   |               |              |   |                    |                       |                            |
|           |   |               |              |   |                    |                       |                            |
|           |   |               |              |   |                    |                       |                            |
|           |   |               |              |   |                    |                       |                            |
|           |   |               |              |   |                    |                       |                            |
| Submitted | зВу                                       | Field Sample  |              |   | Field Sc           | mpler's Signature     |                            |
|           |   |               | Printed Name |   |                    | Signatu               | re                         |

Signature

### CORRELATION BETWEEN AN AUTOMATIC SAMPLER AND A CONVEYOR BELT CUT

- Scope: This is a statistical procedure to determine whether a procedural or equipment bias exists in aggregate testing in samples obtained either with an automatic sampler or with a conveyor belt cut. This statistical procedure compares the aggregate gradations determined for samples collected with an automatic sampler to those obtained with a conveyor belt cut. An automatic sampler is a mechanical device that obtains a representative sample from a moving conveyor belt. Acceptable sampler types are those that collect the whole stream of material when in use. Paired t-tests are run on each sieve size on the aggregate gradations determined by the two sampling methods. This procedure determines whether one can be 99 percent confident that the two sampling methods are achieving different test results. This procedure will not detect minor differences between the sampling methods.
- Use: This procedure is used to determine if an automatic sampler is acceptable for obtaining aggregate samples for gradation tests. This procedure will be performed annually and after each move of the equipment and/or at the discretion of the engineer.

If any directional bias occurs or if the paired t-test indicates that the two sampling methods are achieving significantly different results, further evaluation of the correlation between the automatic sampler and conveyor belt cuts will be performed. "Directional bias" is considered to exist when all five tests are higher for one laboratory than for the other and the average difference on at least one sieve exceeds the Allowable Gradation Difference in Table 3 of WYDOT 126.0. If directional bias exists, consult Subsection 114.3.3, Correlation. Continue evaluation to find the cause of the directional bias. "Directional bias" does not exist when five tests are higher for one laboratory than for the other and the average gradation difference on all sieves is less than the Allowable Gradation Difference in Table 3 of WYDOT 126.0, or at least one test is less than or equal to the paired test of the other laboratory.

| Reference  |               |   |
|------------|---------------|---|
| Documents: | WYDOT 126.0   | Correlation of Aggregate Gradation Test Results |
|            | WYDOT 804.0   | Aggregate Sampling                              |
|            | WYDOT 814.0   | Sieve Analysis of Combined Aggregate            |
|            | WYDOT T-165AG | Correlation of Aggregate Gradations             |
|            |               | 0000  |

Procedure: Five sample pairs are taken by the contractor in the presence of a WYDOT technician. Label samples caught at the same time so they may be paired up during statistical analysis. Samples are taken from the automatic sampler and then off the conveyor belt after all aggregate splits have been combined and

WYDOT 124.0 (Rev. 10-18)

before the addition of any additives (lime, asphalt, cement, fly ash, etc.), and when the conveyor belts are running free and clear and at 80 percent or more of normal production capacity. After each automatic sample has been taken, the conveyor belt is immediately stopped so that the conveyor belt cut sample can be obtained in accordance with WYDOT 804.0.

Gradation tests are run on both samples by the contractor in accordance with procedure WYDOT 814.0. Gradation test will be performed by the same contractor technician using the same equipment since this procedure is used to detect differences due only to the different sampling methods.

Paired two tailed t-tests are performed separately for each sieve using an  $\alpha$  (alpha) with the level of significance of 0.01. The statistical method is the same as the one presented in WYDOT 126.0.

Calculations: The calculations are performed in the same manner as in WYDOT 126.0.

Report: The results are reported on Form T-165AG.

### CORRELATION OF AGGREGATE GRADATION TEST RESULTS

- Scope: This statistical procedure compares the aggregate gradations determined by two different laboratories. Paired t-tests are run on the aggregate gradations for each sieve size determined by the two laboratories. This procedure determines whether one can be 99 percent confident that the two laboratories are achieving different test results. Additional tests determine whether excessively large or small variability has caused a t-test to produce results that, though they are statistically correct, are practically wrong in the current situation. These tests combine to determine whether the two laboratories achieve results that are significantly different. This procedure will not detect minor differences between the two laboratories.
- Use: This procedure determines whether there is any substantial systematic bias between the aggregate gradations determined by the WYDOT field laboratory and by the contractor's laboratory. If the data generated by the WYDOT field laboratory and by the contractor's laboratory are found to be significantly different, then the dispute resolution procedure will be followed.

This procedure may be used for concrete aggregate or other aggregate sources. When the procedure is different for concrete aggregate, the differences are noted in this procedure.

The paired t-test determines if the differences in aggregate gradations are significantly different for each sieve size.

If any directional bias occurs or if the t-test indicates that the two laboratories are achieving significantly different results, further evaluation of the correlation between the laboratories will be performed.

If there is any change in testing personnel or equipment, the correlation process is repeated using production test results.

### Reference

| D (        |               |  |
|------------|---------------|--|
| Documents: | AASHTO T 27   | Standard Method of Test for Sieve Analysis of Fine and |
|            |               | Coarse Aggregate                                       |
|            | WYDOT 114.3.3 | WYDOT Standard Specifications                          |
|            | WYDOT 401     | WYDOT Standard Specifications                          |
|            | WYDOT 803     | WYDOT Standard Specifications                          |
|            | WYDOT 417.0   | Precision Statements for Comparing Contractor QA       |
|            |               | Results to WYDOT Verification Results                  |
|            | WYDOT 804.0   | Aggregate Sampling                                     |
|            | WYDOT 814.0   | Sieve Analysis of Combined Aggregate                   |
|            | WYDOT 816.0   | Sieve Analysis of Concrete Aggregate                   |
|            | WYDOT E-119   | Pay Adjustment for Density                             |
|            | WYDOT T-165AG | Correlation of Aggregate Gradations                    |
|            | WYDOT T-166   | Aggregate Analysis                                     |

### WYDOT 126.0 (Rev. 10-18) Procedure:

Fifteen aggregate samples are collected in groups of three according to WYDOT 405.0. During each of the five sampling events, the contractor will obtain three samples; one to be tested by the contractor, one by WYDOT, and one retained as a referee sample. The middle sample will be the referee sample when cutting samples from the conveyor belt. Label samples obtained at the same time so they may be compared up during statistical analysis. The WYDOT field laboratory will test five samples, the contractor's laboratory will test five samples, and five samples will be retained by WYDOT as referee samples.

Determine the percentage passing each sieve size for each aggregate sample according to WYDOT 814.0 (or WYDOT 816.0 for concrete aggregate). Report the test result pairs (percentages) on Form T-165AG passing each sieve to the nearest 0.1 percent as previously recorded on Form T-166 (Aggregate Analysis), Combined Aggregate, % Passing column item "to 0.1%".

Perform the correlation (first column on Form T-165AG) and specification sieves per the *WYDOT Standard Specifications*, Section 803 for which the minimum percent passing is less than 90 percent.

Perform two-tailed paired t-tests separately for each sieve using an " $\alpha$ " (alpha) level of significance of 0.01. If the standard deviation of the differences is less than the 1S standard deviation for multilaboratory precision in Table 1 of this section (adapted from AASHTO T 27, Table 2), use the 1S standard deviation for multilaboratory precision instead of the calculated standard deviation. Similarly, if the calculated standard deviation is greater than the D2S value in Table 1 of this section, use the D2S percent for multilaboratory precision instead of the calculated standard deviation.

When the sample is a Coarse Aggregate Test sample (only retained No. 4) use Coarse column of Table 1 of this section, when a Fine Aggregate Test sample (has only minus No. 4) use Fine column Table 1 of this section (adapted from AASHTO T 27, Table 3).

- Note: When evaluating gradation for acceptance in the CMS application, enter the gradation test result to the nearest tenth (0.1). This will allow the acceptance to be calculated with the correct significance level (whole number) and also allow verification comparisons. Results produced from CMS on form E-119 (Pay Adjustment for Density).
- Calculations: 1. Calculate the difference between the percent passing each sieve for each pair of samples. Use the following equation:

$$X_i - Y_i = Z_i$$
  
Difference = A<sub>i</sub> - B<sub>i</sub>

- Where: $X_i$  is the percentage passing for sample pair i for an individual sieve from the first data set (the Contractor's data); $Y_i$  is the percentage passing for sample pair i for an individual sieve from the second data set (WYDOT's data); $Z_i$  is the difference in percentage passing between paired samples for sample i for an individual sieve.
- On Form T-165AG;  $X_i$  is always Tester A (Contractor's data);  $Y_i$  is always Tester B (WYDOT's data);  $Z_i$  is Tester Difference (A – B);
  - Note: It is important to record whether the difference is positive or negative to determine bias.
- 2. Calculate the mean of the differences between paired samples. Use the following equation:

$$\overline{Z} = \left(\frac{1}{n}\right) \sum_{i=1}^{n} Z_i = Difference$$

- Where: $\bar{Z}$  is the mean difference in percentages passing an<br/>individual sieve for paired samples. The mean difference<br/>considers the absolute difference and negates the positive<br/>or negativity of the number.<br/>n is the number of paired samples, usually five<br/>as per WYDOT Standard Specifications 114.3.3.2<br/>Subcategory 1;
- On Form T-165AG; (Tester A + Tester B  $\div$  Number of samples) in the Avg. column, usually ten samples;  $\overline{Z}$  is the Average difference Percent Passing for pairs on each control sieve;
- 3. Calculate the sample standard deviation of the differences in percentage passing an individual sieve. This is done using the sample standard deviation function on a calculator or spreadsheet according to the following equation:

$$s = \sqrt{\left(\frac{1}{n-1}\right)\sum_{i=1}^{n} \left(Z_i - \overline{Z}\right)^2}$$

Where: s is the sample standard deviation<sup>1</sup> of the differences in percentage passing an individual sieve.

On Form T-165AG; *s* is Std Dev on the Difference Row

### Paired t-test

- 4. Determine the appropriate standard deviation to be used to calculate the ttest statistic for each sieve size as follows:
  - a. Calculate the average percentage retained on each sieve by subtracting the average percentage passing the next highest sieve from the average percentage passing the sieve in question.

The average percent retained is the average of the two results being checked for correlation.

% passing =  $100.0 - \sum \overline{Z} = \%$  retained difference

% passing is 100.0 minus the sum of the averaged tests = difference of % retained

On Form T-165AG; in the Avg column,  $\overline{Z}$  (from Step 2); numerical results are recorded below the Sieve Size being tested in the row difference and column, Control Sieve Sizes & Avg % Retained;

b. Table 1 of this section (adapted from AASHTO T 27, Table 2) contains the minimum and maximum allowable standard deviations used to calculate the t-test statistic. Use the Coarse values unless the nominal maximum aggregate size is No. 4 or less, in which case, use the Fine values. If the calculated standard deviation is less than the minimum value from Table 1 for the  $t_{crit}$  calculation, use the minimum value from Table 1. If the calculated standard deviation is between the minimum and maximum values in Table 1, use the calculated standard deviation for the  $t_{crit}$  calculation. If the calculated standard deviation is greater than the maximum value from Table 1, use the maximum value from Table 1 for the  $t_{crit}$  calculation.

<sup>&</sup>lt;sup>1</sup> On most calculators and spreadsheets there are two standard deviations, a population standard deviation and a sample standard deviation. Use the sample standard deviation. To use a calculator, first calculate and record the differences,  $Z_i$ . Then calculate the standard deviation of these differences.

| Percent             | Coa     | arse    | Fine    |         |  |
|---------------------|---------|---------|---------|---------|--|
| Retained            | Minimum | Maximum | Minimum | Maximum |  |
| Ketaineu            | (1S)    | (D2S)   | (1S)    | (D2S)   |  |
| < 3%                | 0.39    | 3.00    | 0.21    | 0.60    |  |
| $\geq$ 3% to <10%   | 1.06    | 3.00    | 0.57    | 1.60    |  |
| $\geq 10\%$ to <20% | 1.66    | 4.70    | 0.95    | 2.70    |  |
| $\geq$ 20% to < 30% | 2.01    | 5.70    | 1.24    | 3.50    |  |
| $\geq$ 30% to <40%  | 2.44    | 6.90    | 1.41    | 4.00    |  |
| ≥ 40%               | 3.18    | 9.00    | 1.41    | 5.20    |  |

**<u>Table 1.</u>** Allowable Range of Standard Deviations

5. Calculate the t-test statistic using the following equation:

$$t = \frac{\left|\overline{Z}\right|}{\sqrt{\frac{s^2}{n}}}$$

Where: t is the t-test statistic;  $|\overline{Z}|$  is the absolute value of the mean of the differences from Step 2; s is standard deviation determined in Step 4;

On Form T-165AG; determined "s" standard deviation is recorded under column "Max SD" for the maximum and under column "Min SD" for the minimum;

> determined "t" t-test statistic is recorded under column " t<sub>crit</sub>" "4.604" "t";

- 6. If t is less than the critical t value<sup>2</sup>,  $t_{crit} = 4.604$ , then the t-test does not indicate a significant difference between the first and second data sets. If t is greater than 4.604 then one can be 99 percent confident that the two data sets are different and that there is a systematic difference between the two testing facilities.
- 7. Evaluate for directional bias. "Directional bias" is considered to exist when all five tests are higher for one laboratory than for the other and the average difference on at least one sieve exceeds the Allowable Gradation Difference in Table 3. If directional bias exists, consult Subsection 114.3.3, Correlation. Continue evaluation to find the cause of the

<sup>&</sup>lt;sup>2</sup> If a different number of samples than five pairs are correlated, a different  $t_{crit}$  must be selected. A two-tailed t-test statistic must be selected for the appropriate degrees of freedom. For four pairs,  $t_{crit}$  is 5.841; for six pairs  $t_{crit}$  is 4.032; for seven pairs  $t_{crit}$  is 3.707; for eight 8 pairs  $t_{crit}$  is 3.499; for nine pairs  $t_{crit}$  is 3.355; for ten pairs  $t_{crit}$  is 3.250. The WYDOT Materials Program or a standard statistics textbook may be consulted for assistance.

directional bias. "Directional bias" does not exist when five tests are higher for one laboratory than for the other and the average gradation difference on all sieves is less than the Allowable Gradation Difference in Table 3, or at least one test is less than or equal to the paired test of the other laboratory.

|                                  |        |                                  |                                  | l Maximum S                      |      |          |
|----------------------------------|--------|----------------------------------|----------------------------------|----------------------------------|------|----------|
|                                  | 1 inch | <sup>3</sup> / <sub>4</sub> inch | <sup>1</sup> / <sub>2</sub> inch | <sup>3</sup> / <sub>8</sub> inch | PMWC | Concrete |
| Sieve                            |        |                                  |                                  | Difference<br>ssing)             |      |          |
| 1 ¼ inch                         | 1.5    |                                  |                                  |                                  |      | 1.5      |
| 1 inch                           | 2.0    | 1.5                              |                                  |                                  |      | 2.0      |
| <sup>3</sup> / <sub>4</sub> inch | 3.0    | 2.0                              | 1.5                              |                                  |      | 3.0      |
| <sup>1</sup> / <sub>2</sub> inch | 3.4    | 3.0                              | 2.0                              | 1.5                              | 1.5  | 3.4      |
| <sup>3</sup> / <sub>8</sub> inch | 3.4    | 3.4                              | 3.4                              | 2.0                              | 2.0  | 3.4      |
| No. 4                            | 3.4    | 3.4                              | 3.4                              | 3.4                              | 3.4  | 3.4      |
| No. 8                            | 3.3    | 3.3                              | 3.3                              | 3.3                              | 3.3  | 3.3      |
| No. 16                           |        |                                  |                                  |                                  |      | 3.3      |
| No. 30                           | 2.9    | 2.9                              | 2.9                              | 2.9                              |      |          |
| No. 50                           |        |                                  |                                  |                                  |      | 2.9      |
| No. 100                          |        |                                  |                                  |                                  |      | 2.9      |
| No. 200                          | 1.2    | 1.2                              | 1.2                              | 1.2                              | 1.2  | 1.2      |

### Table 3. Allowable Gradation Difference

- Example: 1. Data in Table 2 of this section is used to perform example calculations. It represents the percentage passing a particular sieve. This procedure must be used for each sieve size in the specification.
  - 2. Record the five percentages passing for the first (Contractor) and second (WYDOT) data sets.
  - 3. Calculate the mean and standard deviation of these differences.

| % Pass N | ext Large     | est Sieve     | % F           | Ret Sieve             | e Analyzed |
|----------|---------------|---------------|---------------|-----------------------|------------|
|          | Data<br>Set 1 | Data<br>Set 2 | Data<br>Set 1 | Data<br>Set 2         | Difference |
|          | 78.6          | 79.2          | 56.3          | 58.9                  | -2.6       |
|          | 79.0          | 78.9          | 55.4          | 58.0                  | -2.6       |
|          | 77.2          | 76.5          | 55.0          | 59.5                  | -4.5       |
|          | 81.2          | 79.9          | 60.4          | 60.2                  | 0.2        |
|          | 81.0          | 80.5          | 59.8          | 62.3                  | -2.5       |
| Average  | 79.4          | 79.0          | 57.4          | 59.8                  | -2.40      |
|          |               |               |               | Standard<br>Deviation | 1.68       |

 Table 2: Example Data

- 4. Select the appropriate *s* for calculating the t-test statistic.
  - a. The percentage retained on the sieve in question must be determined.
  - b. From Table 2;
    - 1. The average percentage passing the next largest sieve is (79.4 + 79.0) / 2 = 79.2%.
    - 2. The average percentage retained on the sieve in question is (57.4 + 59.8) / 2 = 58.6%.
    - 3. Therefore, the average percent retained on the sieve in question is 79.2 58.6 = 20.6%.
  - c. From Table 1, assuming the nominal maximum aggregate size is greater than No. 4, the minimum standard deviation is 2.01% and the maximum is 5.70%.
  - d. Since the calculated standard deviation of 1.68% is less than the minimum standard deviation, use the minimum standard deviation of 2.01%.
- 5. Calculate the t-test statistic.

$$t = \frac{|\overline{Z}|}{\sqrt{\frac{s^2}{n}}} = \frac{|-2.40|}{\sqrt{\frac{2.01^2}{5}}} = 2.670$$

- 6. The t-test statistic is 2.670. The critical t value is 4.604. Since the test statistic is less than the critical value, conclude that the two data sets are not significantly different. This means that one cannot be 99 percent certain that the two data sets are significantly different since the level of significance,  $\alpha$ , is 0.01.
- 7. For four of the paired data points, the values from data set 2 are higher. Since for one of the paired data points the value from data set 1 is higher, no directional bias exists.



### WYOMING DEPARTMENT OF TRANSPORTATION

**Correlation of Aggregate Gradations** 

Report Date: 08/22/2018

| Tester A: Mark Johnson          | Organization A: WYDOT       | Test is to Correlate |
|---------------------------------|-----------------------------|----------------------|
| Tester B: Frankie Adams         | Organization B: Croell, Inc | Testers              |
| Testing Date: <u>7/16/2018</u>  | Contractor: Croell, Inc.    | O Mechanical Sampler |
| dent Engineer: Steve Cook, P.E. |                             |                      |

| Control Sieve Sizes<br>Avg Retained | Tester     | Percents Passing |        |        |        |        | Avg   | Std  | Max  | Min<br>SD | Tont    | Pass/<br>Fail | Bias |
|-------------------------------------|------------|------------------|--------|--------|--------|--------|-------|------|------|-----------|---------|---------------|------|
|                                     |            | Pair A           | Pair B | Pair C | Pair D | Pair E |       | Dev  | SD   | SD        |         | Fail          |      |
| 1/2" (12.5 mm)                      | A          | 94.8             | 96.5   | 93.3   | 94.4   | 93.1   |       |      |      |           |         | -             | 1    |
|                                     | В          | 94.6             | 94.6   | 93.5   | 94.2   | 94.2   | 94.3  |      |      | _         |         |               |      |
| 5.7                                 | Difference | 0.2              | 1.9    | -0.2   | 0.2    | ~1.1   | 0.20  | 1.09 | 3.00 | 1.06      | 0.411   | Pass          | NC   |
| 3/8" (9.50 mm)                      | A          | 76.5             | 79.8   | 76.5   | 75.0   | 75.9   |       |      |      |           |         |               |      |
|                                     | В          | 76.7             | 76.2   | 74.8   | 76.0   | 75.7   | 76.3  |      | -    |           | diam'r. | 1             |      |
| 18.0                                | Difference | -0.2             | 3.6    | 1.7    | -1.0   | 0.2    | 0.86  | 1.82 | 4.70 | 1.66      | 1.057   | Pass          | N    |
| No. 4 (4.75 mm)                     | A          | 44.4             | 48.3   | 44.3   | 43.6   | 42.7   | 1.44  |      |      |           | -       | -             |      |
|                                     | В          | 43.7             | 42.9   | 44.3   | 43.4   | 43.2   | 44.1  |      |      |           |         | 10.00         |      |
| 32.2                                | Difference | 0.7              | 5.4    | 0.0    | 0.2    | -0,5   | 1.16  | 2.41 | 6.90 | 2.44      | 1.063   | Pass          | N    |
| No. 8 (2.36 mm)                     | A          | 31.1             | 32.5   | 28.8   | 29.3   | 27.8   |       |      |      |           |         |               | 1    |
|                                     | В          | 29.5             | 29.6   | 29.9   | 27.5   | 27.3   | 29.3  |      |      |           |         |               |      |
| 14.8                                | Difference | 1.6              | 2.9    | -1.1   | 1.8    | 0.5    | 1.14  | 1.51 | 4.70 | 1.66      | 1.536   | Pass          | Ň    |
| No. 30 (600 µm)                     | A          | 17.5             | 16.7   | 13.9   | 14.8   | 13.9   |       |      | -    |           |         | 100.00        | 1    |
|                                     | В          | 16.4             | 15.4   | 15.2   | 13.1   | 12.8   | 15.0  | _    |      |           |         |               |      |
| 14.4                                | Difference | 1.1              | 1.3    | -1.3   | 1.7    | 1.1    | 0.78  | 1.19 | 4.70 | 1.66      | 1.051   | Pass          | N    |
| No. 200 (75 µm)                     | A          | 6.4              | 5.6    | 4,3    | 5.5    | 5.2    |       |      | -    |           |         |               |      |
|                                     | В          | 6.2              | 5,0    | 5.0    | 4.8    | 4.3    | - 5.2 |      |      |           |         | 1.11          |      |
| 9.7                                 | Difference | 0.2              | 0.6    | -0.7   | 0.7    | 0.9    | 0.35  | 0.62 | 3,00 | 1.06      | 0,730   | Pass          | N    |

Directional Bias on Any Sieve: NO Which One(s): \_\_\_\_

Comments: For Correlation purposes only. Samples tested did not come from production, but rather from calibrating the Automatic Sampler

WYDOT 126.0 (Rev. 10-18)



## MATERIALS TESTING LABORATORY Plant Mix Pavement Density Pay Factors

E-119 (Rev. 05-17

| Engineer: 5                         | STEVE GOOK PE                 |         |                |                            | 0.01        | CA 11-11-1       |  |  |
|-------------------------------------|-------------------------------|---------|----------------|----------------------------|-------------|------------------|--|--|
|                                     |                               |         |                | Method                     |             | CQA Method       |  |  |
| NYDOT Tester M<br>ntractor Tester F | partition and an and a second |         |                | MTC Number:<br>MTC Number: | 2.3.7       |                  |  |  |
| intractor rester -                  | Tankie Adams                  |         |                | wije wumber.               | 0//         | 1                |  |  |
| Lot #:                              | 2                             |         |                | Voidless Uni               | Weight: 162 | .1               |  |  |
|                                     |                               |         |                | Use Tes                    | ts From: 🔽  | Contractor Wydot |  |  |
| 1                                   | Contractor                    | % Max   | WYDOT          | % Max                      |             | 7                |  |  |
| Test Number                         | Density lbs/cf                | Density | Density lbs/cf | Density                    | Verified    |                  |  |  |
| 1                                   | 152.4                         | 94.04   |                | 1.1.1                      | No          |                  |  |  |
| 2                                   | 152.3                         | 93.92   |                | 1                          | No          |                  |  |  |
| 3                                   | 150.2                         | 92.65   | 148.7          | 91.75                      | YES         |                  |  |  |
| 4                                   | 151.7                         | 93.56   |                |                            | No          |                  |  |  |
| 5                                   | 152.7                         | 94.18   |                |                            | No          |                  |  |  |
| 6                                   | 150.2                         | 92.65   |                |                            | No          |                  |  |  |
| 7                                   | 149.9                         | 92.48   | 1              |                            | No          |                  |  |  |
|                                     | Average                       | 93.35   |                |                            |             |                  |  |  |
|                                     | Std Deviation                 | 0.74    |                |                            |             |                  |  |  |
|                                     | Pay Factor                    | 1.00    |                |                            |             |                  |  |  |
|                                     | Override                      |         |                |                            |             |                  |  |  |
|                                     | Overnde                       |         |                |                            |             |                  |  |  |
| Item Number Project                 |                               | ct      | Quantity       | Unit Price                 | Pay Adj     | ustment          |  |  |
| 401.03310 NHPPI-I80                 |                               | 04261   | 1,500.00       | \$31.75                    | \$0.        | .00              |  |  |
|                                     |                               |         |                |                            |             |                  |  |  |

### ASSESSMENT OF FIELD LABS PERFORMING MIX VOLUMETRIC QUALITY ACCEPTANCE TESTING

- Scope: This procedure is intended to provide general guidance for assessing the competency of non-AASHTO accredited laboratories and personnel performing field testing of production mix volumetrics for quality acceptance.
- Use: This procedure should be used to assess competencies of field laboratories and personnel engaged in volumetric testing of production samples of mix for quality acceptance purposes and establish correlation of the field laboratory to the AASHTO accredited mix design facility. Assessment of field laboratories and personnel will be performed at the frequency stated in the contract documents or once per construction season, whichever is greater.

ReferenceDocuments:WYDOT Current Edition<br/>WYDOT 416.0WYDOT Standard Specifications<br/>Precision Statements for Comparing Mix Design and<br/>Aggregate Property Test Results<br/>Precision Statements for Comparing Contractor QA<br/>Results to WYDOT Verification Results

- Procedure: The engineer may visit the field laboratory to verify the following is maintained and available on-site:
  - 1. Copies of relevant contract documents, including contract plans and associated specifications, JMF, mix design, etc.
  - 2. Safety equipment is in good condition
  - 3. Copies of current WYDOT Standard Specifications and WYDOT Materials Testing Manual
  - 4. Copies of the current applicable test procedures
  - 5. The appropriate equipment to perform the required tests
  - 6. The equipment is serviced and calibrated as required, documentation of such is on file, and calibration/service decals are affixed to all testing equipment

Obtain a sample of plant produced mix, mix from the project where the field laboratory is intended to be used is preferred, of sufficient size. The quantity must be large enough that when the sample is split in half, there is enough quantity of mix in each half to determine the following: air voids, voids in mineral aggregate, voids filled with asphalt (for Superpave mixes only), voidless unit weight, stability & flow (Marshall mixes only), extracted asphalt content, extracted gradation, dust-to-effective asphalt content, and film thickness.

One half of the original sample will be tested by the field laboratory and the other half will be tested by an AASHTO accredited laboratory for the fore-mentioned properties.

The results from each laboratory will be compared by the engineer using the criteria in WYDOT 416.0 and WYDOT 417.0. If the results are within the allowable limits (ie, correlate), the field laboratory and associated personnel are approved to perform field mix volumetric acceptance testing for the remainder of the construction season on WYDOT projects.

If any of the results are not within the allowable limits, the field laboratory and the accredited laboratory must resolve the discrepancy(s) (additional mix testing may be necessary) and document the resolution of the discrepancy(s). If the resolution is acceptable to the engineer, the field laboratory and associated personnel are approved to perform field mix volumetric acceptance testing for the remainder of the construction season on WYDOT projects.

### **MISCELLANEOUS ITEMS - SAMPLE SIZE**

Scope: This section lists miscellaneous items used on construction projects. Sections pertaining to a specific item's sample size are listed in the section(s) of the WYDOT Materials Testing Manual pertaining to the particular item.

Use: The following table lists the minimum sample size required for many of the miscellaneous materials used on WYDOT construction projects.

| Reinforcing Steel  | Minimum two pieces, 54 inch in length   |
|--|---|
| Epoxy Coated Reinforcing Steel   | Minimum two pieces, 54 inch in length   |
| Spiral Steel   | Minimum two 54 inch straight pieces   |
| Welded Wire Fabric   | 12 inch x 24 inch   |
| Barbed Wire  | 48 inch length  |
| Barbless Wire  | 48 inch length  |
| Woven Wire   | 24 inch x height of wire  |
| V-Mesh/Gabion Fabric   | 24 inch x height of fabric  |
| Industrial Fence<br>Fabric<br>Tension Wire<br>Line Post<br>End/Corner Post | <ul><li>12 inch x height of fabric</li><li>48 inch length</li><li>24 inch length</li><li>24 inch length</li></ul> |
| Expansion Joint Material   | 4 inch x 12 inch  |
| Geotextile Fabrics   | 72 inch x width of roll   |
| Geogrid  | 2 feet x 2 feet with 1 factory edge   |
| Geocell  | 72 inch x width of roll   |
| Rip Rap Aggregate  | Minimum two each, 2 lb samples  |
| Paint  | 1 qt - if not pretested   |
| Water  | 1 qt glass or Nalgene container   |

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### **SOIL BEHAVIOR**

Particle Shapes

- 1. Angular particles tend to interlock
- 2. Rounded particles tend to shift and slide

Strength and Stability of Soils (ability to support loads)

- 1. Determination of strength:
  - a. Stabilometer Test, "R" value
  - b. California Bearing Ratio, CBR
  - c. Resilient Modulus, M<sub>R</sub>
- 2. What gives strength to soils:
  - a. Compaction:
    - 1. In general, the heavier the unit density, the greater the strength
    - 2. In general, reducing the voids, the greater the strength
  - b. Granular soils:
    - 1. Internal friction resistance
    - 2. The "safe slope" of a granular fill remains the same, regardless of the height
  - c. Cohesive soils (clays):
    - 1. No internal friction
    - 2. Resists shearing only by cohesive or molecular strength
    - 3. The "safe slope" of clay fill becomes flatter as the fill becomes higher

### Compaction and Optimum Moisture

- 1. Undercompacted soils:
  - a. Support less load
  - b. Increase frost action
  - c. Settle, swell, and absorb water
- 2. Factors necessary for good compaction:
  - a. Optimum moisture
  - b. Moisture, well mixed (soil-cured)
  - c. Rolling (speed, weight and number of passes)
  - d. Lift thickness (thinner for clays)

### Capillarity

- 1. Types of water in soils:
  - a. Free water drains away if no frost is present
  - b. Capillary water:
    - 1. Resists gravity
    - 2. Held to soil particles by surface tension

- 2. Capillary action in different soils:
  - a. Coarse gravel: no capillary action
  - b. Coarse sand: up to 12 inch
  - c. Fine sand: up to 3 ft
  - d. Clay:
    - 1. Low (because of imperviousness)

### Frost Action

- 1. Soils high in capillary action are high in frost action
- 2. Most damage is at the time of thawing
- 3. Prevention of frost damage:
  - a. Minus No. 200 material should be at a minimum in base and sub-base materials (10% generally resists frost)
  - b. 95 to 100% compaction of embankment (to reduce capillary action)
  - c. Liquid limit of less than 25 generally prevents frost

### Swell

- 1. Usually fine textured with high clay concentrations
- 2. Compact and keep close to optimum moisture to minimize swell; moisture needs to be uniform may be difficult achieve
- 3. Excessive swell may require remediation recommendations from the Geology Program

### MOISTURE - DENSITY METHOD SELECTION AND BORROW MOISTURE TEST

Scope: This procedure is used to determine the method to be used to determine moisturedensity relations of soils by determining the percentage of rock in an individual sample.

In addition, this procedure is also used to determine the approximate gallons of water that will be added per cubic yard to excavation material to obtain working moisture in the embankment. Usually water will be added by prewetting of a cut or borrow area prior to excavation.

### Apparatus: 1. Shovel

- 2. Pan 15 inch square or diameter, suggested
- 3. Rammer and guide, 5<sup>1</sup>/<sub>2</sub> lb, *See Appendix A, WYDOT 213.0 for tolerances*
- 4. Drying stove
- 5. Moisture tins
- 6. Trowel
- 7. Steel straightedge, 15 inch length minimum
- 8. No. 4 screen
- 9. Wooden block, suggest 2 inch x 4 inch
- 10.  $0.03 \text{ ft}^3 [0.001 \text{ m}^3] \text{ mold},$ 
  - See Appendices A & B, WYDOT 213.0 for tolerances.
- 11. Compaction block, 300 lb minimum
- 12. Extruder
- 13. Gram scale, sensitive to 0.1 g
- 14. 35 lb [15 kg] scale sensitive to 0.01 lb [5 g]
- 15. 100 ml graduated cylinder

### Reference

| "A"  |
|------|
| "С"  |
|      |
| et ( |
|      |
|      |

\* Note: Use of weekly reports is optional

- Sample: Representative samples of the soil and in-place moisture should be taken prior to the addition of water. Samples of material, weighing 45 lb each, are needed to run WYDOT 213.0 Method "A" or WYDOT 214.0 Method "C", four point curves.
  - Note: Install compaction block on solid foundation, such as outside on a prepared level surface.

Procedure: Before screening, the entire sample, the mass (weight) is recorded on Form T-112 as item "I". (See example Form T-112, *Soils Compaction Worksheet*, of this section.)

Note: The No. 4 screen will not be used on any specification testing.

Screen a full sack of the material over the No. 4 screen to determine the percent rock in the sample.

After screening, the mass (weight) of the rock, the plus No. 4, is determined and recorded as item "J" on Form T-112.

Note: Coarse is defined as material retained on the No. 4 screen. For this procedure, percent rock is used to describe the percent of coarse material in a sample.

The % of rock, item "K" is calculated by dividing item "J" by item "I" on Form T-112.

% Rock = 
$$\frac{\text{mass of retained rock, g}}{\text{mass of sample, g}} X 100$$

- 1. A sample containing 0% to 15% rock will be run as outlined in WYDOT 213.0 Method "A".
- 2. A sample with 15% to 40% rock will be run as outlined in WYDOT 214.0 Method "C".

Determine the moisture content (Roadway) (on Form T-112) by taking a representative moisture sample of not less than 100 g for Method "A" or not less than 500 g for Method "C."

- a. Determine the empty weight of a moisture tin and record as item "N" on Form T-112.
- b. Place the moisture sample in the moisture tin and record the mass (weight) as item "L" on Form T-112.
- c. Dry the moisture sample to a constant mass and let cool.
- d. Record the mass (weight) of the dry soil and tin as item "M" on Form T-112.

e. Determine the mass of Water, item "P" by subtracting the dry weight and tin, item "M" from the wet weight and tin, item "L" on Form T-112.

$$P = M - L$$

f. Determine the mass of dry soil, item "Q" by subtracting the tare of the tin, item "N" from the dry soil and tin, item "M" on Form T-112.

$$\mathbf{Q} = \mathbf{M} - \mathbf{N}$$

g. Determine the % Moisture, item "R" by dividing the mass of Water, item "P" by the mass of dry soil, item "Q" and multiplying by 100.

$$R = \frac{P}{0} \times 100$$

The Example Form T-112 of this section was determined by Method "A" (WYDOT 213.0) and is for informational purposes.

Computations:

- 1. Using Form T-140, *Plotting Worksheet*, (example follows in this section) plot the dry density and moisture content for each cylinder and record on Form T-112.
- 2. Compute the minimum moisture and plot on Form T-140 dry density curve.
  - Minimum moisture = The plotted maximum Dry Density x 0.93. This is plotted on a "French" curve in lb per  $ft^3$  on the example Form T-140 and the moisture is read directly for this point.

EXAMPLE: Minimum Moisture:

Plotted maximum Dry Density x 0.93 (for 93% compaction)

 $119.0 \text{ lb/ft}^3 \text{ x } 0.93 = 113.1 \text{ lb/ft}^3$ 

113.1 lb/ft<sup>3</sup> plotted on the curve has a minimum moisture of 8.5%

3. Compute Working Moisture.

Working Moisture = $\frac{\text{Minimum moisture + Optimum moisture}}{2}$ Minimum Moisture = 8.5%<br/>Optimum Moisture = 12.2%EXAMPLE: $\frac{8.5\% + 12.2\%}{2} = \frac{20.7\%}{2} = 10.4\%$  Working MoistureNote:Working Moisture should not be used if it falls more than 4<br/>points below optimum.

Optimum Moisture = 12.2% Working Moisture = 10.4%

EXAMPLE: 12.2% - 10.4% = 1.8% below optimum.

4. Compute additional moisture required.

Additional moisture required = Working moisture - Field moisture

Working Moisture = 10.4% Field Moisture = 5.7%

10.4% - 5.7% = 4.7% additional moisture required

Field Moisture is calculated as item R on Form T-112

On Form T-112 the plotted Optimum Moisture % is item "GG", plotted Max Dry Density is item "HH" and Roadway Moisture  $\% \pm$  Optimum is recorded directly above the remarks section.

5. Convert "Additional Moisture Required" from percent to gallons, using the "Embankment Moisture Conversion Table" of this section.

For 119.0  $lb/ft^3$ , with 4.7% additional moisture required is 18.1 gal/yd<sup>3</sup>, interpolating between 4% and 5%.

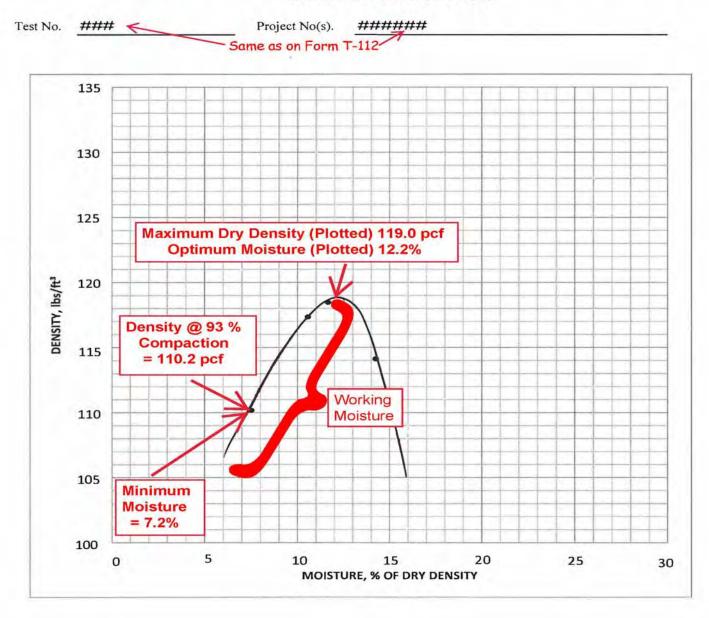
Report: Report weekly result on optional Form T-113 *Weekly Report for Compaction of: Embankment.* See example Form T-113 in WYDOT 213.0.

# WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SOIL COMPACTION WORKSHEET

**T-112** (Rev. 09-16)

| Project No(s).: ERP Number<br>Submitted By: Resident Engineer |  |                    |                |  | Station Sampled: 0+00<br>At: Resdient's town |                               |   |                                       |                        | ,                 |                    |              |
|---|--|--------------------|----------------|--|--|-------------------------------|---|---------------------------------------|------------------------|-------------------|--------------------|--------------|
| Depth Taken: 3 ft.  |  |                    |                |  | Ver  | Vertical Limits: 2 ft - 8 ft. |   |                                       |                        |                   |                    |              |
| Section Represented: Sta. 0+00 To Sta. 0+00                   |  |                    |                |  |  | County: Any County            |   |                                       |                        |                   |                    |              |
| See   |  | pled: ##/#         |                | DAL OF LEVEL   |  | Da                            |   |                                       | ##/##/#                | HHH               |                    |              |
|   | Date Sam   |                    |                | The Part of the  |  |                               | ic Re                                   |                                       |                        |                   |                    |              |
|   |  |                    | Т              | est was made   |  | Same                          | _                                       | $-^{day(s)}$                          | after fill was         | placed.           |                    | 1            |
| A   | Density of Sta   | undard Sand, Ib    | /ft³           |  | 96.4   |                               | Moisture Content (Roadway) Wt. of Water |                                       |                        |                   |                    | Wt.<br>Dry S |
| -   | 201  |                    |                |  |  |                               |   | Soil and<br>Fin, g                    | Dry Soil and<br>Tin, g | Tare of           | L - M, g           | M - N        |
| В   | Wt. of Appar   | atus and Sand,     | lb             |  | 17.28  |                               | L                                       | 651.8                                 | M 630.9                | Tin, g<br>N 263.9 | P 20.9             | Q            |
| С   | Wt. of Appar   | atus and Unuse     | d Sand, lb     | 1 .  | 8.76   |                               | R                                       | % Moi                                 | sture, (P/Q) x         | 100               |                    | 5.7          |
| D   | Sand Used (B   | - C), lb           |                |  | 8.52   |                               | 1                                       |                                       |                        |                   |                    |              |
| Е   |  | o Fill Funnel, lk  | ,              |  | 3.54   | 0                             | s                                       | Wet De                                | ensity, lb/ft³ ( (A    | x (* I)) / F      |                    | 102          |
| F   | The state of the s | Iole (D - E), lb   |                |  | 4.98   |                               | 1                                       | -                                     | % - 15% Rock,          |                   | (J/3))             | 152          |
|   | 1  | -/, -M             |                |  |  | Check %                       | F                                       | -                                     | 5% - 40% Rocl          |                   |                    | 1            |
| G   | Wt. of Soil. R   | ock and Contai     | ner, lb        |  | 6.15   | 11-0-50                       |   |                                       |                        |                   |                    |              |
| н   | Tare Wt. of C  |                    |                |  | 0.65   |                               | Т                                       |                                       | Drv                    | Density lb/ft³    | i                  | 1            |
| I   |  | Rock (G - H), lb   |                | 7  | 5.50   | 0                             | -                                       |                                       |                        | (100 + R)         |                    | 100          |
|   | Tour an unit of the  |                    |                |  |  |                               | -                                       | ** For                                | 0% - 15% Roci          |                   | + (K/3))           |              |
| J   | Wt. of Rock (  | Retained on No     | . 4), lb       |  | 0.68   |                               | ~                                       | • • • • • • • • • • • • • • • • • • • | (K/3) is to near       |                   |                    | 1.0          |
| к   | % of Rock, (J  |                    |                |  | 12.4   |                               |   |                                       | 15% - 40% Ro           |                   |                    |              |
| v   | Wet Wt. of Se  | oil and Mold, lb   |                |  |  | 14.08                         | 1                                       | 4.46                                  | 14.54                  | 14.48             |                    |              |
| w   | Tare Wt. of M  |                    |                |  |  | 10.14                         | -                                       | 10.14                                 | 10.14                  | 10.14             |                    |              |
| Y   | Wet Wt. of Soil in 1/30 ft <sup>3</sup> Mold (V - W), lb   |                    |                |  |  | 3.94                          | -                                       | 4.32                                  | 4.40                   | 4.34              |                    | -            |
| Z   |  | of Soil, lb/ft³, Y |                | ,  |  | 118.2                         | -                                       | 29.6                                  | 132.0                  | 130.2             |                    | -            |
| 1   | 1  |                    | ty of Soil, lb | √∰ <sup>3</sup>  |  |                               |   |                                       |                        |                   | -                  |              |
|   |  |                    | x 100          |  | 10 mil                                       | 110.2                         | 1                                       | 17.4                                  | 118.4                  | 114.1             |                    |              |
|   | (100   | + (AA or BB or     |                | or EE or FF))  | -  |                               |   |                                       |                        |                   |                    | · · · · · ·  |
|   |  |                    |                |  |  |                               | 1                                       | _                                     | 1                      |                   | -                  |              |
| м   | L  | м                  | N              | Р  | Q  |                               |   |                                       | % Moistur<br>10        |                   |                    |              |
| o<br>i  |  |                    |                | Wt. of   | Wt. of                                       |                               |   |                                       |                        |                   |                    |              |
| s   |  | Dry Soil and       | Tare of        | Water L  | Dry Soil                                     |                               |   |                                       |                        |                   |                    |              |
| t<br>u  | Tin, g   | Tin, g             | Tin, g         | - M, g   | M - N, g                                     |                               |   |                                       |                        |                   |                    |              |
| r<br>e  | 683.7  | 658.5              | 310.4          | 25.2   | 348.1  | 7.2                           |   |                                       |                        |                   |                    |              |
| с   | 493.5  | 471.9              | 264.1          | 21.6   | 207.8  | AA                            | 1                                       | 10.4                                  |                        |                   |                    |              |
| o<br>n  | 609.1  | 578.3              | 310.7          | 30.8   | 267.6  |                               | 1                                       | BB                                    | 11.5                   |                   |                    |              |
| n<br>t  | 492.2  | 464.0              | 264.1          | 28.2   | 199.9  | 9                             |   |                                       | CC                     | 14.1              |                    |              |
| e<br>n  |  |                    | 1271.25        |  |  |                               |   |                                       |                        | DD                | 1.1.1.1.1          | -            |
| t   |  |                    |                |  |  |                               |   |                                       |                        |                   | EE                 |              |
|   | hards  | 1.4                |                | And the second s | and the second                               |                               | -                                       |                                       | Second Second          | C                 | Rectar Destruction | FF           |
|   | Optimum Mc   |                    |                | Max Dry Den  |  |                               |   |                                       | sture, % (+ or         | -)                | % Field Comp       |              |
|   | Plotted GG   | 12.2               |                | Plotted HH   | 119.0  |                               | Optir                                   | num                                   | -6.5                   |                   | (T/HH)x100         | . 84.        |
| ks  |  |                    |                |  | 2  |                               |   |                                       |                        |                   |                    | -            |
|   |  |                    |                |  |  |                               |   |                                       |                        |                   |                    |              |
|   |  |                    |                |  |  |                               |   |                                       |                        |                   |                    |              |

# WYOMING DEPARTMENT OF TRANSPORTATION T-140 MAXIMUM DRY DENSITY - OPTIMUM MOISTURE (Rev. 09-16) PLOTTING WORKSHEET

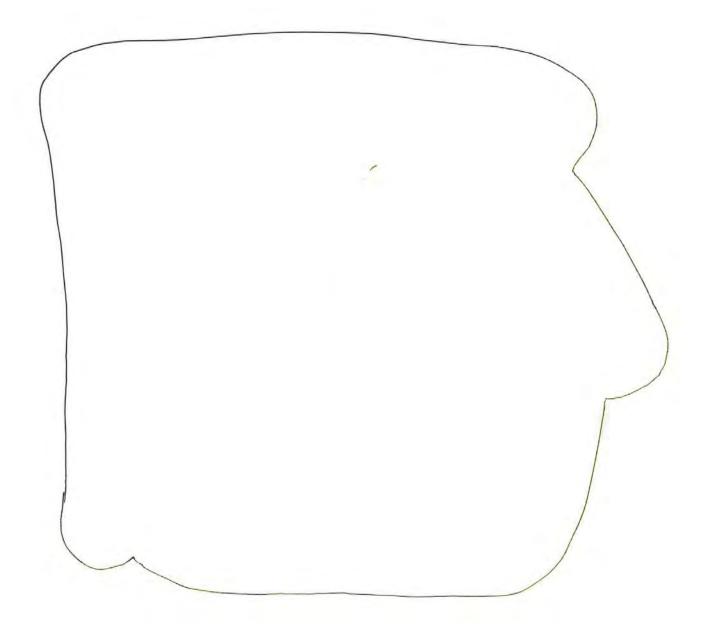


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### 44.2 44.7 45.2 45.7 45.7 46.2 46.6 47.1 47.1 48.1 48.6 49.1 49.6 50.0 51.0 51.5 52.5 52.5 53.4 53.9 54.4 54.9 53.0 55.4 55.9 56.4 56.8 15% 57.3 57.8 58.3 59.3 59.8 60.2 60.7 61.2 62.2 62.7 63.2 61.7 44.9 45.3 45.8 46.3 46.7 47.2 47.6 48.1 48.5 49.0 49.4 49.9 50.3 51.2 14% 40.8 41.7 41.7 42.6 42.6 43.1 43.5 44.0 44.4 52.1 52.6 53.1 53.5 54.0 54.4 54.9 55.3 55.8 56.2 56.7 57.1 57.6 58.0 58.5 58.9 51.7 37.9 38.7 38.7 39.6 39.6 40.4 40.4 40.8 41.3 13% 41.7 42.1 42.5 42.9 43.4 43.4 43.8 43.8 44.6 45.5 45.5 45.9 46.3 46.7 47.2 47.2 48.0 48.4 48.8 49.3 50.1 50.5 50.5 50.9 51.4 51.8 52.2 52.6 53.1 53.1 53.9 54.3 54.3 $\begin{array}{c} 12\%\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 35.6\\ 33.6\\ 35.6\\ 33.6\\ 35.6\\ 33.6\\ 35.6\\ 33.6\\ 35.6\\ 33.6\\ 35.6\\ 33.6\\ 35.6\\$ 35.3 35.5 5 36.0 36.0 36.3 36.3 36.7 37.4 37.4 37.4 37.4 37.4 37.4 37.4 37.4 37.4 37.4 37.4 37.4 37.3 38.5 38.5 39.5 11% 32.1 32.4 32.8 33.5 33.5 33.5 33.6 34.6 34.6 34.9 42.0 42.4 42.8 43.1 43.5 43.8 44.5 44.5 44.9 45.2 45.6 46.0 46.0 35.3 35.6 36.0 36.3 36.6 38.2 38.5 39.2 39.2 10% 29.5 29.5 29.8 30.1 30.4 30.8 31.1 31.7 31.7 32.1 32.4 32.7 33.0 33.7 33.7 34.0 34.0 34.3 34.3 34.3 34.3 34.3 36.9 37.9 ADDITIONAL MOISTURE REQUIRED 37.2 39.8 40.2 40.5 40.8 41.5 41.8 41.1 31.8 32.1 32.4 32.6 32.9 33.2 33.5 33.8 34.1 34.4 34.7 35.0 35.3 35.3 35.9 36.1 36.4 36.7 37.0 37.3 37.6 28.2 28.5 28.8 29.0 29.3 29.5 29.8 30.1 30.3 30.6 30.8 31.1 31.4 31.6 31.9 32.1 32.4 32.6 32.9 33.2 33.4 33.7 8% 7% 2014 22019 2014 27.9 28.1 28.3 28.6 28.8 28.8 28.8 28.8 29.0 29.0 6% 6% 17.5 17.5 17.9 18.3 18.3 18.3 18.3 18.3 18.3 18.3 18.3 18.3 19.6 19.6 19.2 20.8 20.8 20.8 20.8 21.1 22.1 22.0 22.0 22.0 22.0 22.0 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 22.1 22.2 14.6 14.7 14.9 15.1 15.2 15.4 15.7 15.7 15.9 16.4 16.5 16.7 16.7 17.0 17.1 17.2 17.1 17.2 17.3 17.1 17.2 17.1 17.2 17.1 17.2 17.3 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17.5 18.0 18.5 18.9 19.1 19.4 19.8 19.8 19.8 20.1 20.1 20.4 20.4 16.0 16.2 20.6 20.7 20.9 21.1 5% 12.2 12.3 12.4 12.6 12.6 12.7 11.8 11.9 12.0 13.0 13.1 13.3 13.5 13.6 13.7 13.9 14.0 14.1 14.3 14.6 14.6 14.8 14.9 15.0 15.2 15.3 15.4 15.5 15.7 15.9 16.1 16.2 16.3 16.5 16.6 16.7 16.8 15.8 11.7 4% 10.0 10.1 10.1 10.2 10.3 10.4 10.5 10.6 10.7 10.8 10.9 10.1 10.1 10.2 10.3 10.4 10.3 11.0 11.5 12:0 12:1 12:3 12:5 12:5 12:5 11.1 11.2 11.3 11.4 11.6 11.7 8.7 8.9 9.1 9.2 9.2 9.5 9.5 9.6 9.9 9.9 11.9 3% 6.3 6.5 6.5 6.6 6.6 7.0 7.1 7.2 5.8 6.0 6.2 6.2 6.3 6.7 6.8 6.9 6.9 7.3 7.4 7.7 7.8 7.8 8.2 8.3 8.4 7.6 7.6 7.9 8.0 8.1 2% 8.2 $\begin{array}{c} 1\, \frac{1}{8} \\ 3\, \frac{1}{3} \\ 3\, \frac{1}{3}$ 3.9 3.9 3.9 3.9 4.0 4.0 4.0 4.1 4.1 4.2 4.2 SOIL DRY DENSITY lbs/ft<sup>3</sup> $\begin{array}{c} 999 \\ 991 \\ 992 \\ 992 \\ 992 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 993 \\ 911 \\ 111 \\$ 117 $\begin{array}{c} 1118 \\ 1120 \\ 1121 \\ 1126 \\ 1128 \\ 1129 \\ 1129 \\ 1129 \\ 1129 \\ 1129 \\ 1129 \\ 1129 \\ 1120 \\ 1129 \\ 1120 \\ 11$

# GALLONS OF WATER PER CUBIC YARD OF EMBANKMENT



Example of French Curve

Must be made of solid material, i.e., plexiglass or cardboard

Can be acquired from a WYDOT IA Inspector or the WYDOT Materials Program

### **STANDARDIZATION OF SAND**

| Scope:                  | This procedure is used to obtain a standard density of sand.  |  |  |  |  |  |
|-------------------------|---|--|--|--|--|--|
| Apparatus:              | <ol> <li>Sand cone apparatus (jar and funnel)</li> <li><sup>1</sup>/<sub>10</sub> ft<sup>3</sup> measure</li> <li>Glass plate (use the glass from <i>Plastic Limit Test and Plasticity Index</i> WYDOT 813.0)</li> <li>Thermometer, capable of measuring water temperature to ±1°F</li> <li>Steel straightedge, 15 inch</li> <li>Scale, sensitive to 0.01 lb</li> <li>Sieves, No. 10, No. 20, and No. 40</li> <li>Sand container, 15 inch round pan or 15 inch x 15 inch square pan, suggested</li> </ol> |  |  |  |  |  |
| Reference<br>Documents: | <ul> <li>AASHTO T 19M/T 19</li> <li>Standard Method of Test for Bulk Density ("Unit<br/>Weight") and Voids in Aggregate</li> <li>Standard Method of Test for Density of Soil In-<br/>Place by the Sand-Cone Method</li> </ul>   |  |  |  |  |  |

|           |             | Moisture Test   |
|-----------|-------------|---|
|           | WYDOT 813.0 | Plastic Limit Test and Plasticity Index                   |
|           | WYDOT T-112 | Soils Compaction Worksheet                                |
|           | WYDOT T-302 | Standardization of Sand Worksheet                         |
| ibration: |             | foot measure before use. Tare the measure with a piece of |

Definitions – Water Table

Moisture - Density Method Selection and Borrow

WYDOT 100.0

WYDOT 210.0

Calibration: Calibrate the  $\frac{1}{10}$  cubic foot measure before use. Tare the measure with a piece of plate glass on top. Fill the mold with water at room temperature and cover with a piece of plate glass in such a way as to eliminate bubbles and excess water. Determine the mass of water in the mold using a balance. Measure the temperature of water to the nearest  $\pm 1^{\circ}$ F to determine its density from the WYDOT 100.0 – *Definitions* – *Water Table*.

Calculate the volume of the mold by dividing the mass of water required to fill the mold by its density. For temperature/density of water refer to WYDOT 100.0 - Definitions - Water Table.

$$V = \frac{B - C}{D}$$

- V = Volume of the measure, ft<sup>3</sup>
- B = Mass of the water, plate glass, and measure, lb
- C = Mass of the plate glass and measure, lb
- D = Density of the water for measured,  $lb/ft^3$

Procedure: Calibrate the sand used to fill the funnel by filling the 1 gal jar with standard sand. Weigh the apparatus and sand. Invert the sand cone apparatus into a <u>flat</u> level pan, open the valve and let the sand run into the funnel until the sand has ceased to flow, close the valve, and weigh the sand in either the pan or the apparatus and remaining sand; either way will give you the amount of sand to fill the funnel. Care should be taken not to agitate the apparatus while the sand is moving, as this would rearrange the sand particles and give an erroneous answer. Repeat this two more times and average the weight. Record the average weight as item "E" on Form T-112. This weight should remain constant for each test as long as the standard density of sand remains the same.

Screen out approximately 20 pounds of sand between two sieve sizes. These sieves, No. 10 to No. 20, No. 10 to No. 40, or No. 20 to No. 40 may be selected to most conveniently fit the gradation of the sand. Discard the material outside the limits of these sieves.

Fill the sand cone apparatus with sand and invert the cone over a calibrated  $\frac{1}{10}$  cubic foot measure, open the valve at the neck of the cone and allow the sand to run freely into the measure. When the sand ceases to move in the jug, close the valve and raise the sand cone and jug vertically away from the measure. While using the straightedge, strike the sand off level with the top of the measure with as few strokes as possible. Use extreme care not to jar or shake any part of the apparatus during this operation, as this would tend to rearrange sand particles and provide an erroneous standard weight. Weight of measure filled with sand, minus the tare, equals the weight of standard sand. To figure the weight per cubic foot of standard sand, divide the weight of the sand to fill the measure by the volume of the measure.

The standard sand should be cleaned by re-sieving after each time it is used to remove dirt particles. The sand should be rechecked for its standard weight per cubic foot after it has been used for several compaction tests, and should be checked after any large variance in humidity to compensate for any possible bulking. If bulking has occurred, the sample should be dried and rescreened.

Example: Measure holds 6.00 pounds of water and 8.26 pounds of sand.

$$\frac{6.00}{62.4} = 0.0961 \text{ ft}^3 \text{ (volume)} = \frac{8.26}{0.0961} = 86.0 \text{ pcf}$$

Report: Report the density of the sand  $(D_B)$  on Form T-112, Soils Compaction Worksheet, as Item A.

Report results on Form T-302, *Standardization of Sand Worksheet*. An example of Form T-302 is included in this section.

An example of Form T-112 is in WYDOT 210.0, *Moisture - Density Method Selection and Borrow Moisture Test.* 



# WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LAB STANDARDIZATION OF SAND WORKSHEET

Tested By: Tester Date Tested: XX/XX/XX

T-302 (Rev. 10-18)

Project No(s).: ####### Project Name: Name of Project Engineer: Engineer's Name

| TARE OF MEASURE + PLATE   | 8.23   | lb     |
|---|--------|--------|
| B WEIGHT OF MEASURE + PLATE + WATER   | 14.40  | Ъ      |
| $\sum$ weight of water = (B - A)  | 6.17   | lb     |
| TEMPERATURE OF WATER *  | 62     | •      |
| D DENSITY OF WATER *  | 62.355 | lbs/ci |
| *For temperature/density of water refer to WYDOT 100.0 - Definitions Water Table. | 1.1.1  |        |
| VOLUME OF MEASURE = (C / D)   | 0.099  | cf     |
| TARE OF MEASURE   | 5.22   | lb     |
| G WEIGHT OF MEASURE + SAND #1   | 14.81  | lb     |
| WEIGHT OF MEASURE + SAND #2   | 14.80  | 1b     |
| I WEIGHT OF MEASURE + SAND #3   | 14.83  | lb     |
| J average weight of sand + measure = (F + G + H) / 3                              | 14.81  | _1b    |
| WEIGHT OF SAND = (J - F)  | 9.59   | 16     |
| , DENSITY OF SAND = $(K / E)$   | 96.87  | lb/cf  |

WEIGHT OF SAND TO FILL FUNNEL

| TOTAL WEIGHT OF APPARATUS | A | 17.30 | lb |
|---------------------------|---|-------|----|
|---------------------------|---|-------|----|

STEP 1 WEIGHT OF APPARATUS - SAND TO FILL FUNNEL

| 12 68 | lb    |
|-------|-------|
| 13.00 | 10    |
|       | 13.68 |

 $\underline{STEP\,2} \text{ weight of sand to fill funnel}$ 

E 3.62 lb (A - B)

| F | 3.59    | lb |
|---|---------|----|
|   | (B - C) |    |

C 10.09 lb

D 6.49 lb

3.60 lb G (C - D)

AVERAGE K 3.60 lb (E + F + G) / 3

#### SAND CONE METHOD FIELD DENSITY TEST

- Scope: This procedure is intended to determine the density of a soil, either in its natural state or after being compacted. The procedure described below is intended to test soils containing particles not larger than 2 inches in diameter.
- Apparatus: 1. Sand cone apparatus, 1 gal jar and funnel
  - 2. Containers with lids, suggest two concrete cylinder cans
  - 3. Chisel and hammer
  - 4. Rammer with guide,  $5\frac{1}{2}$  lb
  - 5. Spoon or half round dish
  - 6. Shovel
  - 7. Square pans 15 inch, suggested
  - 8. Drying stove
  - 9. Moisture tins
  - 10. No. 4 screen
  - 11. Wooden block, suggest 2 inch x 4 inch
  - 12. Gram scale, sensitive to 0.1 g
  - 13. 35 lb [15 kg] scale sensitive to 0.01 lb [5 g]
  - 14. Base plate optional
  - 15. 2 inch [50 mm] screen
  - 16. Standard Sand
  - 17. Clean canvas sample sacks
  - Note: For WYDOT personnel, contact the WYDOT Materials Program (Field Services) for information or sources for standard sand.

## Reference

| Documents: | AASHTO T 191 | Standard Method of Test for Density of Soil In-Place by the |
|------------|--------------|---|
|            |              | Sand-Cone Method  |
|            | WYDOT 211.0  | Standardization of Sand                                     |
|            | WYDOT 213.0  | Moisture - Density Relations of Soils Method "A"            |
|            | WYDOT T-112  | Soils Compaction Worksheet                                  |
|            | *WYDOT T-113 | Weekly Report of Compaction of: Embankment                  |

- \* Note: Use of weekly reports is optional
- Procedure: Laboratory Preparations
  - 1. Record the standard sand density as item "A" on Form T-112, *Soil Compaction Worksheet*, see WYDOT 211.0, *Standardization of Sand*. Also see example Form T-112 of this section.
  - 2. Calibrate the sand used to fill the funnel by filling the 1 gal jar with standard sand. Weigh the apparatus and sand. Invert the sand cone apparatus into a <u>flat</u>

level pan, open the valve and let the sand run into the funnel until the sand has ceased to flow, close the valve, and weigh the sand in either the pan or the apparatus and remaining sand; either way will give you the amount of sand to fill the funnel. Care should be taken not to agitate the apparatus while the sand is moving, as this would rearrange the sand particles and give an erroneous answer. Repeat this two more times and average the weight. Record the average weight as item "E" on Form T-112. This weight should remain constant for each test as long as the standard density of sand remains the same.

- 3. Fill the sand cone; 1 gal jar with standard sand, weigh the apparatus and sand. Record as item "B" on Form T-112.
- 4. Weigh an empty container and lid (concrete cylinder can) and record the weight as item "H" on Form T-112.

#### Field Operation

- 1. Have a motor grader or loader scrape off about 1 foot of the surface. Level off an area approximately 2  $ft^2$  to accommodate the sand cone, removing all loose material from the test area.
- 2. Place the sand cone in the cleared area and scribe an outline of the cone on the soil for a guide while digging the hole. Using the chisel and spoon, dig a test hole a minimum of 4 inches in diameter by 6 inches deep. Place soil into a tared container with an air tight lid to prevent moisture loss. Remove all loose soil from the hole. Take care not to disturb the sides of the hole when removing the material.

When a rock 2 inches or larger is encountered, it is recommended that another test hole be dug fairly close to the first one started. If a rock 2 inches or larger is encountered again, then it may be necessary to try a few more locations, but if at all possible, the test hole should be completed. This information is also used to establish the percent rock encountered within the fill area.

If no test hole can be dug in any of the locations attempted, then determine the percent rock by shovel sampling a representative area of the fill. If the percent rock falls below 40%, a test hole will have to be dug.

Note: A base plate may be used in place of scribing an outline of the cone on the soil. The base plate gives the advantage of a larger diameter hole especially when rock and/or thin lifts of gravel for surfacing or soils is encountered. If the base plate is used, it will be considered a part of the funnel and becomes part of the calibration of the funnel and entered as item "E" on Form T-112.

- 3. Invert the sand cone apparatus, placing the cone over the hole, open the valve all of the way and allow the sand to flow freely. Be careful not to agitate the apparatus or the surrounding ground while the sand is running. When the sand ceases to flow, close the valve and carefully remove the jar from the hole. Gather as much sand from the hole area as possible, placing the sand into a separate container to be reclaimed later.
  - Note: Dig out approximately 45 lb of material from around the hole; keep in mind that the material needed should be as close as possible to the material from the hole. Dig in a 2 ft radius of the hole; be careful not to dig deeper than the test hole.

#### Laboratory Operation

- 1. Weigh the sand cone apparatus and the remaining sand. Record as item "C" on Form T-112.
- 2. Weigh the soil, rock, and container. Record as item "G" on Form T-112.
  - Note: Coarse is defined as material retained on the No. 4 screen. For this procedure, percent rock is used to describe the percent of coarse material in a sample.
- 3. Using the 2 inch x 4 inch wooden block, separate soil and rock on the No.4 screen. Material remaining on the No. 4 screen is rock and must be free of soil or clay coatings. Weigh the rock retained and record as item "J" on Form T-112. Determine the percent rock as outlined on Form T-112, item "K".
- 4. Take a representative moisture sample of not less than 100 g for material with 0% to 15% rock, or 500 g for material with 15% to 40% rock. If the percent rock is found to be between 15% to 40%, recombine the percent rock back into the moisture sample at the same percent as found on Form T-112, item "K".
- 5. Complete all computations up to and including item "S" on Form T-112.
- 6. Dry the field moisture sample, calculate the percent moisture, record as item "R" and then compute dry density of fill, item "T" on Form T-112. Take the moisture sample from the cylinder can before screening the 45 lb sample.

7. Rock correction is used with material that has between 0 to 15% rock.

Percent Rock (to nearest whole number) = <u>Percent Rock</u>

3

Report: Report weekly results on optional Form T-113, *Weekly Report for Compaction of: Embankment*. See example Form T-113 in WYDOT 213.0.



#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SOIL COMPACTION WORKSHEET

FORM T-112 (Rev. 09-16)

|          | d Test No.<br>mitted By         |                              | BM-E#1<br>Resident E | naineer       |               |       | Date<br>At |           |            |           | t#/#<br>ent Er | nginee             | r's Tc   | wn      |          |       |
|----------|---------------------------------|------------------------------|----------------------|---------------|---------------|-------|------------|-----------|------------|-----------|----------------|--------------------|----------|---------|----------|-------|
|          | ion Sampled                     |                              | STA 0+50             | inginiee.     |               |       |            | tical Lim | -          | 2 ft -    | _              | .g                 |          |         |          |       |
|          | th Taken                        |                              | 3 ft                 |               |               | _     |            | ject No(s |            |           | 4##            |                    |          |         |          |       |
| 0.000    | ion Represe                     | 1                            | STA 0+00             | To 0+100      |               |       | 2.2.2      |           | -          | and the s | 010340         |                    |          |         |          | -     |
|          |                                 |                              | Tes                  | t was made    | 0             | Same  | -          | day(s)    | after fi   | ll wa     | s plac         | ed.                |          |         |          |       |
| A        | Density of S                    | itandard Sand                | 1 16/603             |               | 96.7          | h mai |            |           | Conte      | nt (R     | oadwa          | ay)                | Wt. c    | ofWater | - 3373   | t. of |
| <u> </u> | Density of a                    |                              | i, 10/11             | -             | 30.7          | P(    | Wet        | Soil and  | Dry Soi    | l and     | Tar            | e of               |          |         | Dry      |       |
| -        |                                 |                              |                      |               | 1.0.00        | N     |            | lin, g    | Tin,       |           |                | n, g               |          | - M, g  | M -      |       |
| В        | the second second second second | ratus and Sar                |                      |               | 15.83         |       | L          | 265.6     |            | 227.1     | N              | 42.1               | P        | 38,5    | Q        | 18    |
| c        |                                 | ratus and Uni                | used Sand, I         | b             | 5.84          |       | R          | % Mois    | ture, ( P  | • / Q) :  | k 100          |                    |          |         | 20.8     |       |
| D        | Sand Used                       |                              | -                    |               | 9,99          | 6     |            | harro     |            | 10.2 1 1  | A 14           |                    |          |         |          |       |
| F        |                                 | to Fill Funnel               |                      |               | 3.62          | <     | S          |           | nsity, Ib  |           |                |                    | (1 (2)   |         | 11       | 6.7   |
| 1.5      | Sand to Fill                    | Hole (D - E), I              | D                    |               | 6.37          | *     |            | -         | % - 15%    | _         |                | _                  | (3/3)    | ,       | Net II.  |       |
| G        | Wt. of Soil                     | Coarse and C                 | ontainer Ib          | 1             | 8.82          | йн    |            | 1.100     | 5% - 403   | a nego    | 101            |                    |          |         | Not Us   | 500   |
| н        |                                 | Container, Ib                | oritainer, ib        |               | 1.08          | Q     | Т          | T         |            | Dry D     | ensity         | lb/ft <sup>3</sup> |          |         | <u> </u> | -     |
| 1        |                                 | Coarse (G - I                | -1), Ib              |               | 7.74          |       | <u> </u>   | 1.00      |            |           | / (100         |                    |          |         | 9        | 7.6   |
|          | 1                               |                              | 19.23                |               |               |       |            | ** For 0  | % - 15%    | _         |                |                    | 0 + (K/  | (3))    |          |       |
| J.       | Wt. of Coars                    | se (Retained o               | on No. 4), Ib        |               | 0.16          | h. I. |            | where     | (K/3) is t | to nea    | rest w         | hole n             | umber    |         |          |       |
| к        | % of Coarse                     | , (J / I) x 100              | <                    |               | 2.1           |       |            | * For 1   | 5% - 40    | % Roi     | sk, let        | \$=S :             | 100      |         | Not Us   | sed   |
|          |                                 |                              |                      |               |               | 1     |            |           | -          |           |                |                    |          |         |          |       |
| V        | Wet Wt. of S                    | Soil and Mold,               | lb                   |               |               | 13.28 |            | 13.18     |            |           |                |                    |          |         |          |       |
| W        | Tare Wt. of                     | Mold, Ib                     | (                    |               |               | 9.31  |            | 9.31      | 1.1.1      | 11        |                |                    |          |         |          |       |
| Y        |                                 | Soil in 1/30 ft <sup>s</sup> |                      | V)            | 11            | 3.97  | -          | 3.87      | 21         | - 18      |                |                    | *        |         |          | -     |
| z        | Wet Density                     | of Soil, Ib/ft3,             | Y x 30               | ÷             |               | 119,1 |            | 116.1     | 1          | I i       |                |                    |          |         |          |       |
|          |                                 |                              | ity of Soil, Ib      | o∕ft³         |               |       |            |           |            |           |                |                    |          |         |          |       |
|          |                                 |                              | 2 x 100              |               | -             | 100.8 |            | 99.4      |            |           |                |                    |          |         |          |       |
|          | (100                            | + (AA or BB o                | r CC or DD o         | or EE or FF)) |               | -     | -          |           |            |           |                | -                  | -        |         | -        | _     |
| м        |                                 |                              |                      |               | 1             | ¢.    |            |           | %          |           | re (P/Q)       |                    | ° 17     |         |          |       |
| o<br>i   | <b>L</b> o                      | M                            | N                    | P<br>Wt. of   | Q<br>Wt. of   |       |            |           | 1 Oct      | X 1I      | 00             |                    |          |         |          |       |
| s<br>t   | Wet Soil                        | Dry Soil                     | Tare of              | Water         | Dry Soil      |       |            |           |            |           |                |                    |          |         |          |       |
| u        | and Tin, g                      | and Tin, g                   | Tin, g               | L - M, g      | M - N, g      |       | 1          |           |            |           |                |                    |          |         |          |       |
| re       | 293.2                           | 254.0                        | 38.4                 | 39.2          | 215.6         | 18.2  |            | _         | 1 10       |           |                |                    |          |         |          |       |
| с        | 219.1                           | 193.6                        | 42.1                 | 25.5          | 151.5         | AA    | -          | 16.8      | 2          |           |                |                    | 44       |         |          |       |
| o<br>n   |                                 |                              |                      |               |               |       |            | BB        |            |           | 1              | _                  | din.     |         |          |       |
| t        |                                 |                              |                      |               |               | 2     |            |           | CC         | 1         |                | 20                 | <u> </u> |         | - N      |       |
| e<br>n   |                                 |                              |                      |               |               |       |            |           |            |           |                | D                  | L        | CE .    |          | _     |
| t        |                                 |                              |                      |               | 1             | 2     |            |           |            |           |                |                    |          | EE      | 1        | F     |
|          | Optimum M                       | oisture %                    |                      | Max Dry De    | nsity, Ib/ft³ |       | Roa        | dway Moi  | sture %    | ( + or    | -)             |                    | % Fie    | d Comp  |          |       |
|          | Plotted GG                      | 20.8                         |                      | Plotted HH    | 102.5         |       |            | mum       | 0.0        |           |                |                    | (т/нн    | )x100   | 95       | 5.2   |
| arks     |                                 |                              |                      |               |               |       |            |           |            |           |                |                    |          |         | -        |       |
| 27       | d.                              |                              |                      |               |               |       |            |           |            |           |                |                    |          |         |          |       |

Certification No. ###



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Remarks

#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SOIL COMPACTION WORKSHEET

FORM T-112 (Rev. 09-16)

15 to 40% Rock Example BM-E #1 ##/##/## Field Test No. Date Resident Engineer Submitted By At Resident Engineer's Town STA 0+50 Vertical Limits 2 ft - 8 ft Station Sampled 3 ft N##### **Depth Taken** Project No(s). Section Represented STA 0+00 To 0+100 day(s) after fill was placed. Test was made Same Wt. of Moisture Content (Roadway) Wt. of Water Density of Standard Sand, Ib/ft<sup>3</sup> 96.7 Dry Soil Wet Soil and Dry Soil and Tare of L - M, g M - N, g Tin, g Tin, g Tin, g B Wt. of Apparatus and Sand, Ib 15.73 L 788.6 M 744.5 N 105.1 P 44.1 Q 639.4 C Wt. of Apparatus and Unused Sand, Ib 6.35 R % Moisture, (P/Q) x 100 6.9 Sand Used (B - C), Ib 9.38 3.45 S Wet Density, Ib/ft<sup>3</sup> ( (A x (\* I) ) / F 136.2 5.93 Not Used \* For 15% - 40% Rock, let I = I 9.45 т 1.10 Dry Density Ib/ft<sup>3</sup> 8.35 \*\* S / (100 + R) 127.4 For 0% - 15% Rock, S = 5 x (100 + (K/3)) 2.51 Not Used \*\* For 15% - 40% Rock, let S = S x 100 30.1 13.94 14.13 9.52 9.52 4.42 4.61 132.6 138.3 Dry Density of Soil, lb/ft<sup>3</sup> Z x 100 123.7 127.0 (100 + (AA or BB or CC or DD or EE or FF)) % Moisture (P/Q) x 100 L M Ν P Q Wt. of Wt. of Wet Soil **Dry Soil** Tare of Water Dry Soil Tin, g and Tin, g and Tin, g

D Wt. of Sand to Fill Funnel, Ib Ε Sand to Fill Hole (D - E), Ib F G Wt. of Soil, Coarse and Container, Ib H Tare Wt. of Container, Ib I. Wt. Soil and Coarse (G - H), lb Wt. of Coarse (Retained on No. 4), Ib J κ % of Coarse, (J / I) x 100 V Wet Wt. of Soil and Mold, Ib W Tare Wt. of Mold, Ib Wet Wt. of Soil in 1/30 ft<sup>3</sup> Mold (V - W) Y Z Wet Density of Soil, Ib/ft<sup>3</sup>, Y x 30 L - M, g M - N, g 873.5 822.0 106.7 715.3 7.2 51.5 851.9 790.9 105.1 AA 685.8 61.0 8.9 BB сс DD EE FF Max Dry Density, Ib/ft3 Roadway Moisture % (+ or -) % Field Compaction **Optimum Moisture %** Plotted GG 10.6 Plotted HH 129.7 (T/HH)x100 98.2 Optimum -3.7 Tested By Tester Certification No. ###

## MOISTURE - DENSITY RELATIONS OF SOILS METHOD "A"

Scope: The following method will be used when rock is encountered from 0% to 15%. If the rock is over 15%, Method "C" will be used (see WYDOT 214.0). If rock is determined to exceed 40%, compaction tests are not required in accordance with *WYDOT Standard Specifications* Section 203.4.3.1; place and compact material in accordance with *WYDOT Standard Specifications* Section 203.4.1, and at least 24 inches below the finished grade. Moisture-density control is required.

This procedure is intended to determine the maximum dry density and optimum moisture content of a soil using a standard compactive effort. This is accomplished by running several cylinders at various moisture contents with the same compactive effort.

#### Apparatus: 1. Pans, 15 inch suggested

- 2. Rammer with guide, 5<sup>1</sup>/<sub>2</sub> lb, *See Appendix A of this section for tolerances*
- 3. Drying stoves
- 4. Moisture tins
- 5. Trowel
- 6. Steel straightedge, 15 inch length minimum
- 7. No. 4 screen
- 8. Wooden block, suggest 2 inch x 4 inch
- 9. 0.03 ft<sup>3</sup> [0.001 m<sup>3</sup>] mold, See Appendices A & B of this section for tolerances
- 10. Compaction block, 300 lb minimum
- 11. Extruder
- 12. Gram scale, sensitive to 0.1 g
- 13. 35 lb [15 kg] scale sensitive to 0.01 lb [5 g]
- 14. 100 ml graduated cylinder

#### Reference

| Documents: | AASHTO T 19 M/T | Standard Method of Test for Bulk Density ("Unit Weight")<br>and Voids in Aggregate   |
|------------|-----------------|--|
|            | AASHTO T 99     | Standard Method of Test for Moisture-Density Relations of<br>Soils Using a 2.5-kg (5.5 lb) Rammer and a 305-mm (12-<br>in.) Drop |
|            | WYDOT 203.4.1   | WYDOT Standard Specifications  |
|            | WYDOT 203.4.3.1 | WYDOT Standard Specifications  |
|            | WYDOT 100.0     | Definitions  |
|            | WYDOT 212.0     | Sand Cone Method Field Density Test  |
|            | WYDOT 214.0     | Moisture – Density Relations of Soils Method "C"   |
|            | WYDOT T-112     | Soils Compaction Worksheet   |
|            | *WYDOT T-113    | Weekly Report of Compaction of: Embankment   |
|            | WYDOT T-140     | Plotting Worksheet   |

\* Note: Use of weekly reports is optional

- Sample: Representative soil samples are taken from either field density tests *Sand Cone Method*, WYDOT 212.0, or from any material where maximum dry density or optimum moisture content is requested. The percent rock in the soil should be determined before any cylinders are compacted. If a field density test is run, the percent rock is taken from Form T-112, item "K". To find the percent rock in any soil sample, separate the minus 2 in material over the No. 4 screen and weigh the rock retained on the screen; divide the rock retained by the total weight of the sample retained.
  - Note: Coarse is defined as material retained on the No. 4 screen. For this procedure, percent rock is used to describe the percent of coarse material in a sample.
  - Note: Individual 7 lb samples should be used for each cylinder. Generally four cylinders are required to plot a curve; enough material should be screened on the No. 4 screen to have four separate and new samples for each cylinder; three cylinders under optimum moisture and one cylinder over optimum.
- Procedure: 1. Use material passing the No. 4 screen. A 7 lb sample of thoroughly mixed material, air-dried or stove-dried at 140 °F to approximately 4% points below optimum moisture or, damp enough that when a portion is tightly squeezed in the palm of the hand, it will hold together.

Weigh the mold and base plate and record as "Tare Weight of Mold", item "W" on Form T-112.

With the screened material, fill the 0.03 ft<sup>3</sup> mold fit with collar attached to  $\frac{1}{3}$  of its depth and place on a compaction block of 300 lb or more which is on a rigid uniform foundation. Using the 5½ lb rammer with a free fall of 12 inches above the soil, distribute 25 blows over the entire surface of the soil within the mold. Add more soil to the mold, approximately  $\frac{2}{3}$  of its depth, compact this layer with 25 blows of the rammer. Add the last lift to the mold, compacting this lift with 25 blows of the rammer to a total compacted depth of approximately 5 inches.

- 2. After the soil has been compacted, the mold collar is removed from the mold assembly and the compacted soil carefully trimmed evenly with the top of the mold cylinder using the 15 inch straightedge. Weigh the 0.03 ft<sup>3</sup> mold, base plate and the compacted soil, record under "Wet Weight of Soil and Mold" first cylinder, item "V" on Form T-112.
- 3. Remove the base plate and extract the compacted soil from the mold. An extruder and plug can be used when necessary. Slice the compacted soil vertically through the center. Cut a representative moisture sample, weighing not less than 100 g from the center of one of the faces, which includes all three lifts. The weight of the moisture sample and container will be recorded under item "L", Moisture Content (Cylinder), on Form T-112.

- 4. With the first cylinder completed and recorded on Form T-112, compact the 7 lb sample for the next cylinder using the same procedure with 2% additional moisture. Each additional 7 lb sample which is used for compacting cylinders should have moisture increases in increments of 2%. As water is added, give the moisture time to work into the soil before the sample is compacted.
  - Note: If for some reason there is not enough material for the four 7 lb samples, it is permissible to reuse one sample of 7 lb. For this one sample, repeat the sequence of compacting, screening on the No. 4 and re-compacting at each 2% increase increment in moisture. For A-4 soils, the four samples must be used only once. Always weigh the sample after screening and then add moisture.
- 5. Continue compacting cylinders at 2% moisture increases until the soil becomes saturated or there is a decrease or leveling off of item "V", on Form T-112.
- 6. Using the graph on the *Plotting Worksheet*, Form T-140, plot the dry density and moisture content for each cylinder run. Connect these points, using a French curve.
  - Note: For consistency. M-D curves will be hand-drawn using a french curve. While individual points may be plotted with the assistance of a computer program, the curve must be hand drawn.

The maximum dry density is the highest point on the curve and is recorded as item "HH" on Form T-112. The moisture content corresponding to the peak of the curve will be the optimum moisture and is recorded as item "GG" on Form T-112. Complete the calculations on Form T-112.

- Note: A separate and new sample will be used in each compaction test in instances where the soil material is fragile in character and will reduce significantly in grain size due to repeated compaction and in cases where the soil is a heavy-textured clay material into which it is difficult to incorporate water.
- Report: Report weekly results on optional Form T-113, *Weekly Report for Compaction of: Embankment*.

## WYDOT 213.0 APPENDIX A MOLD & RAM TOLERANCES

This appendix adopted from AASHTO T 99.

- 1. A 4 inch mold having a capacity of  $\frac{1}{30} \pm 0.0003$  ft<sup>3</sup> with an internal diameter of 4.000  $\pm$  0.016 inch and a height of 4.584  $\pm$  0.005 inch.
- 2. Molds Out of Tolerance Due to Use A mold that fails to meet manufacturing tolerances after continued service may remain in use provided those tolerances are not exceeded by more than 50 percent and the volume of the mold calibrated in accordance with Appendix B Calibration of Mold in this section is used in the calculations.
- 3. Rammer Manually Operated. Metal rammer with a mass of  $5\frac{1}{2} \pm 0.02$  lb, and having a flat circular face of 2.000 inch diameter with a manufacturing tolerance of  $\pm 0.01$  inch. The in-service diameter of the flat circular face will be not less than 1.985 inch. The rammers will be equipped with a suitable guide-sleeve to control the height of drop to a free fall of  $12.00 \pm 0.06$  inch above the elevation of the soil. The guide-sleeve will have at least 4 vent holes, no smaller than  $\frac{3}{8}$  inch diameter spaced approximately 90 degrees apart and approximately  $\frac{3}{4}$  inch from each end and provide sufficient clearance so the free fall of the rammer shaft and head is unrestricted.
- 4. Calibration Equipment A piece of the plate glass, preferably at least <sup>1</sup>/<sub>4</sub> inch thick and at least 1 inch larger than the diameter of the measure to be calibrated. Water pump or chassis grease can be placed on the rim of the container to prevent leakage.

## WYDOT 213.0 APPENDIX B VOLUME OF MOLD

## This Appendix adopted from AASHTO T 19M/T.

Calibrate measures (molds) once a year or whenever there is reason to questions the accuracy.

- 1. Fill the mold with water at room temperature and cover with a piece of plate glass in such a way as to eliminate bubbles and excess water.
- 2. Determine the mass of water in the mold using a balance.
- 3. Measure the temperature of water to determine its density from Table 1, interpolating if necessary.
- 4. Calculate the volume of the mold by dividing the mass of water required to fill the mold by its density. For temperature/density of water refer to WYDOT 100.0 *Definitions Water Table*.

$$V = \frac{B - C}{D}$$

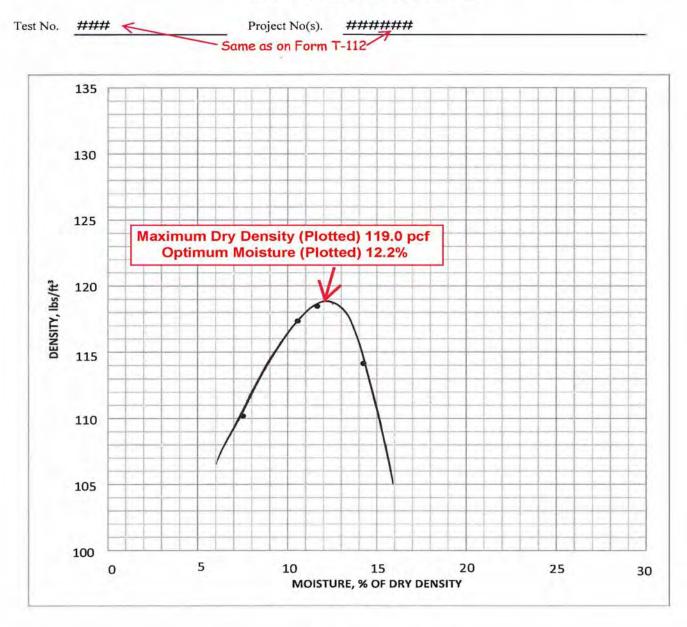
- $V = Volume of the measure, ft^3$
- B = Mass of the water, plate glass, and measure, 1 lb
- C = Mass of the plate glass and measure, 1 lb
- D = Density of the water for measured, lb/ft<sup>3</sup>

# WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SOIL COMPACTION WORKSHEET

|        |   | d By: Reside                  | ent Engine      | er            |              |         |  |             | Resdient's          | town              |        |           | _           | _             |
|--------|---|-------------------------------|-----------------|---------------|--------------|---------|--|-------------|---------------------|-------------------|--------|-----------|-------------|---------------|
|        | Deptn 1<br>tion Represe   | aken: 3 ft.                   |                 | - 0.00        |              | ver     |  |             | 2 ft - 8 ft.        |                   |        |           |             | -             |
| Sec    |   |                               |                 | La se e la se |              | De      |  |             | Any County          |                   |        |           | _           |               |
|        | Date San  | pled: <u>##/#</u>             | +++/ ++++++     | 7             | _            | Da      | ite Ke                                   | cervea      | ##/##/#             | ###               |        |           | _           | -             |
| 1      | a descenter of  |                               | Т               | est was made  |              | Same    | -  | _day(s)     | after fill was      | placed.           |        |           |             |               |
| A      | Density of St   | andard Sand, Ib               | o/ft³           |               | 96.4         |         | 13                                       | Moistu      | re Content (R       | oadway)           | Wt.    | of Water  | 1. A. S. S. | Vt. o<br>ry S |
| -      |   |                               |                 |               |              |         | 1. |             | Dry Soil and        | Tare of           | L      | - M, g    | м           | - N           |
| В      | Wt of Annar   | atus and Sand,                | lb              |               | 17.28        |         | L  | in, g       | Tin, g<br>M 630.9   | Tin, g<br>N 263.9 |        | 20.9      | Q           | 13            |
| C      | -   | atus and Unuse                |                 |               | 8.76         |         | R  |             | sture, (P / Q) x    |                   | 1 -    |           | 5.7         | 1.            |
| D      | Sand Used (E  |                               |                 |               | 8.52         |         |  | 1.2000      |                     |                   |        |           |             | -             |
| Е      |   | o Fill Funnel, II             | )               |               | 3.54         |         | S  | Wet D       | ensity, lb/ft³ ( (# | Ax(*I))/F         | -      |           | 1           | 02.           |
| F      | a cost and there are  | Hole (D – E), lb              |                 | 21            | 4.98         |         | U  | 1.000       | 9% - 15% Rock,      |                   | (J/3)) | 2         |             |               |
|        |   |                               |                 |               |              | Check % |  | 17-0-0      | .5% - 40% Roc       |                   |        |           |             |               |
| G      | Wt. of Soil, R  | ock and Contai                | ner, lb         |               | 6.15         |         |  |             |                     |                   |        |           |             |               |
| H      | Tare Wt. of C   | Container, lb                 |                 |               | 0.65         |         | Т  |             |                     | Density lb/ft³    |        |           |             |               |
| I      | Wt. Soil and  | Rock (G - H), lt              | 0               |               | 5.50         |         |  |             | **                  | S / (100 + R)     |        |           | 1           | 00.           |
| -      | lease and   |                               |                 |               | 222          |         | 1  | 4 102 CL2 V | 0% - 15% Roc        |                   |        | 5))       |             |               |
| J      | 1 4 5 5 1 5 5 T   | Retained on No                | o. 4), lb       |               | 0.68         |         | E I                                      | -           | (K/3) is to near    |                   |        | -         |             |               |
| K      | % of Rock, (  | 0 / 1) x 100                  |                 |               | 12.4         |         | ш  | ** For      | 15% - 40% Ro        | ck, let S = S x   | 100    |           | I)          |               |
| V      | Wet Wt. of S  | oil and Mold, lb              | ( . ····        |               |              | 14.08   | 1  | 4.46        | 14.54               | 14.48             | -      |           | 1           |               |
| W      | Tare Wt. of M   |                               | -               |               |              | 10.14   | -  | 10.14       | 10.14               | 10.14             | -      |           |             |               |
| Y      |   | oil in 1/30 ft <sup>3</sup> M |                 | , lb          |              | 3.94    | -  | 4.32        | 4.40                | 4.34              |        | _         |             |               |
| Z      | Wet Density   | of Soil, lb/ft³, Y            |                 | 1.20          |              | 118.2   | 1  | 29.6        | 132.0               | 130.2             | -      | -         |             |               |
|        |   | 1                             | ity of Soil, Il | p/ft³         |              | 110.2   |  | 17.4        | 118.4               | 114.1             | 1.     |           |             |               |
|        | (100  | + (AA or BB or                | CC or DD        | or FF or FF)  | -            | 110.2   |  | 47.7        | 110.4               |                   |        |           |             |               |
|        | (100  |                               | CC OF DD        | OF EE OF FF)) |              |         |  | _           |                     |                   | -      |           |             |               |
| м      | L   | м                             | N               | Р             | Q            |         |  |             | % Moistu<br>10      |                   |        |           |             |               |
| o<br>i |   |                               |                 | Wt. of        | Wt. of       |         |  |             |                     |                   |        |           |             |               |
| s<br>t | and the second se | Dry Soil and                  | Tare of         | Water L       | Dry Soil     |         |  |             |                     |                   |        |           |             |               |
| u      | Tin, g  | Tin, g                        | Tin, g          | - M, g        | M - N, g     |         |  |             |                     |                   |        |           |             |               |
| r<br>e | 683.7   | 658.5                         | 310.4           | 25.2          | 348.1        | 7.2     |  |             |                     |                   |        |           |             |               |
| с      | 493.5   | 471.9                         | 264.1           | 21.6          | 207.8        | AA      | 1.54                                     | 10.4        |                     |                   |        |           |             |               |
| o<br>n | 609.1   | 578.3                         | 310.7           | 30.8          | 267.6        |         |  | BB          | 11.5                |                   |        |           |             |               |
| t<br>e | 492.2   | 464.0                         | 264.1           | 28.2          | 199.9        | 8       | _  |             | CC                  | 14.1              | _      |           | . II.       |               |
| n      |   |                               | 1.2.1.2.2       |               |              |         |  |             |                     | DD                | -      |           |             |               |
| t      |   |                               |                 |               |              |         |  |             |                     |                   | 1      | EE        |             |               |
|        | Optimum Me  | oisture %                     |                 | Max Dry Den   | sity, lb/ft³ |         | Road                                     | way Moi     | sture, % (+ or      | -)                | % Fi   | eld Compa |             | FF            |
|        | Plotted GG  | 12.2                          |                 | Plotted HH    | 119.0        |         | Optin                                    | num         | -6,5                |                   |        | H)x100    |             | 84.4          |
| rks    |   |                               |                 | 100 C         |              |         |  |             |                     | 2                 |        |           |             |               |

Certification No.: ###

# WYOMING DEPARTMENT OF TRANSPORTATION T-140 MAXIMUM DRY DENSITY - OPTIMUM MOISTURE (Rev. 09-16) PLOTTING WORKSHEET



Tested By

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| T-113<br>(Rav. 09-16)   | I              |                        | /####   |                                | COMPACTION TESTED BY: |                     |              |       |       |       |   |               |       |       |       |       |   |               |       |       |       |   | T TALEN  |                  |                |                                     |        | CN           |          |                  |  |
|---|----------------|------------------------|---|--------------------------------|-----------------------|---------------------|--------------|-------|-------|-------|---|---------------|-------|-------|-------|-------|---|---------------|-------|-------|-------|---|--|------------------|----------------|-------------------------------------|--------|--------------|----------|------------------|--|
|   |                | End Week               | ##/ ##  | PERCEI                         | COMPAC <sup>-</sup>   | FILL<br>(B/Gi x 100 |              |       |       |       |   | 98.2          |       |       |       |       |   | 84.5          |       |       |       |   | TOTAL TESTS  | 133<br>133       | 22             | 7                                   |        | L YES        |          |                  |  |
|   |                | 10                     | DRATORY                                       | VVATER<br>%PTS.                | + OR -<br>FROM        |                     | -6.6         |       |       |       |   | -3.7          |       |       |       |       |   | -6.6          |       |       |       |   | TOT  | DENSITIES        | FINAL EMB.     | F NAL SUB-BASE                      |        |              |          |                  | 47   |
|   |                |                        | DATE RECD IN LABORATORY ## / ## / #####       | %                              | COARSE                |                     | 12.4         |       |       |       |   | 30.1          |       |       |       |       |   | 12.4          |       |       |       |   |  |                  |                | F NAL S                             |        | FINAL        |          | 8<br>8<br>8<br>8 | Joe Tester<br>###                                      |
| N   | C OTHER        | DATE <u>Begin Week</u> | DATE REC                                      | S - 2                          | Σ                     | bff°                | 119.0        |       |       |       |   | 129.7         |       |       |       |       | 2 | 119.0         |       |       |       |   |  |                  |                |                                     |        | Ĭ            |          |                  | TESTED BY: <b>Joe Tester</b><br>CATION NO.: <b>###</b> |
| DRTATIC<br>OF :   |                | DATE B                 |   | LAB, OR TYPICAL<br>CURVE VALUE | OPTIMUM I<br>WATER    | ,<br>жш             | 12.2         |       |       |       |   | 10.6          |       |       | 77 KA | .0 13 |   | 12.2          |       |       |       |   | 16700 (16.7)   | 12000(12)        | 5200 (5.2)     |                                     |        |              |          |                  | TESTED BY: Joe T<br>CERTIFICATION NO.: ####            |
| WYOMING DEPARTMENT OF TRANSPORTATION<br>Materials Testing Laboratory<br>WEEKLY REPORT FOR COMPACTION OF : |                |                        | 000   | %<br>WATER                     |                       | CYL NDER<br>F       | 5.6          | 7.2   | 10.4  | 141   | ! | 6.9           | 7.2   | 8.9   |       |       |   | 5.6           | 7.2   | 11.5  | 14.1  |   | 16   | F ¥              | <u>کا</u>      |                                     |        |              |          |                  | 0  |
| DEPARTMENT OF TRANS<br>Materials Testing Laboratory<br>Y REPORT FOR COMPACTIC                             | C CRUSHED BASE |                        |   |                                | DER                   | ×                   |              | 110.2 | 117.4 | 114.1 | 1 |               | 123.7 | 127.0 |       |       |   | 1             | 110.2 | 118.4 | 114.1 |   | M. GALS WATER  | JED THIS WEFK    | TOTAL TO DATE  | PREWET BY:                          |        | CUTS DRILLED |          |                  |  |
| PARTME<br>terials Te<br>REPORT  |                | -                      |   | SITY, Ib/ff                    | CYL NDER              | MET C               |              | 118.2 | 129.6 | 132.0 |   |               | 132.6 | 138.3 |       |       |   | 1             | 118.2 | 132.0 | 130.2 | Π | M GALS WATER   | USEU FRE         | TOTAL          | PRE                                 | CURING | CUIS         |          |                  |  |
| ING DEF<br>Ma<br><i>N</i> EEKLY I   |                | on plans               | ##  | FIE_D DENSITY, Ib/ff           |                       | DRY<br>B            | í            |       |       |       |   | 127.4         |       |       |       |       |   | 100.6         |       |       |       |   |  |                  |                |                                     |        |              |          |                  |  |
| WO YW   | CMENT          | COUNTY on plans        | REPORT NO. ##                                 |                                | E                     | WET                 |              |       |       | T     | I | 136.2         |       |       |       |       |   | 102.1         |       |       |       |   | 88   |                  | 00             |                                     |        |              |          |                  | ENGINEER   |
|   | C EMBANKMENT   |                        | RE  | DAYS<br>AFTER                  | FILL                  | TEST                |              |       |       | T     |   |               |       |       |       |       |   |               |       |       |       |   | 370,000  | 1/12<br>10.9     | 26,000         |                                     |        |              |          |                  | 1000   |
|   |                |                        |   |                                | SECTION               | REPRESENTED         | 0+00 - D+100 |       |       |       |   | 0+00 TC 0+10C |       |       |       |       |   | 0+00 TC 0+10C |       |       |       |   | yd <sup>a</sup> EMBANKMENT:<br>Di acen ppeviotistix. | PLACED THIS WEEK | TOTAL TO DATE: | ROLLERS USED (Make, Type, & Weight) | ls .   |              |          |                  | Joe Boss PE<br>Resident                                |
| <b>()</b>   | DEPURTMENT     | ERP Number             | ATION <b>On plans</b><br>ROAD <b>On Plans</b> |                                | STATION               | SAMPLED             | 0-50         |       |       |       |   | 0-50          |       |       |       |       |   | 0-50          |       |       |       |   | л с<br>Ē   |                  |                | s USED (Mal                         |        |              |          |                  | SUBMITTED BY Joe Boss PE                               |
|   | 9              | PRCJECT ERP Number     | LOCATION On plans<br>ROAD On Plans            | ТҮРЕ                           | ř.                    | Ω                   | B/N-E#1      |       |       |       |   |               |       |       |       |       |   |               |       |       |       |   |  |                  |                | ROLLERS                             | 6      |              | REMARKS: |                  | SUBM   |

WYDOT 213.0 (Rev. 09-16)

#### MOISTURE - DENSITY RELATIONS OF SOILS METHOD "C"

Scope: The following method will be used for soil with percent rock from 15% to 40%. If rock is determined to exceed 40%, compaction tests are not required in accordance with *WYDOT Standard Specifications* Section 203.4.3.1; place and compact material in accordance with *WYDOT Standard Specifications* Section 203.4.1.

The maximum dry density and optimum moisture is found by compacting several cylinders, each using the same compactive effort at different moisture contents. This method will incorporate the rock in the soil during the compaction of each cylinder.

## Apparatus: 1. Pans 15 inch, suggested

- 2. Rammer and guide, 5<sup>1</sup>/<sub>2</sub> lb, See Appendix A, WYDOT 213.0 for tolerances
- 3. Drying stove
- 4. Moisture tins
- 5. Trowel
- 6. Steel straightedge, 15 inch length minimum
- 7. No. 4 screen
- 8. Wooden block, suggest 2 inch x 4 inch
- 9. 0.03 ft<sup>3</sup> mold, See Appendices A & B, WYDOT 213.0 for tolerances.
- 10. Compaction block, 300 lb minimum
- 11. Extruder
- 12. Gram scale, sensitive to 0.1 g
- 13. 35 lb [15 kg] scale sensitive to 0.01 lb [5 g]
- 14. 100 ml graduated cylinder

#### Reference

| AASHTO T 99     | Standard Method of Test for Moisture-Density Relations of<br>Soils Using a 2.5-kg (5.5 lb) Rammer and a 305-mm (12-in.) |
|-----------------|---|
|                 | Drop  |
| WYDOT 203.4.1   | WYDOT Standard Specifications   |
| WYDOT 203.4.3.1 | WYDOT Standard Specifications   |
| WYDOT 212.0     | Sand Cone Method Field Density Test   |
| WYDOT 213.0     | Moisture – Density Relations of Soils Method "A"  |
| WYDOT 221.0     | Final Embankment  |
| WYDOT T-112     | Soils Compaction Worksheet  |
| *WYDOT T-113    | Weekly Report of Compaction of: Embankment  |
| WYDOT T-140     | Plotting Worksheet  |
|                 | WYDOT 203.4.1<br>WYDOT 203.4.3.1<br>WYDOT 212.0<br>WYDOT 213.0<br>WYDOT 221.0<br>WYDOT 7-112<br>*WYDOT T-113            |

\* Note: Use of weekly reports is optional

Sample: The percent rock, in any representative soil sample should be determined before any cylinders are compacted. If the sample is taken along with a field density test, *Sand Cone Method*, WYDOT 212.0, the percent rock is found as item "K" on Form T-112, *Soil Compaction Worksheet*.

To find the percent rock of a soil sample, screen either a representative portion of not less than 7 lb or screen the entire sample over a No. 4 screen. Weigh the material retained on the No. 4 screen.

Note: Coarse is defined as material retained on the No. 4 screen. For this procedure, percent rock is used to describe the percent of coarse material in a sample.

 $Percent Rock = \frac{Percent Retained on No. 4, lb}{Total Sample, lb}$ 

Example:

Sample = 7.58 lb Rock = 2.56 lb

 $\frac{2.56 \text{ lb}}{7.58 \text{ lb}} = 0.3377 \times 100 = 34 \% \text{ Rock}$ 

- Note: Use individual 7 lb samples for each cylinder to be compacted. Generally four cylinders are required to plot a curve, three cylinders under optimum moisture and one cylinder over optimum.
- Procedure: 1. Screen a sufficient amount of rock and soil to run four, 7 lb samples. The percent rock added to each 7 lb sample should remain the same as the original field sample. The material used as rock for each 7 lb sample should be rock, retained No. 4 material. Weigh and discard any rock remaining above the  $\frac{3}{4}$  inch sieve. Replace the plus  $\frac{3}{4}$  inch material with an equal amount of material passing the <sup>3</sup>/<sub>4</sub> inch sieve and retained on the No. 4 sieve. If additional rock is needed, use only material from the same test area or test hole. Large enough field samples should be taken so that you will have enough rock between the No. 4 sieve and <sup>3</sup>/<sub>4</sub> inch sieve to run four separate 7 lb samples.

Example: Calculation for percent rock in separate 7 lb samples.

34% Rock: 7 lb 
$$\times \frac{34}{100} = 2.38$$
 lb of Rock  
66% Soil: 7 lb  $\times \frac{66}{100} = 4.6$  lb of Soil

The separate 7 lb samples should be thoroughly mixed and covered until ready for use. Water should be added to each sample in sufficient amounts to increase the moisture by two percentage points for each cylinder.

Example:

5 ml per lb = 1%10 ml per lb = 2%

Using a 7lb sample, adding 2% moisture

7 lb 
$$\left(\frac{10 \text{ ml}}{\text{lb}}\right) = 70 \text{ ml}$$

- 2. With the prepared soil, fill the 0.03 ft<sup>3</sup> mold assembly (mold, base plate and collar) with the collar attached to  $\frac{1}{3}$  of the depth of the mold. Compact this layer with 25 uniformly distributed blows with the 5½ lb sleeve type rammer dropped free from a height of 12 inches above the soil. The mold base plate will rest on a compaction block of 300 lb or more, which is on a uniform rigid foundation. The next layer to be compacted is filled to  $\frac{2}{3}$  the depth of the mold and 25 uniformly distributed blows with the 5½ lb rammer. The last layer is placed in the mold to a depth equal to the first two and compacted with 25 blows of the rammer to a compacted depth of approximately 5 inches.
- 3. After the soil has been compacted, remove the collar from the mold assembly and carefully trim the compacted soil evenly with the top of the cylinder using the 15 inch straightedge. Fill holes that develop in the surface from the removal of rock material, with smaller size material. Wipe all loose material from the outside of the mold and base plate. Weigh the mold, base plate and compacted soil and record as item "V" on Form T-112.
- 4. Detach the base plate and remove the sample from the mold. The compacted soil is then sliced vertically through the center and a representative moisture sample of not less than 500 g is taken from one of the two cut faces, which includes all three lifts. Immediately weigh and record as item "L" (wet soil and tin) on Form T-112. Dry the moisture sample to a constant weight on a stove or in an oven, using care not to burn the sample. After the moisture sample has been taken, the rest of the 7 lb sample is discarded.
- 5. The next 7 lb sample is compacted with an incremented increase of two percent moisture, using the same procedure as outlined above, three equal layers with 25 blows of the  $5\frac{1}{2}$  lb rammer on each layer.

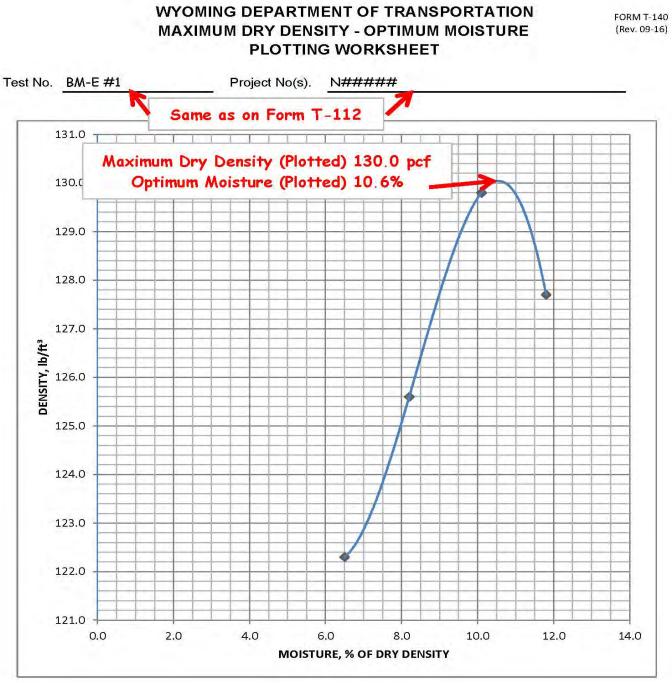
| Calculations: | A.    | Retained on No. 4 sieve   | 2.56 lb of Rock                                 |
|---------------|-------|---|---|
|               | B.    | Passing the No. 4 sieve   | 5.02 lb of Soil                                 |
|               | C.    | Weight of total sample  | 7.58 lb of Soil and<br>Rock                     |
|               | D.    | Percent of Rock,  | 34% of Rock<br>Aggregate (plus No. 4)           |
|               |       | Calculated: $\frac{A}{C} \times 100$  |   |
|               | E.    | Percent of Soil,  | 66% of Fines (minus<br>No. 4)                   |
|               |       | Calculated: $\frac{B}{C} \times 100$  |   |
|               | F.    | For a 7 lb sample,  | 2 lb of rock passing the <sup>3</sup> ⁄4 in and |
|               |       | Calculated: $\frac{D}{100} \times 7 \text{ lb}$                                 | retained on the No. 4                           |
|               | G.    | For a 7 lb sample,  | 4.63 lb of soil passing the No. 4               |
|               |       | Calculated: $\frac{E}{100} \times 7 \text{ lb}$                                 | sieve   |
|               | Note: | From the above calculations; $A = \text{item "}_{C}$<br>$C = \text{item "}_{C}$ | J" on Form T-112<br>I" on Form T-112            |

Report: Report weekly results on optional Form T-113, *Weekly Report for Compaction of Embankment*. See example Form T-113 in WYDOT 221.0.

D = item "K" on Form T-112

|          | Submitte                          | o(s).: N##<br>d By: <u>Resid</u><br>iken: 3 ft |                            | SOIL CO      | MPACT         | ION WO | DIZE     |                | -                      |                 |                 |                |
|----------|-----------------------------------|--|----------------------------|--------------|---------------|--------|----------|----------------|------------------------|-----------------|-----------------|----------------|
|          | Submitte<br>Depth Ta<br>n Represe | d By: Resid                                    |                            |              |               |        | πnə      | HEE            | I                      |                 |                 |                |
|          | Submitte<br>Depth Ta<br>n Represe | d By: Resid                                    | <i>!###</i>                |              |               |        |          |                | Met                    | hod "C" E       | xample          |                |
|          | Submitte<br>Depth Ta<br>n Represe | d By: Resid                                    | ####                       |              |               | Fie    | eld Te   | st No.:        | BM-E #1                |                 |                 |                |
|          | Depth Ta<br>n Represe             |  |                            |              |               | Statio | on San   | npled:         | STA 0+50               |                 |                 |                |
|          | Depth Ta<br>n Represe             |  | lent Engine                | er           |               |        |          | At:            | Resident Ei            | ngineer's T     | own             |                |
|          | n Represe                         |  |                            |              |               | Ver    | tical L  |                | 2 ft - 8 ft            | -               |                 |                |
|          |                                   |  | 0+00 to 0+                 | 100          |               |        | С        | ounty:         | Resident Ei            | ngineer's T     | own             |                |
| ·        | Date dam                          |  |                            |              |               | Dat    |          |                | XX/XX/XX               | -               |                 |                |
|          |                                   |  |                            |              |               |        |          |                |                        | •               |                 |                |
|          |                                   |  | Test                       | was made     |               | Same   |          | day(s)         | after fill w           | as placed.      |                 |                |
| A        | Density of                        | Standard S                                     | and, lbs/ft³               |              | 96.7          |        | Mo       | oisture        | Content (R             | oadway)         | Wt. of<br>Water | Wt. o<br>Drv S |
|          |                                   |  |                            |              |               |        | 1        | t Soil         | Dry Soil               | Tare of         | L - M           | M -            |
|          |                                   |  | Canad                      |              | 14.00         | 1      | and<br>L | Tin            | and Tin<br>M 700.3     | Tin<br>N 106.7  | P 38.6          |                |
|          |                                   | aratus and                                     | Sano<br>Unused Sa          | nd           | 16.33<br>7.21 |        | _        | 738.9<br>% Moi | M 700.3<br>sture, (P/C |                 | P 38.6          | Q 5<br>6,5     |
|          | Sand Used                         |  | unuseu sa                  | iu           | 9.12          |        | ĸ        | 76 WOI         | sture, (P/G            | () X 100        |                 | 0.0            |
| _        |                                   | to Fill Fun                                    | nel                        |              | 3.45          |        | S        | Wet D          | aneity lhe/f           | t³ ( (A x (* I) | ) / F           | 129.           |
|          |                                   | Hole (D - E                                    |                            |              | 5.67          |        |          |                |                        | k, letl=(       | -               |                |
| <u> </u> | Sand to Th                        |  | /                          |              | 0.07          |        |          |                | 5% - 40% Ro            |                 | 1-(3/3/)        | -              |
| G        | Wt. of Soil.                      | Coarse an                                      | d Containe                 | r            | 8.68          | 1      |          | 1011           | 376 - 4076 KO          | ick, icti-i     |                 |                |
|          |                                   | Container                                      |                            |              | 1.10          |        | Т        |                | Dry De                 | ensity lbs/ft   | 3               |                |
|          |                                   | d Coarse (0                                    |                            |              | 7.58          |        | · ·      |                | -                      | / (100 + R)     |                 | 121.           |
|          |                                   |  | ,                          |              |               | I      |          | ** For         |                        | ck, S = S x (   | 100 + (K/3))    |                |
| J        | Wt. of Coar                       | se Retaine                                     | d on #4 (4.7               | 75 mm)       | 2.56          |        |          |                |                        | nearest wh      |                 | r l            |
| K 9      | % of Coars                        | e, (J / I) x 1                                 | 00                         |              | 33.8          |        |          | ** For         | 15% - 40% R            | ock, let S =    | S x 100         |                |
|          | Mat 104 af                        | Soil and Mo                                    | -14                        |              |               | 13.86  |          | .05            | 14.26                  | 14.28           |                 |                |
|          | Tare Wt. of                       |  | Jiu                        |              |               | 9.52   |          | .05<br>52      | 9.52                   | 9.52            |                 | -              |
|          |                                   |  | ft <sup>3</sup> Mold (V    | - W)         |               | 4.34   | -        | 53             | 4.74                   | 4.76            |                 |                |
|          |                                   |  | s/ft <sup>3</sup> , Y x 30 | -            |               | 130.2  | +        | 5.9            | 142.2                  | 142.8           |                 |                |
|          |                                   |  | ty of Soil, It             |              |               |        |          | •              |                        |                 |                 |                |
|          |                                   | -  | Z x 100                    |              |               | 122.3  | 12       | 5.6            | 129.1                  | 127.7           |                 |                |
|          | (100 +                            |  |                            | or EE or FF) | )             |        |          |                |                        |                 |                 |                |
| мГ       | _                                 |  |                            |              |               |        |          |                | X Moi                  |                 |                 |                |
| o<br>i   | L                                 | м  | N                          | P<br>Wt. of  | Q<br>Wt. of   |        |          |                | (P/Q)                  | x 100           |                 |                |
| 5        | Wet Soil                          | Dry Soil                                       | Tare of                    | Water        | Dry Soil      |        |          |                |                        |                 |                 |                |
| •        | and Tin                           | and Tin  | Tin                        | L - M        | M - N         |        |          |                |                        |                 |                 |                |
| · ·      | 908.6                             | 859.6  | 105.1                      | 49.0         | 754.5         | 6.5    |          |                |                        |                 |                 |                |
| c        | 847.0                             | 790.8  | 105.5                      | 56.2         | 685.3         | AA     | 8        | 2              |                        |                 |                 |                |
| •        | 1032.9                            | 947.9  | 106.7                      | 85.0         | 841.2         |        | E        | 3B             | 10.1                   |                 |                 |                |
|          | 1035.4                            | 937.2  | 105.1                      | 98.2         | 832.1         |        |          |                | CC                     | 11.8            |                 |                |
| •        |                                   |  |                            |              |               |        |          |                |                        | DD              |                 |                |
| · [      |                                   |  |                            |              |               |        |          |                |                        |                 | EE              |                |
| _        |                                   |  |                            |              |               |        |          | -              |                        |                 |                 | FF             |
|          | -                                 | Aoisture %                                     |                            | Max Dry De   | -             | tt°    |          | -              | oisture % (·           | + or - )        | % Field Co      | -              |
|          | Plotted GG                        | 10.6   |                            | Plotted HH   | 150.0         |        | Optin    | num            | -4.1                   |                 | (T/HH)x100      | 93.            |
| _        | Method "C"                        |  | lling is needed.           |              |               |        |          |                |                        |                 |                 |                |

Tested By Tester's Name Certification No. ###



(Rev. 09-16)

Tested By Tester

## CHECK CURVE - EMBANKMENT (CC - E)

- Scope: This procedure is used to compare field calculated results of Method "A" or Method "C", maximum dry density and optimum moisture, with the results as determined by the Materials Program.
- Apparatus: 1. Pans 15 inch, suggested
  - 2. Rammer and guide, 5<sup>1</sup>/<sub>2</sub> lb, *See Appendix A, WYDOT 213.0 for tolerances*
  - 3. Drying stove
  - 4. Moisture tins
  - 5. Trowel
  - 6. Steel straightedge, 15 inch length minimum
  - 7. No. 4 screen
  - 8. Wooden block, suggest 2 inch x 4 inch
  - 9. 0.03 ft<sup>3</sup> mold, See Appendices A & B, WYDOT 213.0 for tolerances.
  - 10. Compaction block, 300 lb minimum
  - 11. Extruder
  - 12. Gram scale, sensitive to 0.1 g
  - 13. 35 lb [15 kg] scale sensitive to 0.01 lb [5 g]
  - 14. 100 ml graduated cylinder

#### Reference

| Documents: | WYDOT 213.0 | Moisture – Density Relations of Soils Method "A" |
|------------|-------------|--|
|            | WYDOT 214.0 | Moisture – Density Relations of Soils Method "C" |
|            | WYDOT T-112 | Soils Compaction Worksheet                       |
|            | WYDOT T-120 | Sample Transmittal                               |
|            | WYDOT T-140 | Plotting Worksheet                               |

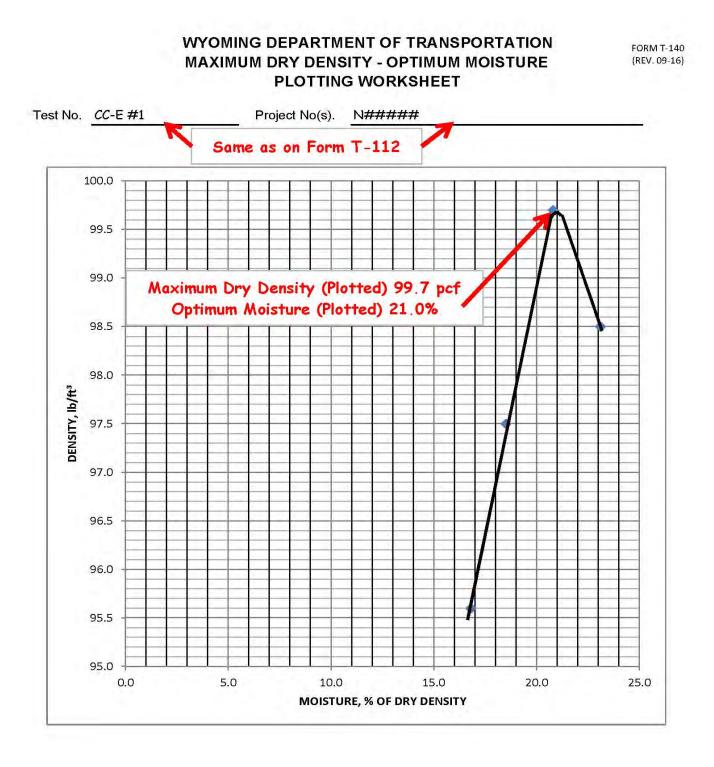
Sample: Sometime during the first few weeks of construction, coordinate with Field Services Inspector, then secure a representative soil sample, enough material for two compaction tests. Thoroughly mix the material and split. Run a compaction test, either Method "A" or Method "C", on one half of the material and send the other half to the Materials Program. If the sample has over 15% rock, separate 7 lb samples are used; enough material should be sent to the Materials Program to run at least four of these 7 lb samples. At least 90 lb of material should be sent to the Materials Program if there is a large amount of material above the 2 inch sieve.

Submit a completed Form T-120, *Sample Transmittal*, with each sack. Additionally, complete a Form T-112, *Soil Compaction Worksheet*, and the corresponding Form T-140, *Maximum Dry Density – Optimum Moisture Plotting Worksheet*, to accompany each sample sack. See Example T-112 and T-140 of this section.

Procedure: Method "A" will be used for samples with less than 15% rock (WYDOT 213.0) or Method "C" for samples with over 15% rock (WYDOT 214.0). Additional compaction curves may be sent to the Materials Program as desired or needed. At least one check curve (CC) should be sent in by each field tester during construction, usually at the start of the project.

| PARTME | MT            |                                |                   |                  |                   |  |         |                |                        |                            |             |         |            |    |
|--------|---------------|--------------------------------|-------------------|------------------|-------------------|--|---------|----------------|------------------------|----------------------------|-------------|---------|------------|----|
|        |               |                                |                   |                  |                   | F  | ield Te | st No.:        | BM-E #1                |                            |             |         | _          | 5  |
|        | Project N     | o(s).: N##                     | ###               |                  |                   | Stati  | ion Sa  | mpled:         | STA 0+50               |                            |             |         |            |    |
|        | Submitte      | d By: Reside                   | ent Enginee       | er               |                   |  |         | At             | Resident E             | ngineer's T                | own         |         |            | j) |
|        | Depth T       | aken: 3 ft                     |                   |                  |                   | Ve   |         |                | 2 ft - 8 ft            |                            |             |         |            | į, |
| Sect   | ion Represe   | ented: STA (                   | 0+00 to 0+1       | 00               |                   |  | C       | county:        | Resident E             | ngineer's T                | own         |         |            | 2  |
|        | Date Sam      | pled: XX/X                     | X/XX              |                  |                   | Da   | ate Ree | ceived:        | XX/XX/XX               | (                          |             |         |            | i. |
|        |               |                                | Test              | was made         |                   |  |         | _day(s         | ) after fill wa        | is placed.                 |             |         |            |    |
| A      | Density of S  | tandard Sand                   | 11-74-3           |                  |                   |  | N       | loistur        | e Content (R           | loadway)                   | Wt. o       | fWater  | W          |    |
| A      | Density of 3  | tanuaru sanu                   | , 10/1C           |                  |                   |  | Wet s   | JON STREET     | Dry Soil and<br>Tin, g |                            | L.          | M, g    | Dry<br>M - |    |
| в      | Wt. of Appa   | ratus and San                  | id, Ib            |                  |                   |  | L       |                | M                      | N                          | P           |         | Q          |    |
| С      |               | ratus and Unu                  |                   | b                |                   |  | R       | % Moi          | sture, (P/Q)           | x 100                      |             |         |            |    |
| D      | Sand Used (   | B - C), lb                     |                   |                  |                   |  | 2       |                |                        |                            |             |         |            | _  |
| Е      | Wt. of Sand   | to Fill Funnel                 | , Ib              |                  | []                |  | S       | Wet D          | ensity, lb/ft³ (       | (A x (* l) ) / l           | F           |         |            |    |
| F      | Sand to Fill  | Hole (D - E), I                | b                 |                  |                   |  | 100     | * For (        | 0% - 15% Roci          | <pre>c, let l = ( l</pre>  | - (J / 3) ) | K       | -          |    |
|        | in a second   |                                |                   |                  |                   |  |         | * For 1        | 15% - 40% Roo          | ≫k,leti=i                  | -           | -       |            |    |
| G      |               | Rock and Con                   | itainer, Ib       |                  |                   |  | (       | r -            |                        | 27 1.01-1.02.02.0          |             |         |            | _  |
| H      | Tare Wt. of ( |                                | n                 | _                |                   |  | T       | -              |                        | Density Ib/ft <sup>a</sup> | -           |         |            |    |
| 4      | wt. Soll and  | Rock (G - H),                  | di                |                  | 25.14             |  |         | tt For         | 0% - 15% Roc           | S / (100 + R)              | 00 + ///    | 211     | -          | _  |
| J      | With of Rock  | (Retained on                   | No (1) Ib         | -                | 2.24              |  |         | 1. 10 March 1. |                        |                            |             | 5))<br> |            |    |
| ĸ      | % of Rock, (  |                                | 110. 47, 10       | -                | 8.9               | where (K/3) is to nearest whole number<br>** For 15% - 40% Rock, let S = S x 100 |         |                |                        |                            |             |         |            |    |
|        | 1.4           |                                |                   |                  |                   |  |         | <u></u>        |                        |                            |             | -       |            |    |
| ۷      | Wet Wt. of S  | oil and Mold,                  | lb                |                  |                   | 13.32  | 1       | 3.47           | 13.60                  | 13.64                      |             | 1       | -          | -  |
| W      | Tare Wt. of I | Viold, Ib                      |                   |                  |                   | 9.60   | 9       | 9.60           | 9.60                   | 9.60                       |             |         | _          |    |
| Y      | Wet Wt. of S  | in 1/30 ft <sup>s</sup>        | Mold (V - V       | V), Ib           |                   | 3.72   | 3       | 8.87           | 4.00                   | 4.04                       | 1 42 7      |         | _          |    |
| z      | Wet Density   | of Soil, Ib/ft3,               | Y x 30, lb        |                  |                   | 111.6  | 1       | 16.1           | 120.0                  | 121.2                      |             |         |            |    |
|        |               |                                | ity of Soil, Ib   | ft <sup>3</sup>  |                   | 2412   | 1       | 22             | 1.22                   | 1.00                       | 1           |         |            |    |
|        |               | and the star star for the star | 2 x 100           | 1.22             | <u>-</u> 8,       | 95.6   | 9       | 7.5            | 99.3                   | 98.5                       |             |         |            |    |
| -      | (100 -        | + (AA or BB o                  | r CC or DD o      | or EE or FF))    |                   |  | -       | -              |                        |                            | -           | -       | -          |    |
| M      | L             | м                              | N                 | Р                | Q                 |  |         |                |                        | ure (P/Q)<br>100           |             |         |            |    |
| Ĩ      | Wet Soil      | Dry Soil                       |                   | Wt. of           | Wt. of            |  |         |                |                        |                            |             |         |            |    |
| s<br>t | and Tin, g    | and Tin, g                     | Tare of<br>Tin, g | Water            | Dry Soil          |  |         |                |                        |                            |             |         |            |    |
| u<br>r | 203.5         | 180.3                          | 42.1              | L - M, g<br>23,2 | M - N, g<br>138,2 | 16.8   |         |                |                        |                            |             |         |            |    |
| e      | 203.5         | 220.2                          | 42.1<br>53.5      | 31.7             | 138.2             | 16.8<br>AA   | 1       | 9.0            | -                      |                            |             |         |            |    |
| c      | 229.5         | 197.2                          | 42,1              | 32.3             | 155.1             |  | -       | BB             | 20.8                   |                            |             |         |            |    |
| o<br>n | 234.7         | 200.7                          | 53.5              | 34.0             | 147.2             |  |         |                | CC                     | 23.1                       |             | _       |            |    |
| t<br>e | -9.07         | 200.7                          | 50.0              |                  |                   |  | _       |                |                        | DD                         |             | -       |            |    |
| n<br>t |               |                                |                   |                  |                   |  |         |                |                        |                            | F           | E       | 1          | -  |
| ·      |               |                                |                   |                  |                   |  |         |                | · · · · · ·            |                            |             | -       | D          | F  |
|        | Optimum Me    |                                |                   | Max Dry De       |                   |  |         |                | oisture % ( + o        | r - )                      |             | d Compa |            | 1  |
|        | Plotted GG    | 21.0                           |                   | Plotted HH       | 99.7              |  | Optin   | num            |                        |                            | (T/HH)      | x100    |            |    |

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## FAMILY OF CURVES

Scope: This procedure is used to develop a series of several four point maximum dry density and optimum moisture curves of similar soils. A family of curves is a group of typical soil moisture-density relationships determined using WYDOT 213.0 and WYDOT 214.0, which reveal certain similarities and trends characteristics of the soil type and source. Soils sampled from one source will have many different moisture-density curves, but if a group of these curves are plotted together certain relationships usually become apparent.

#### Intent

For Use: Repeating the compaction process for several different types of cohesive-soils will result in curves of similar shape and geometry. By plotting these curves on one sheet, a family of curves may be used to estimate the maximum dry density and optimum moisture content of a similar cohesive-soil sample in the field based on one point. To use the "one point" method based on the family of curves, the "one point" must fall on one of the established curves.

## Apparatus: 1. Pans 15 inch, suggested

- 2. Rammer and guide, 5<sup>1</sup>/<sub>2</sub> lb, *See Appendix A, WYDOT 213.0 for tolerances*
- 3. Drying stoves
- 4. Moisture tins
- 5. Trowel
- 6. Steel straightedge, 15 inch length minimum
- 7. Wooden block, suggest 2 inch x 4 inch
- 8. 0.03 ft<sup>3</sup> mold, See Appendices A & B, WYDOT 213.0 for tolerances.
- 9. Compaction block, 300 lb minimum
- 10. Extruder
- 11. Gram scale, sensitive to 0.1 g
- 12. 35 lb [15 kg] scale sensitive to 0.01 lb [5 g]
- 13. 100 ml graduated cylinder

#### Reference

| Documents: | AASHTO T 272 | Standard Method of Test for Family of Curves - One Point Method |
|------------|--------------|---|
|            | WYDOT 213.0  | Moisture – Density Relations of Soils Method "A"                |
|            | WYDOT 214.0  | Moisture – Density Relations of Soils Method "C"                |
|            | WYDOT T-140  | Plotting Worksheet  |

Sample: Take representative soil samples large enough to be used in the compaction of four point curves. When you encounter large amounts of 2 inch material, then at least 90 lb will be needed to get enough rock between the retained on No. 4 sieve and the passing <sup>3</sup>/<sub>4</sub> inch sieve for three 11 lb samples.

Procedure: After the completion of several Method "A" (WYDOT 213.0) or Method "C" (WYDOT 214.0) Moisture-Density tests, plot as many of the completed four point maximum dry density and optimum moisture curves as possible onto Form T-140, *Plotting Worksheet*.

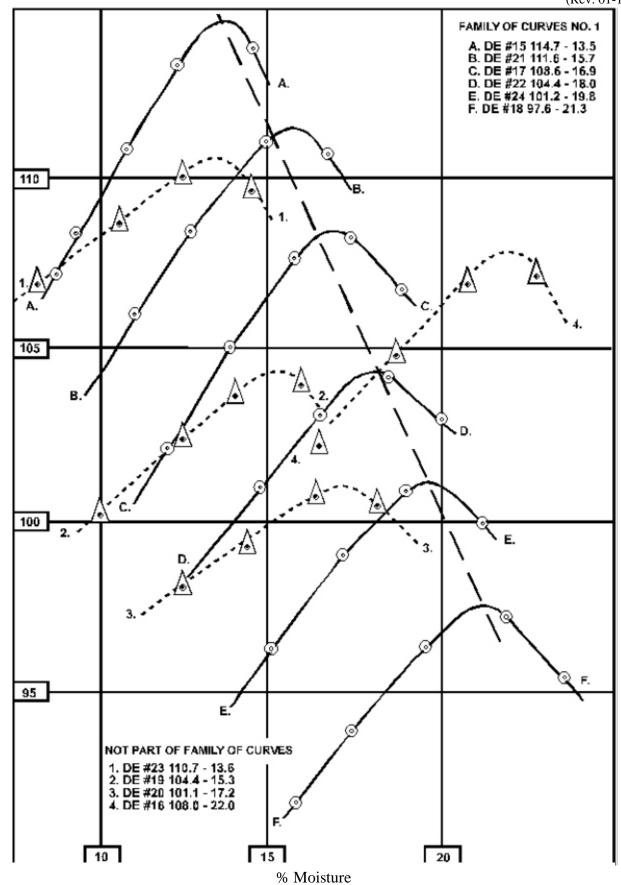
The curves used to make a family will be curves of similar soils typically cohesive, which when plotted will have a tendency to peak in somewhat of a straight line. Curves that do not fall onto this alignment perfectly could still be in the same family if, in the judgment of the technician, the deviation from alignment is not too great. Any curves which obviously do not fit the alignment could possibly be used in the development of other families. A family of curves should consist of at least five curves so that a maximum range can be utilized.

When a family of curves has been developed and is being used, forward a copy to the Materials Program. As additional curves are added to the family or other families developed, send copies of these to the Materials Program.

A family of curves can be developed gradually while taking construction density tests on a regular basis.

Example: On the Form T-140 of this section, "A" through "F" were taken from a set of ten curves. The six curves used to make up this family all have the same dry density slope as compared to curves numbers one through three. The dry density slope is as important as the peaks in developing a family. Curves one through three can be used as the beginning of another family which can be developed as other curves are compacted.

WYDOT 217.0 (Rev. 01-15)



Density, pcf

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#### **REFERENCE TEST**

- Scope: The following method is intended to reduce the number of compacted cylinders needed in calculating maximum dry density and optimum moisture of soils from four cylinders to two cylinders. See *Family of Curves* (WYDOT 217.0).
- Apparatus: 1. Pans 15 inch, suggested
  - 2. Rammer and guide, 5<sup>1</sup>/<sub>2</sub> lb, *See Appendix A, WYDOT 213.0 for tolerances*
  - 3. Drying stoves
  - 4. Moisture tins
  - 5. Trowel
  - 6. Steel straightedge, 15 inch length minimum
  - 7. No. 4 screen
  - 8. Wooden block, suggest 2 inch x 4 inch
  - 9. 0.03 ft<sup>3</sup> mold, See Appendices A & B, WYDOT 213.0 for tolerances.
  - 10. Compaction block, 300 lb minimum
  - 11. Extruder
  - 12. Gram scale, sensitive to 0.1 g
  - 13. 35 lb [15 kg] scale sensitive to 0.01 lb [5 g]
  - 14. 100 ml graduated cylinder

#### Reference

| Documents: | WYDOT 212.0 | Sand Cone Method Field Density Test              |
|------------|-------------|--|
|            | WYDOT 213.0 | Moisture – Density Relations of Soils Method "A" |
|            | WYDOT 214.0 | Moisture – Density Relations of Soils Method "C" |
|            | WYDOT 217.0 | Family of Curves                                 |
|            | WYDOT T-112 | Soil Compaction Worksheet                        |
|            | WYDOT T-140 | Plotting Worksheet                               |

- Sample: Representative soil samples for this type of test are usually taken as part of a *Sand Cone Method Field Density Test*, (WYDOT 212.0).
  - Note: Always take large enough samples so that four cylinder maximum dry density and optimum moisture curves can be tested if needed.
- Procedure: Determine the percent rock in the soil samples by weighing the sample, then screening the sample carefully over the No. 4 screen. Weigh the plus No. 4 material, and divide the total weight of the sample into the weight of retained on the No. 4 screen. If the soil sample is taken as part of a "Field Density Test", sand cone method, then the percent rock is item "K" on Form T-112, *Soil Compaction Worksheet*.

With the percent rock determined, determine the percent of moisture in the sample, using not less than 100 g of Method "A" for rock between 0% to 15% or not less than 500 g for a Method "C" for rock between 15% to 40%. When using a Method "C", incorporate the rock back into the moisture sample at the same percentage as found in the original field sample.

<u>Mix</u> enough material for two separate 7 lb samples, one usually at field moisture and the other at plus or minus 2% from field moisture. If the sample is taken as part of a "Field Density Test" sand cone method, then one of the two samples will be material from the test hole, and the other 7 lb sample will be material taken from around the test hole.

Enough material should always be taken and <u>mixed</u> to run four compaction cylinders if necessary.

If the percent rock falls between 0% to 15%, then *Method "A"*, (WYDOT 213.0) procedure is followed for the compaction of two cylinders. If the percent rock is between 15% to 40%, then *Method "C"*, (WYDOT 214.0) procedure is used for the compaction of two cylinders. The difference is that rock over 15% is incorporated back into the 7 lb sample during compaction in the 0.03 ft<sup>3</sup> mold.

After the two cylinders have been compacted, plot the dry density and the moisture for each cylinder onto Form T-140, *Plotting Worksheet*, a maximum dry density and optimum moisture curve. The curve selected should be of similar soil and from the same general area. If the dry density and moisture for each cylinder does not plot very close to the curve you select, and you are not using a Family of Curves, it may be necessary to choose from other curves of similar soil already compacted. If none of the curves available come very close, then a new curve should be compacted using the remaining two, 7 lb samples.

When the proper curve is selected, use the maximum dry density and optimum moisture from that curve as item "HH" and "GG" on Form T-112. Under "Remarks" on Form T-112, the test number that the maximum dry density and optimum moisture were taken from should be indicated.

When referencing two cylinders to a Family of Curves, and the two cylinders fall between two plotted curves of the same family, one of two procedures can be followed:

- 1. Use either interpolation of the data between the two curves or,
- 2. Completion of the compaction test.

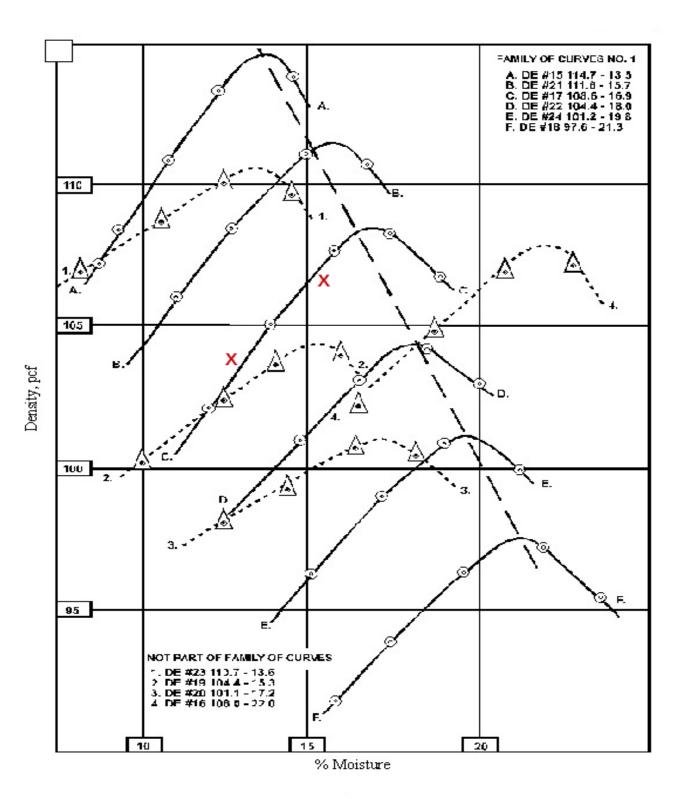
Completion of the compaction test is the preferred procedure as this will add another curve to the family, thereby furnishing more accurate data for future referencing of tests.

Rock correction (to nearest whole number) =

 $\frac{Percent Rock}{3}$ 

Example: Dry Density #1, 104.1 pcf @ 12.5% moisture Dry Density #2, 105.9 pcf @ 15.3% moisture

From family of curve (C), Dry Density 108.0 pcf @ 16.2% moisture



3

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| Failure           |     | Possible Reason  |                      | Possible Correction   |
|-------------------|-----|--|----------------------|---|
| Low<br>Compaction | 1.  | Moisture not mixed evenly<br>into soil.  | a.<br>b.<br>c.<br>d. | Pre-wetting of cuts by sprinklers or<br>water trucks.<br>Cultivation of soil by disk, harrow,<br>grader, pad foot roller, etc.<br>Allow to cure for longer period of<br>time when pre-wet (up to 36 days,<br>depending upon conditions and<br>types of soils).<br>Rotary mixer. |
|                   | 2.  | Moisture above optimum<br>(see section on Embankment<br>Control under "Watering"). | a.<br>b.             | Cultivation of soil and air drying.<br>Addition of drier soil and mix.  |
|                   | 3.  | Moisture below optimum<br>(see section on Embankment<br>Control under "Watering"). | a.                   | Addition of water by truck or sprinklers and mix.   |
|                   | 4.  | Not enough rolling/compaction.   | a.<br>b.<br>c.<br>d. | Add additional rolling equipment.<br>Speed rollers to 3 to 5 mph<br>maximum.<br>Cut down on earth hauling<br>equipment.<br>Decrease lift thickness.   |
|                   | 5.  | Rolling equipment too light.   | a.                   | Weigh rollers and check manufacturers' specifications.  |
|                   | 6.  | Speed of rollers and number of passes insufficient.                                | a.                   | Adjust accordingly (See<br>Embankment Control under<br>"Rolling").  |
|                   | 7.  | Lifts too thick.   | a.                   | Decrease lift thickness.  |
|                   | 8.  | Large, hard "dirt clods".  | a.<br>b.             | Use pad foot roller to break up.<br>Allow longer curing period if pre-<br>wet.  |
|                   | 9.  | Weight of roller, 50 T, is shearing soils.   | a.                   | Reduce the weight down to 35 T to 40 T or use other type of roller.   |
|                   | 10. | Vibratory rollers must have a firm foundation to work on.                          | a.                   | Compact a foot or more with other<br>type of roller before placing<br>vibratory roller.   |

## CONTROL OF EMBANKMENT DURING CONSTRUCTION

| Failure  | Possible Reason   | Possible Correction  |  |  |  |
|--|---|--|--|--|--|
| Spongy<br>Surface,<br>Ravelling  | <ol> <li>Excessively wet condition<br/>below grade.</li> </ol>                          | <ul> <li>a. Sub-excavate and backfill with suitable bridging material and provide adequate drainage.</li> <li>b. <i>For example</i>: Lower water table with the use of drain pipes or by cutting borrow ditches deeper.</li> </ul> |  |  |  |
|  | 2. Expansive or non-<br>compactable soils.  | a. Sub-excavate and backfill with suitable material.   |  |  |  |
| <b>NOTE:</b> In the above two conditions the use of coarse graded material (gravel) should not be used because of the ponding or "bathtub" condition which may be created. |   |  |  |  |  |
| Layering<br>(Wet & Dry)  | <ol> <li>Improper mixing or mixing<br/>equipment not mixing deep<br/>enough.</li> </ol> | a. Use additional mixing equipment.  |  |  |  |

#### FINAL EMBANKMENT

- Scope: This recommended procedure sets forth a recognized method by which a soil sample of construction embankment is taken from the top 2 ft below the surfacing (upper 2 ft of the roadbed) and submitted to the Materials Program.
- Apparatus: 1. Shovel 2. Pick 3. Sample sacks 4. Form T-112

Reference

| Documents: | WYDOT T-112  | Soils Compaction Worksheet                 |
|------------|--------------|--|
|            | *WYDOT T-113 | Weekly Report of Compaction of: Embankment |
|            | WYDOT T-128  | Construction Test Requirements             |

\* Note: Use of weekly reports optional

Procedure: Soil samples from the top 2 ft of embankment are needed to get a comparison between soils anticipated during the preliminary design and soils found in actual construction. The intent is to sample subgrade which is defined as native soils or borrow soils within the top 2 ft below the surfacing. If Borrow Special Excavation (BSE) is 24 inches or greater, it will be considered as subgrade. If the BSE is less than 24 inches, then the 2 ft below the BSE will be considered to be the subgrade. Materials used in the structural design, such as subbase, are not considered to be subgrade.

A minimum of one soil sample should be taken for each 0.5 mile of roadway throughout the project when the soil in the top 2 ft of roadway remains basically the same. Any change in soil type requires at least one sample for each change. If more than one soil change is encountered in the top 2 ft of fill, a sample should be taken of each type, along with the vertical limits, as outlined on the example Form T-112 of this section.

The minimum number of samples needed for each project can be found on Form T-128, *Construction Test Requirements* sent out for each project.

All samples should be sent to the Materials Program as soon as possible so that the engineer can be advised of any increase or reduction in design surfacing thickness.

Each sample will consist of one completely full sack of material.

- Note: This information is included with the test result data on the soils profile for future pavement design and analysis; completing all fields is important for future reference.
- Report: Report weekly results on optional Form T-113, Weekly Report for Compaction of: Embankment.



# WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SOIL COMPACTION WORKSHEET

**T-112** (Rev. 09-16)

| DEPARTMEN | NT                     |                             |                   |               |               |       |          |                   |                        |                            |   |                    |
|-----------|------------------------|-----------------------------|-------------------|---------------|---------------|-------|----------|-------------------|------------------------|----------------------------|---|--------------------|
|           |                        |                             |                   |               |               | Fi    | eld Te   | st No.:           | BM-E #1                |                            |   |                    |
|           | Project N              | lo(s).: <u>N#</u> #         | ###               |               |               | Stati | on Sa    | mpled:            | STA 0+50               |                            |   |                    |
|           | Submitte               | d By: Resid                 | lent Engine       | er            |               |       |          | At:               | Resident Er            | ngineer's To               | wn                                      |                    |
|           | Depth T                | aken: <u>3 f</u> t          |                   |               |               | Ve    | rtical   | Limits:           | 2 ft - 8 ft            |                            |   |                    |
| Sect      | ion Represe            | ented: STA                  | 0+00 to 0+1       | 100           |               |       | С        | county:           | Resident Er            | ngineer's To               | wn                                      |                    |
|           | Date Sam               | pled: XX/>                  | (X/XX             |               |               | Da    | te Red   | ceived:           | XX/XX/XX               |                            |   |                    |
|           |                        |                             | Tes               | t was made    |               |       |          | _day(s)           | ) after fill wa        | s placed.                  |   |                    |
| А         | Density of S           | itandard Sand               | d, Ib/ft³         |               |               |       |          |                   | e Content (R           |                            | Wt. of Water                            | Wt. of<br>Dry Soil |
|           |                        |                             |                   |               |               |       |          | Soil and<br>in, g | Dry Soil and<br>Tin, g | Tare of<br>Tin, g          | L - M, g                                | M - N, g           |
| в         | Wt. of Appa            | ratus and Sa                | nd, Ib            |               |               |       | L.       | , g               | M                      | N                          | P                                       | Q                  |
| с         |                        | ratus and Un                | 1107              | b             |               |       | R        | % Mois            | sture, ( P / Q)        | x 100                      |   |                    |
| D         | Sand Used (            | (B - C), Ib                 |                   |               |               |       |          |                   |                        |                            |   |                    |
| E         | Wt. of Sand            | to Fill Funne               | l, lb             |               |               |       | S        | Wet De            | ensity, Ib/ft³ (       | (A x (* l) ) / F           |   |                    |
| F         | Sand to Fill           | Hole (D - E),               | lb                |               |               |       |          | * For 0           | % - 15% Rock           | ., let I = (I -            | (J / 3) )                               |                    |
| -         |                        |                             |                   |               |               |       |          | * For 1           | 5% - 40% Roc           | ⊧k, let I= I               |   |                    |
| G         | Wt. of Soil,           | Rock and Co                 | ntainer, Ib       |               |               |       |          |                   |                        |                            |   |                    |
| Н         |                        | Container, Ib               | 1.19.00           |               |               |       | T        | 4                 |                        | Density Ib/ft <sup>3</sup> |   |                    |
| 1         | Wt. Soil and           | Rock (G - H)                | , Ib              |               |               |       |          |                   |                        | \$ / (100 + R)             |   |                    |
| <u> </u>  |                        |                             |                   |               |               |       |          |                   | 0% - 15% Roc           | a (*                       |   |                    |
| J         |                        | (Retained on                | NO. 4), ID        |               |               |       |          |                   | (K/3) is to nea        | the second second          | 2 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A |                    |
| к         | % of Rock, (           | J / I) X 100                |                   |               |               |       |          | ** For            | 15% - 40% Ro           | CK, IEL 5 = 5 )            | K 100                                   |                    |
| v         | Wet Wt. of S           | Soil and Mold               | , Ib              |               |               |       |          |                   |                        |                            |   | 9                  |
| W         | Tare Wt. of            | Mold, Ib                    |                   |               |               |       |          |                   |                        |                            |   | ÷                  |
| Y         | Wet Wt. of S           | Soil in 1/30 ft³            | Mold (V - V       | V), Ib        |               |       |          |                   |                        |                            |   |                    |
| z         | Wet Density            | of Soil, Ib/ft <sup>s</sup> | , Y x 30 , Ib     |               |               |       |          |                   |                        |                            |   |                    |
|           |                        | Dry Dens                    | ity of Soil, It   | o ft°         |               |       |          |                   |                        |                            |   |                    |
|           | -                      | MALE 25 10 10 10 10 10      | Z x 100           |               | -31           |       |          |                   |                        |                            |   |                    |
|           | (100                   | + (AA or BB o               | or CC or DD       | or EE or FF)) |               |       |          |                   |                        |                            |   |                    |
| м         | <u> </u>               |                             | N                 | _             |               |       |          |                   | % Moistu               |                            |   |                    |
| o<br>i    | L                      | М                           | N                 | P<br>Wt.of    | Q<br>Wt.of    |       |          |                   | × 1                    | 00                         |   |                    |
| s<br>t    | Wet Soil<br>and Tin, g | Dry Soil<br>and Tin, g      | Tare of<br>Tin, g | Water         | Dry Soil      |       |          |                   |                        |                            |   |                    |
| u         | and m, g               | anu m, g                    | ini, g            | L - M, g      | M - N, g      |       | 4        |                   |                        |                            |   |                    |
| r<br>e    |                        |                             |                   |               |               |       | <u> </u> |                   |                        |                            |   |                    |
| с         |                        |                             |                   |               |               | AA    |          |                   |                        |                            |   |                    |
| o<br>n    |                        |                             |                   |               |               |       |          | BB                |                        |                            | 4                                       |                    |
| t<br>e    |                        |                             |                   |               |               |       |          |                   | CC                     | DD                         |   |                    |
| n         |                        |                             |                   |               |               |       |          |                   |                        | DD                         | EE                                      |                    |
| t         |                        |                             |                   |               |               |       |          |                   |                        |                            |   | FF                 |
|           | Optimum M              | oisture %                   |                   | Max Dry Der   | nsity, Ib/ft³ |       | Road     | way Mo            | isture % ( + o         | r - )                      | % Field Compa                           |                    |
|           | Plotted GG             | <u>.</u>                    |                   | Plotted HH    |               |       | Optin    | num               | е<br>5                 |                            | (T/HH)x100                              |                    |
| Remarks   | This material          | will be the sam             | e throughout t    | his section.  |               |       |          |                   | n 6                    |                            | 12                                      |                    |

Tested By Tester Certification No. ###

| Č                                 | . 22                                   |   |                                 | Ŵ                         | OMING D   | EPARTM                  | ENT OF .  | WYOMING DEPARTMENT OF TRANSPORTATION                   | <b>STATION</b>  |                               |                    |  |   | T.113        |
|-----------------------------------|--|---|---------------------------------|---------------------------|---|-------------------------|---|--|---|-------------------------------|--------------------|--|---|--------------|
| K                                 | - Standy                               |   |                                 |                           |   | Materials <sup>-</sup>  | Materials Testing Laboratory                              | oratory  |   |                               |                    |  | Ð   | (Rev. 09-16) |
|                                   | 5)                                     |   |                                 |                           | WEEKLY  | REPORT                  | FOR CO  | WEEKLY REPORT FOR COMPACTION OF :                      | 4 OF :  |                               |                    |  |   |              |
|                                   |  | ×   | X EMBANKMENT                    | IENT                      | 754   | CRUSHED BASE            | BASE  |  |   | Ĭ                             | OTHER              |  |   |              |
| PROJECT<br>LOCATION               | PROJECT N######<br>OCATION Resident En | aineer's Town   | RE                              | COUNTY<br>PORT NO.        | COUNTY County of Project<br>REPORT NO. This Report Number | Project<br>1 Number     |   |  | DATE  | DATE <u>Beginning Of</u> Week | f Week             | ę  | Ending Of Week                              | ÷            |
| ROAD                              | As Per Plans                           | ROAD As Per Plans   | 8                               |                           |   |                         |   | 0  | 122   | DATE REC'D IN LABORATORY      | DIN LABC           | DRATORY                                      |   |              |
| TYPE                              |  |   | DAYS<br>AFTER                   |                           | FIELD DENSITY, IbAff                                      | ISITY, Ib <i>M</i> ⁵    |   | %<br>WATER   | LAB, OR TYPICA<br>CURVE VALUE   | <u> </u>                      | *                  | WATER<br>%PTS.                               | PERCENT                                     |              |
| OF TEST<br>AND<br>TEST<br>NIIMBER | STATION<br>SAMPLED                     | SECTION<br>REPRESENTED                                    | FILL<br>PLACED<br>TEST<br>TAKEN | FI<br>WET<br>A            | FILL<br>DRY<br>B  | CYLII<br>WET<br>C       | CYLINDER<br>ET DRY  | IN FILL<br>OR<br>CYLINDER                              | OPTIMUM DENSITY<br>WATER DRY<br>% IbAt  |                               | L COARSE           | + OR -<br>FROM<br>OPTIMUM<br>I               | COMPACTION TESTED BY:<br>FILL<br>/R/Giv 100 | TESTED BY:   |
| As Required                       | Station                                | As Per Plans  | Same                            | Ę)                        | Too Rocky   | Too Rocky For Density   | -   | J  | -   | ,                             | 42.2               | -  |   | 1            |
|                                   |  |   |                                 |                           | Test Repr   | esents Abo              | Test Represents About 4,000 C.Y                           | Y.   |   |                               |                    |  |   |              |
|                                   |  |   |                                 |                           |   |                         |   |  |   |                               |                    |  |   |              |
| As Required                       | Station                                | As Per Plans  | 1                               | 134.6                     | 125.6   |                         |   | 7.5  | 11.3  | 124.9                         | 30.3               | -3.8   | 100.6                                       |              |
|                                   |  |   |                                 |                           |   | 131.4                   | 122.5   | 7.3  | The second |                               |                    |  |   |              |
|                                   |  |   |                                 |                           |   | 135.6                   | 123.6   | 9.7  |   |                               |                    |  |   |              |
|                                   |  |   |                                 |                           |   | 139.0                   | 124.9   | 11.3   |   |                               |                    |  |   |              |
|                                   |  |   |                                 |                           |   | 138.8                   | 122.2   | 13.6   |   | T                             |                    |  |   |              |
|                                   |  |   |                                 |                           |   |                         |   |  |   |                               |                    |  |   |              |
| As Required                       | Station                                | As Per Plans  | Same                            | 123.7                     | 112.0   |                         |   | 10.4   | 11.5  | 112.6                         | 14.2               | -1.1   | 5.99  |              |
|                                   |  |   |                                 |                           |   | 124.0                   | 112.6   | 10.1   |   |                               |                    |  |   |              |
|                                   |  |   |                                 |                           |   | 127.4                   | 113.1   | 12.6   | Referenced to curve "A" Set 1   | to curve "                    | A" Set 1           |  |   |              |
|                                   |  |   |                                 |                           |   |                         |   |  |   |                               |                    |  |   |              |
| As Required                       | Station                                | As Per Plans  |                                 | This mate                 | rial will be  | the same t              | hroughout 1   | This material will be the same throughout this section |   |                               |                    |  |   |              |
|                                   |  |   |                                 |                           |   |                         |   |  |   |                               |                    |  |   |              |
|                                   |  |   |                                 |                           |   |                         |   |  |   |                               |                    |  |   |              |
|                                   |  | yd <sup>s</sup> EMBANKMENT:                               | 000,070                         | 00                        |   | M. GAI                  | M. GALS WATER   |  | 27.8  | -                             |                    | _0T  | TOTAL TESTS                                 |              |
|                                   | PLAC                                   | PLACED PREVIOUSLY:  | 400,000 +                       | 400.000 + 280.000         |   | USED PR                 | USED PREVIOUSLY   |  | 22.3  |                               |                    |  | REO'D                                       | TAKEN        |
|                                   | ЪГ                                     | PLACED THIS WEEK:   | 52,300                          | 52,300 + 4,000            |   | USED T                  | USED THIS WEEK  |  | 0.8   | Ĭ                             |                    | DENSITIES                                    |   |              |
| ROLLER                            | s used (Mal                            | I U I AL TU DA LE:<br>ROLLERS USED (Make, Type, & Weight) |                                 | 736,000<br>F.W. C. Wagner |   | CURIN<br>CURIN<br>CURIN | PREWET BY:<br>PREWET BY:<br>CURING PERIOD<br>CUTS DRILLED |  | 73.1  |                               | FINAL S<br>FINAL S | FINAL EMB.<br>FINAL SUB-BASE<br>FINAL REPORT | 30<br>30<br>7                               |              |
| REMARKS:                          |  |   |                                 |                           |   |                         | -   | 2  |   | 1                             |                    |  |   |              |
|                                   |  |   |                                 |                           |   |                         |   |  |   |                               |                    |  |   |              |
| SUBI                              | MITTED BY:                             | SUBMITTED BY: Resident Engineer                           |                                 |                           |   |                         |   |  | TE  | TESTED BY: Tester             | ester              |  |   |              |
|                                   |  | RESI  | RESIDENT ENGINEER               | INEER                     |   |                         |   |  | CERTIFICATION NO.: ####   | ION NO.: ¥                    | ###                |  |   | -            |
|                                   |  |   |                                 |                           |   |                         |   |  |   |                               |                    |  |   |              |

3

WYDOT 221.0 (Rev. 10-17)

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# **DETERMINATION OF MACROTEXTURE OF PAVEMENT SURFACE**

- Scope: This method provides a field procedure for determining the macrotexture depth of pavement surfaces. This method is a modification of ASTM E965. Use: This method is used to evaluate macrotexture depth of milled and chip sealed pavement surfaces. Reference Documents: ASTM E965 Standard Test Method for Measuring Pavement Macrotexture Depth Using a Volumetric Technique WYDOT T-211 Macrotexture Report Apparatus: 1. Test material; solid glass spheres having minimum 90 percent roundness meeting requirements of ASTM E965. An acceptable supplier is Potters Industries LLC, 5650 Hwy 279 North, Brownwood, TX 76801 (phone 325-752-6711; product number P-010 US 60-80, Technical Quality Glass Spheres #602602) 2. Sample container; cylindrical metal or plastic container with minimum
  - internal volume of 250 ml, no inner lip on container edge, tight fitting lid
  - 3. Spreader tool; ice hockey puck
  - 4. Brushes; stiff wire brush and a soft bristle brush only on mill surfaces. Do not use wire brushes on chip seals.
  - 5. Wind screen; Sonatube suggested, approximately 3 feet high, cut in half lengthwise (see Figure 1). Alternative wind screens are acceptable such as hinged plywood windbreak or inverted plastic bucket (5 gallon) with bottom cut out (inside diameter limited to 11-inch maximum).



Figure 1, Wind Screen (Sonatube)

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- 6. Ruler; 12 inch standard ruler with 0.1 inch increments or tape measure.
- 7. Graduated cylinder, 100-mL, Pyrex® glass, with 1-mL graduation lines, funnel top and detachable, hexagonal plastic base (part #70075)

For WYDOT testers, above items are available through the Purchasing Program (307-777-4406).

# Procedure: Lab/Office Preparation (test samples, reports):

- 1. Use one sample container for each test; each testing location requires 3 tests spaced 3 feet from each other (total of 3 sample containers per testing location). Use 3 ounce tin with tight fitting lid for 100 mL sample; use 6 ounce tin with tight fitting lid for 200 mL sample.
- 2. Fill graduated cylinder with test material; use 200±2 mL when testing milled pavements (i.e., fill cylinder twice), use 100±1 mL when testing chip sealed pavements.
- 3. Gently tap the side of the graduated cylinder to level the top surface of the test material; visually verify quantity; add or empty material as necessary.
- 4. Pour applicable volume of test material, either 100 mL or 200 mL, in the sample container; close/seal with lid; label quantity on lid with marker pen
- 5. Repeat Steps 1 through 4 to prepare a sufficient quantity of samples for testing all surfacing location(s).
- 6. Prepare necessary test report(s) for recording measurements prior to field testing. Use Form T-211, and at the top of each report mark an ('**X**') in the appropriate box to select each of the following criteria:
  - a. <u>Surfacing Type</u>, either 'Milled Pavement' or 'Chip Sealing';
  - b. If chip sealing, then <u>Aggregate Size</u>, either <sup>3</sup>/<sub>8</sub> inch or <sup>1</sup>/<sub>2</sub> inch;
  - c. <u>Sample Size</u>, either 100 mL or 200 mL;

The report form automatically generates the appropriate cross reference table based on surfacing type, aggregate size, and sample size.

Field Testing/Measurements:

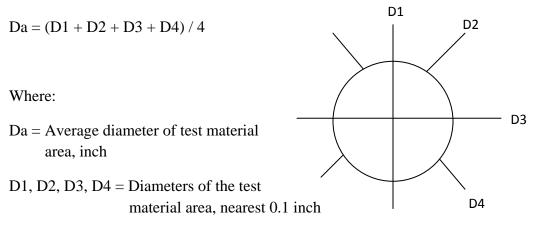
- 1. Test finished pavement surface(s) as follows:
  - a. One test per mile for milled surfaces receiving pavement overlay
  - b. One test per frequency as specified for chip sealed surfaces
- 2. Determine a random, representative testing location on pavement surface to measure macrotexture depth.
- 3. Inspect testing location to ensure it is dry and homogeneous, free of unique or localized features such as cracks, joints, striping, and patching.

- 4. If localized features are present, move up-station at the same transverse offset until a suitable testing location is found.
- 5. Gently clean an area of about 1 foot square for sample location using the stiff-wire brush to remove and residue, debris or loosely bonded material. Be careful not to dislodge bonded material. After using the stiff wire brush, gently brush sample location with the soft bristle brush to remove any remaining debris.
- 6. Place the wind screen on the pavement surface to protect the sample location from air turbulence.
- 7. Hold the sample container with test material above pavement at sample location at a height not greater than 4 inches.
- 8. Pour appropriate, measured volume of test material from the container onto pavement surface forming a conical pile.
- 9. Place the spreader tool (ice hockey puck) lightly on top of conical pile of test material being careful not to compact the test material.
- 10. Move the spreader tool (ice hockey puck) in a slow, circular motion to disperse the test material in a circular area and to create a defined crest around the perimeter.
- 11. Continue spreading the test material until it is well dispersed and the spreader tool (ice hockey puck) rides on top of the high points of the pavement surface.
- 12. Measure and record, to the nearest 0.1 inch, the diameter of the circular area; four times at intervals of 45 degrees as shown below. Measure diameter of circular area from top (crest) of slope on one side, through the center, and to top (crest) of slope on other side of circular area.
- 13. Add all four diameter measurements and divide by 4 to determine average diameter of circular area covered by test material.
- 14. Use cross reference table at bottom of Macrotexture Report, Form T-211, to determine the macrotexture depth of pavement surface at the sample location. Use average diameter rounded to nearest 0.1 inch to determine which row in cross reference table. Record macrotexture depth to nearest 0.001 inch.
- 15. Repeat steps 5 through 14 with a new sample of test material at two more locations spaced 3 feet from each other (3 sample locations will form a triangle with 3 foot sides).
- 16. Add all three results and divide by 3 to determine average macrotexture depth. Report average macrotexture depth to nearest 0.001 inch.

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Calculations:

Calculate average diameter of circular area covered by test material at sample location,



Report: Record macrotexture depth of pavement surface on Form T-211, Macrotexture Report. Report macrotexture depth to nearest 0.001 inch. For chip sealed surfaces, also record percent embedment depth on Form T-211, Macrotexture Report. Report percent embedment depth to nearest 1 percent.



#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY MACROTEXTURE REPORT

Form T-211 Rev. (10-17)

| Resid     | ent Engineer:   | Engineer Na                       | me                       |                          |                          | Town:                    | Engineer T                | own                        |                              |
|-----------|-----------------|-----------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|----------------------------|------------------------------|
|           | Contractor:     | Contractor N                      | Vame                     |                          |                          | Tested By:               | Tester Na                 | ne                         |                              |
|           |                 | X<br>Test Sam                     | Milled Pav               | vement                   |                          | Agg                      |                           | Chip Sealin<br>(nominal ma |                              |
|           | х               | 100 mL                            | 1 1                      | 200 mL                   |                          | r 1                      | ¾ inch                    | -                          | 1⁄2 inch                     |
| Test<br># | Date<br>of Test | Station or<br>RM, Offset,<br>Lane | Diameter<br>D1<br>(inch) | Diameter<br>D2<br>(inch) | Diameter<br>D3<br>(inch) | Diameter<br>D4<br>(inch) | Diameter<br>Avg<br>(inch) | Macro<br>texture<br>Depth  | Percent<br>Embedmen<br>Depth |
| 1         | 1 - 1 - 1 - 4   | 1.5.2                             | 5.3                      | 5.2                      | 5.3                      | 5.4                      | 5.30                      | 0.277                      | N/A                          |
| 2         | 07/18/17        | MP 3.29                           | 5.3                      | 5.4                      | 5.2                      | 5.2                      | 5.28                      | 0.277                      | N/A                          |
| 3         |                 |                                   | 5.2                      | 5.3                      | 5.4                      | 5.4                      | 5.33                      | 0.277                      | N/A                          |
|           |                 |                                   |                          | 1                        | ;;                       | Sub-Test                 | Average =                 | 0.277                      | -                            |
| 1         | 1000            | 1.1                               | 5.2                      | 5.3                      | 5.4                      | 5.5                      | 5.35                      | 0.266                      | N/A                          |
| 2         | 07/19/17        | MP 4.21                           | 5.4                      | 5.5                      | 5.5                      | 5.3                      | 5.43                      | 0.266                      | N/A                          |
| 3         |                 |                                   | 5.5                      | 5.3                      | 5.2                      | 5.5                      | 5.38                      | 0.266                      | N/A                          |
| -         |                 |                                   |                          | _                        |                          | Sub-Test                 | Average =                 | 0.266                      |                              |
|           |                 |                                   |                          | 1 1                      |                          |                          |                           |                            |                              |
|           |                 |                                   |                          |                          |                          |                          |                           |                            |                              |
| -         |                 |                                   | · · · · ·                |                          |                          |                          |                           |                            |                              |
|           |                 |                                   |                          |                          |                          | Sub-Test                 | Average =                 |                            |                              |

| Tested By: |        |              |             |             | Checked By     |             |         |         |
|------------|--------|--------------|-------------|-------------|----------------|-------------|---------|---------|
| Date:      |        |              | -           |             | Date           |             |         |         |
| -          | Macrot | exture Depth | Based on 10 | 00 mL of Te | st Material an | d Average D | iameter |         |
| Average    | Macro  | Dercent      | Average     | Macro       | Percent        | Autorago    | Macro   | Percent |

| Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth |
|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|
| 2.5                           | 1.243                               | N/A                           | 4.5                           | 0.384                               | N/A                           | 6.5                           | 0.184                               | N/A                           |
| 2.6                           | 1.149                               | N/A                           | 4.6                           | 0.367                               | N/A                           | 6.6                           | 0.178                               | N/A                           |
| 2.7                           | 1.066                               | N/A                           | 4.7                           | 0.352                               | N/A                           | 6.7                           | 0.173                               | N/A                           |
| 2.8                           | 0.991                               | N/A                           | 4.8                           | 0.337                               | N/A                           | 6.8                           | 0.168                               | N/A                           |
| 2.9                           | 0.924                               | N/A                           | 4.9                           | 0.324                               | N/A                           | 6.9                           | 0.163                               | N/A                           |
| 3.0                           | 0.863                               | N/A                           | 5.0                           | 0.311                               | N/A                           | 7.0                           | 0.159                               | N/A                           |
| 3.1                           | 0.809                               | N/A                           | 5.1                           | 0.299                               | N/A                           | 7.1                           | 0.154                               | N/A                           |
| 3.2                           | 0.759                               | N/A                           | 5.2                           | 0.287                               | N/A                           | 7.2                           | 0.150                               | N/A                           |
| 3.3                           | 0.713                               | N/A                           | 5.3                           | 0.277                               | N/A                           | 7.3                           | 0.146                               | N/A                           |
| 3.4                           | 0.672                               | N/A                           | 5.4                           | 0.266                               | N/A                           | 7.4                           | 0.142                               | N/A                           |
| 3.5                           | 0.634                               | N/A                           | 5.5                           | 0.257                               | N/A                           | 7.5                           | 0.138                               | N/A                           |
| 3.6                           | 0.600                               | N/A                           | 5.6                           | 0.248                               | N/A                           | 7.6                           | 0.135                               | N/A                           |
| 3.7                           | 0.568                               | N/A                           | 5.7                           | 0.239                               | N/A                           | 7.7                           | 0.131                               | N/A                           |
| 3.8                           | 0.538                               | N/A                           | 5.8                           | 0.231                               | N/A                           | 7.8                           | 0.128                               | N/A                           |
| 3.9                           | 0.511                               | N/A                           | 5.9                           | 0.223                               | N/A                           | 7.9                           | 0.124                               | N/A                           |
| 4.0                           | 0.486                               | N/A                           | 6.0                           | 0.216                               | N/A                           | 8.0                           | 0.121                               | N/A                           |
| 4.1                           | 0.462                               | N/A                           | 6.1                           | 0.209                               | N/A                           | 8.1                           | 0.118                               | N/A                           |
| 4.2                           | 0.440                               | N/A                           | 6.2                           | 0.202                               | N/A                           | 8.2                           | 0.116                               | N/A                           |
| 4.3                           | 0.420                               | N/A                           | 6.3                           | 0.196                               | N/A                           | 8.3                           | 0.113                               | N/A                           |
| 4.4                           | 0.401                               | N/A                           | 6.4                           | 0.190                               | N/A                           | 8.4                           | 0.110                               | N/A                           |

## WYDOT 230.0 (Rev. 10-17)



Form T-211 Rev. (10-17)

| Resid     | ent Engineer:   | Engineer Na                       | me                       |                          |                          | Town:                    | Engineer T                | own                       |                              |
|-----------|-----------------|-----------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------|------------------------------|
|           | Contractor:     | Contractor I                      | Vame                     |                          |                          | Tested By:               | Tester Nar                | ne                        |                              |
|           | 100             | х                                 | Milled Pav               | vement                   |                          |                          |                           | Chip Sealir               |                              |
|           |                 | Test Sam                          | ple Size                 |                          |                          | Agg                      | regate Size               | (nominal ma               | oximum)                      |
|           | <u>i</u>        | 100 mL                            | X                        | 200 mL                   |                          | 1                        | ¾ inch                    | -                         | 1/2 inch                     |
| Test<br># | Date<br>of Test | Station or<br>RM, Offset,<br>Lane | Diameter<br>D1<br>(inch) | Diameter<br>D2<br>(inch) | Diameter<br>D3<br>(inch) | Diameter<br>D4<br>(inch) | Diameter<br>Avg<br>(inch) | Macro<br>texture<br>Depth | Percent<br>Embedmen<br>Depth |
| 1         | 1               | 1000                              | 7.4                      | 7.6                      | 7.5                      | 7.5                      | 7.50                      | 0.276                     | N/A                          |
| 2         | 07/18/17        | MP 3.29                           | 7.3                      | 7.6                      | 7.5                      | 7.7                      | 7.53                      | 0.276                     | N/A                          |
| 3         |                 |                                   | 7.4                      | 7.5                      | 7.4                      | 7.5                      | 7.45                      | 0.276                     | N/A                          |
|           |                 |                                   |                          | i ut                     |                          | Sub-Test                 | Average =                 | 0.276                     |                              |
| 1         |                 | 1.1.1                             | 7.6                      | 7.5                      | 7.7                      | 7.8                      | 7.65                      | 0.262                     | N/A                          |
| 2         | 07/19/17        | MP 4.21                           | 7.6                      | 7.8                      | 7.6                      | 7.7                      | 7.68                      | 0.262                     | N/A                          |
| 3         | 1               |                                   | 7.7                      | 7.5                      | 7.8                      | 7.6                      | 7.65                      | 0.262                     | N/A                          |
|           |                 |                                   | 1.00                     | _                        |                          | Sub-Test                 | Average =                 | 0.262                     | 1                            |
|           |                 |                                   |                          |                          |                          |                          |                           |                           | 1.2                          |
|           |                 |                                   |                          |                          |                          |                          |                           |                           |                              |
| -         |                 | ·                                 |                          | 1                        |                          |                          |                           |                           |                              |

Remarks:

| Tested By: | Checked By: |
|------------|-------------|
| Date:      | Date:       |

| Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth |
|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|
| 4.7                           | 0.703                               | N/A                           | 6.7                           | 0.346                               | N/A                           | 8.7                           | 0.205                               | N/A                           |
| 4.8                           | 0.674                               | N/A                           | 6.8                           | 0.336                               | N/A                           | 8.8                           | 0.201                               | N/A                           |
| 4.9                           | 0.647                               | N/A                           | 6.9                           | 0.326                               | N/A                           | 8.9                           | 0.196                               | N/A                           |
| 5.0                           | 0.622                               | N/A                           | 7.0                           | 0.317                               | N/A                           | 9.0                           | 0.192                               | N/A                           |
| 5.1                           | 0.597                               | N/A                           | 7.1                           | 0.308                               | N/A                           | 9.1                           | 0.188                               | N/A                           |
| 5.2                           | 0.575                               | N/A                           | 7.2                           | 0.300                               | N/A                           | 9.2                           | 0.184                               | N/A                           |
| 5.3                           | 0.553                               | N/A                           | 7.3                           | 0.292                               | N/A                           | 9.3                           | 0.180                               | N/A                           |
| 5.4                           | 0.533                               | N/A                           | 7.4                           | 0.284                               | N/A                           | 9.4                           | 0.176                               | N/A                           |
| 5.5                           | 0.514                               | N/A                           | 7.5                           | 0.276                               | N/A                           | 9.5                           | 0.172                               | N/A                           |
| 5.6                           | 0.496                               | N/A                           | 7.6                           | 0.269                               | N/A                           | 9.6                           | 0.169                               | N/A                           |
| 5.7                           | 0.478                               | N/A                           | 7.7                           | 0.262                               | N/A                           | 9.7                           | 0.165                               | N/A                           |
| 5.8                           | 0.462                               | N/A                           | 7.8                           | 0.255                               | N/A                           | 9.8                           | 0.162                               | N/A                           |
| 5.9                           | 0.446                               | N/A                           | 7.9                           | 0.249                               | N/A                           | 9.9                           | 0.159                               | N/A                           |
| 6.0                           | 0.432                               | N/A                           | 8.0                           | 0.243                               | N/A                           | 10.0                          | 0.155                               | N/A                           |
| 6.1                           | 0.418                               | N/A                           | 8.1                           | 0.237                               | N/A                           | 10.1                          | 0.152                               | N/A                           |
| 6.2                           | 0.404                               | N/A                           | 8.2                           | 0.231                               | N/A                           | 10.2                          | 0.149                               | N/A                           |
| 6.3                           | 0.392                               | N/A                           | 8.3                           | 0.226                               | N/A                           | 10.3                          | 0.146                               | N/A                           |
| 6.4                           | 0.379                               | N/A                           | 8.4                           | 0.220                               | N/A                           | 10.4                          | 0.144                               | N/A                           |
| 6.5                           | 0.368                               | N/A                           | 8.5                           | 0.215                               | N/A                           | 10.5                          | 0.141                               | N/A                           |
| 6.6                           | 0.357                               | N/A                           | 8.6                           | 0.210                               | N/A                           | 10.6                          | 0.138                               | N/A                           |



#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY MACROTEXTURE REPORT

Form T-211 Rev. (10-17)

| Pr        | oject Number:   | ERP Project                       | Number                   |                          | Pr                       | oject Name:              | Project No                | ame                       |                              |
|-----------|-----------------|-----------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------|------------------------------|
| Resid     | lent Engineer:  | Engineer Na                       | me                       |                          |                          | Town:                    | Engineer 1                | Town                      |                              |
|           | Contractor:     | Contractor N                      | Vame                     |                          |                          | Tested By:               | Tester Na                 | me                        |                              |
|           |                 |                                   | Milled Pav               | ement                    |                          |                          | X                         | Chip Sealir               |                              |
|           | -               | Test Sam                          | ple Size                 | Sec. 4                   |                          |                          |                           | (nominal ma               |                              |
|           | X               | 100 mL                            |                          | 200 mL                   | and and a                | X                        | ¾ inch                    |                           | 1/2 inch                     |
| Test<br># | Date<br>of Test | Station or<br>RM, Offset,<br>Lane | Diameter<br>D1<br>(inch) | Diameter<br>D2<br>(inch) | Diameter<br>D3<br>(inch) | Diameter<br>D4<br>(inch) | Diameter<br>Avg<br>(inch) | Macro<br>texture<br>Depth | Percent<br>Embedmen<br>Depth |
| 1         |                 | 1-21                              | 9.0                      | 8.8                      | 8.4                      | 8.8                      | 8.75                      | 0.100                     | 73                           |
| 2         | 06/02/17        | MP 50.1                           | 9.2                      | 9.8                      | 9.6                      | 9.2                      | 9.45                      | 0.086                     | 71                           |
| 3         |                 | n'                                | 8.6                      | 9.6                      | 8.6                      | 9.1                      | 8.98                      | 0.096                     | 74                           |
|           |                 |                                   |                          |                          | g                        | Sub-Test                 | Average =                 | 0.094                     | 75                           |
| 1         |                 |                                   | 6.8                      | 8.6                      | 7.6                      | 7.2                      | 7.55                      | 0.135                     | 64                           |
| 2         | 06/03/17        | MP 50.73                          | 7.1                      | 7.8                      | 6.7                      | 7.0                      | 7.15                      | 0.150                     | 60                           |
| 3         |                 |                                   | 6.7                      | 7.9                      | 7.4                      | 8.0                      | 7.50                      | 0.138                     | 63                           |
| 1.1       | 0.000           |                                   | a                        | 1.00                     | Constant of the          | Sub-Test                 | Average =                 | 0.141                     | 62                           |
| 1         |                 |                                   | 8.9                      | 8.9                      | 8.6                      | 9.0                      | 8.85                      | 0.098                     | 74                           |
| 2         | 06/04/17        | MP 51.85                          | 8.9                      | 10.1                     | 9.4                      | 8.4                      | 9.20                      | 0.092                     | 75                           |
| 3         |                 |                                   | 8.8                      | 9.0                      | 8.3                      | 9.4                      | 8.88                      | 0.098                     | 74                           |
|           |                 |                                   |                          |                          |                          | Sub-Test                 | Average =                 | 0.096                     | 74                           |

Remarks:

| Fested By:                    |                                     |                               |                               |                                     | Checked By:                   |                               |                                     |                               |
|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|
| Date:                         |                                     |                               |                               |                                     | Date:                         |                               |                                     |                               |
| Percent                       | Embedmer                            | nt Depth Based                | on 100 mL                     | of Test Ma                          | terial, Average               | Diameter, a                   | und ¾ inch                          | aggregate                     |
| Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth |
| 4.6                           | 0.367                               | 2                             | 6.6                           | 0.178                               | 53                            | 8.6                           | 0.105                               | 72                            |
| 4.7                           | 0.352                               | 6                             | 6.7                           | 0.173                               | 54                            | 8.7                           | 0.103                               | 73                            |
| 4.8                           | 0.337                               | 10                            | 6.8                           | 0.168                               | 55                            | 8.8                           | 0.100                               | 73                            |
| 4.9                           | 0.324                               | 14                            | 6.9                           | 0.163                               | 57                            | 8.9                           | 0.098                               | 74                            |
| 5.0                           | 0.311                               | 17                            | 7.0                           | 0.159                               | 58                            | 9.0                           | 0.096                               | 74                            |
| 5.1                           | 0.299                               | 20                            | 7.1                           | 0.154                               | 59                            | 9.1                           | 0.094                               | 75                            |
| 5.2                           | 0.287                               | 23                            | 7.2                           | 0.150                               | 60                            | 9.2                           | 0.092                               | 75                            |
| 5.3                           | 0.277                               | 26                            | 7.3                           | 0.146                               | 61                            | 9.3                           | 0.090                               | 76                            |
| 5.4                           | 0.266                               | 29                            | 7.4                           | 0.142                               | 62                            | 9.4                           | 0.088                               | 77                            |
| 5.5                           | 0.257                               | 31                            | 7.5                           | 0.138                               | 63                            | 9.5                           | 0.086                               | 77                            |
| 5.6                           | 0.248                               | 34                            | 7.6                           | 0.135                               | 64                            | 9.6                           | 0.084                               | 78                            |
| 5.7                           | 0.239                               | 36                            | 7.7                           | 0.131                               | 65                            | 9.7                           | 0.083                               | 78                            |
| 5.8                           | 0.231                               | 38                            | 7.8                           | 0.128                               | 66                            | 9.8                           | 0.081                               | 78                            |
| 5.9                           | 0.223                               | 41                            | 7.9                           | 0.124                               | 67                            | 9.9                           | 0.079                               | 79                            |
| 6.0                           | 0.216                               | 42                            | 8.0                           | 0.121                               | 68                            | 10.0                          | 0.078                               | 79                            |
| 6.1                           | 0.209                               | 44                            | 8.1                           | 0.118                               | 69                            | 10.1                          | 0.076                               | 80                            |
| 6.2                           | 0.202                               | 46                            | 8.2                           | 0.116                               | 69                            | 10.2                          | 0.075                               | 80                            |
| 6.3                           | 0.196                               | 48                            | 8.3                           | 0.113                               | 70                            | 10.3                          | 0.073                               | 81                            |
| 6.4                           | 0.190                               | 49                            | 8.4                           | 0.110                               | 71                            | 10.4                          | 0.072                               | 81                            |
| 6.5                           | 0.184                               | 51                            | 8.5                           | 0.108                               | 71                            | 10.5                          | 0.070                               | 81                            |

## WYDOT 230.0 (Rev. 10-17)



Form T-211 Rev. (10-17)

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| Resid     | lent Engineer:  | Engineer Na                       | me                       |                          |                          | Town:                    | Engineer T                | own                        |                               |
|-----------|-----------------|-----------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|----------------------------|-------------------------------|
|           | Contractor:     | Contractor N                      | Vame                     |                          |                          | Tested By:               | Tester Na                 | me                         |                               |
|           |                 | Test Sam                          | Milled Pav               | /ement                   |                          | Agg                      | X<br>regate Size          | Chip Sealir<br>(nominal ma |                               |
|           |                 | 100 mL                            | х                        | 200 mL                   |                          | X                        | ¾ inch                    | 1 1                        | 1∕₂ inch                      |
| Test<br># | Date<br>of Test | Station or<br>RM, Offset,<br>Lane | Diameter<br>D1<br>(inch) | Diameter<br>D2<br>(inch) | Diameter<br>D3<br>(inch) | Diameter<br>D4<br>(inch) | Diameter<br>Avg<br>(inch) | Macro<br>texture<br>Depth  | Percent<br>Embedment<br>Depth |
| 1         | 1               | 1                                 | 11.7                     | 11.6                     | 11.8                     | 11.5                     | 11.65                     | 0.114                      | 70                            |
| 2         | 07/10/17        | MP 5.62                           | 11.6                     | 11.8                     | 11.7                     | 11.9                     | 11.75                     | 0.112                      | 70                            |
| 3         |                 |                                   | 11.4                     | 11.6                     | 11.7                     | 11.6                     | 11.58                     | 0.115                      | 69                            |
| -         |                 |                                   |                          | Careford and             | 1                        | Sub-Test                 | Average =                 | 0.114                      | 70                            |
| 1         | 12-25           | 1.000                             | 10.8                     | 10.9                     | 11.0                     | 11.1                     | 10.95                     | 0.128                      | 66                            |
| 2         | 07/11/17        | MP 6.53                           | 10.9                     | 10.8                     | 10.6                     | 10.7                     | 10.75                     | 0.133                      | 65                            |
| 3         |                 |                                   | 10.7                     | 10.9                     | 10.8                     | 11.0                     | 10.85                     | 0.131                      | 65                            |
|           |                 |                                   | _                        |                          |                          | Sub-Test                 | Average =                 | 0.131                      | 65                            |
|           |                 |                                   |                          |                          |                          |                          |                           |                            |                               |
|           |                 |                                   |                          |                          |                          |                          |                           |                            |                               |
|           |                 |                                   |                          |                          |                          | Sub-Test                 | Average =                 | 11                         |                               |

| Tested By:<br>Date:                      |   |   |  |   | Checked By:<br>Date:          |  |                                     |  |
|--|---|---|--|---|-------------------------------|--|-------------------------------------|--|
| Percent<br>Average<br>Diameter<br>(inch) | Embedmer<br>Macro<br>texture<br>Depth<br>(inch) | nt Depth Based<br>Percent<br>Embedment<br>Depth | on 200 mL<br>Average<br>Diameter<br>(inch) | of Test Ma<br>Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Diameter, a<br>Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Aggregate<br>Percent<br>Embedment<br>Depth |
| 6.5                                      | 0.368   | 2   | 8.5  | 0.215   | 43                            | 10.5   | 0.141                               | 62   |
| 6.6                                      | 0.357   | 5   | 8.6  | 0.210   | 44                            | 10.6   | 0.138                               | 63   |
| 6.7                                      | 0.346   | 8   | 8.7  | 0.205   | 45                            | 10.7   | 0.136                               | 64   |
| 6.8                                      | 0.336   | 10  | 8.8  | 0.201   | 46                            | 10.8   | 0.133                               | 65   |
| 6.9                                      | 0.326   | 13  | 8.9  | 0.196   | 48                            | 10.9   | 0.131                               | 65   |
| 7.0                                      | 0.317   | 15  | 9.0  | 0.192   | 49                            | 11.0   | 0.128                               | 66   |
| 7.1                                      | 0.308   | 18  | 9.1  | 0.188   | 50                            | 11.1   | 0.126                               | 66   |
| 7.2                                      | 0.300   | 20  | 9.2  | 0.184   | 51                            | 11.2   | 0.124                               | 67   |
| 7.3                                      | 0.292   | 22  | 9.3  | 0.180   | 52                            | 11,3   | 0.122                               | 67   |
| 7.4                                      | 0.284   | 24  | 9.4  | 0.176   | 53                            | 11.4   | 0.120                               | 68   |
| 7.5                                      | 0.276   | 26  | 9.5  | 0.172   | 54                            | 11.5   | 0.118                               | 69   |
| 7.6                                      | 0.269   | 28  | 9.6  | 0.169   | 55                            | 11.6   | 0.115                               | 69   |
| 7.7                                      | 0.262   | 30  | 9.7  | 0.165   | 56                            | 11.7   | 0.114                               | 70   |
| 7.8                                      | 0.255   | 32  | 9.8  | 0.162   | 57                            | 11.8   | 0.112                               | 70   |
| 7.9                                      | 0.249   | 34  | 9.9  | 0.159   | 58                            | 11.9   | 0.110                               | 71   |
| 8.0                                      | 0.243   | 35  | 10.0                                       | 0.155   | 59                            | 12.0   | 0.108                               | 71   |
| 8.1                                      | 0.237   | 37  | 10.1                                       | 0.152   | 59                            | 12.1   | 0.106                               | 72   |
| 8.2                                      | 0.231   | 38  | 10.2                                       | 0.149   | 60                            | 12.2   | 0.104                               | 72   |
| 8.3                                      | 0.226   | 40  | 10.3                                       | 0.146   | 61                            | 12.3   | 0.103                               | 73   |
| 8.4                                      | 0.220   | 41  | 10.4                                       | 0.144   | 62                            | 12.4   | 0.101                               | 73   |



## WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY MACROTEXTURE REPORT

Form T-211 Rev. (10-17)

| Project Number: ERP Project Number |                 |                                   | Project Name: Project Name |                          |                          |                          |                           |                            |                              |  |  |
|------------------------------------|-----------------|-----------------------------------|----------------------------|--------------------------|--------------------------|--------------------------|---------------------------|----------------------------|------------------------------|--|--|
| Reside                             | ent Engineer:   | Engineer Na                       | me                         |                          |                          | Town:                    | Engineer 1                | Town                       | wn                           |  |  |
|                                    | Contractor:     | Contractor N                      | Vame                       | -                        |                          | Tested By:               | Tested By: Tester Name    |                            |                              |  |  |
|                                    |                 | Test Sam                          | Milled Pav                 | vement                   |                          | ٨٥٥                      | X<br>recate Size          | Chip Sealir<br>(nominal ma |                              |  |  |
|                                    | x               | 100 mL                            |                            | 200 mL                   |                          |                          | % inch                    | X                          | 1/2 inch                     |  |  |
| Test<br>#                          | Date<br>of Test | Station or<br>RM, Offset,<br>Lane | Diameter<br>D1<br>(inch)   | Diameter<br>D2<br>(inch) | Diameter<br>D3<br>(inch) | Diameter<br>D4<br>(inch) | Diameter<br>Avg<br>(inch) | Macro<br>texture<br>Depth  | Percent<br>Embedmen<br>Depth |  |  |
| 1                                  | 1               | 1                                 | 7.1                        | 7.2                      | 7.4                      | 7.3                      | 7.25                      | 0.146                      | 71                           |  |  |
| 2                                  | 07/22/17        | MP 5.62                           | 7.2                        | 7.5                      | 7.3                      | 7.5                      | 7.38                      | 0.142                      | 72                           |  |  |
| 3                                  |                 |                                   | 6.8                        | 7.0                      | 7.1                      | 6.9                      | 6.95                      | 0.159                      | 68                           |  |  |
|                                    |                 |                                   |                            | 1 Sec. 1                 | -                        | Sub-Test                 | Average =                 | 0.149                      | 70                           |  |  |
| 1                                  |                 | 1 M.                              | 6.6                        | 6.7                      | 6.9                      | 6.8                      | 6.75                      | 0.168                      | 66                           |  |  |
| 2                                  | 07/22/17        | MP 6.53                           | 6.7                        | 6.9                      | 6.6                      | 6.6                      | 6.70                      | 0.173                      | 65                           |  |  |
| 3                                  | 1               |                                   | 6.9                        | 6.8                      | 7.1                      | 6.9                      | 6.93                      | 0.163                      | 67                           |  |  |
|                                    |                 |                                   |                            |                          |                          | Sub-Test                 | Average =                 | 0.168                      | 66                           |  |  |
|                                    | 1               |                                   |                            | 1 2 3                    |                          |                          |                           |                            |                              |  |  |
|                                    |                 |                                   | 1                          | 1                        |                          |                          |                           |                            |                              |  |  |
|                                    |                 |                                   | <u>.</u>                   |                          | . —                      | Cule Test                | Average =                 |                            |                              |  |  |

Remarks:

| Tested By:                    |                                     |                               |                               | -                                   | Checked By:                   |                               |                                     |                               |
|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|
| Date:                         | e:                                  |                               |                               | Date:                               | <u> </u>                      |                               |                                     |                               |
| Percent                       | Embedmer                            | nt Depth Based                | on 100 mL                     | of Test Ma                          | terial, Average               | Diameter, a                   | and ½ inch                          | aggregate                     |
| Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth |

| (inch) | (inch) | Depth | (inch) | (inch) | Depth | (inch) | (inch) | Depth |
|--------|--------|-------|--------|--------|-------|--------|--------|-------|
| 4.0    | 0.486  | 3     | 6.0    | 0.216  | 57    | 8.0    | 0.121  | 76    |
| 4.1    | 0.462  | 8     | 6.1    | 0.209  | 58    | 8.1    | 0.118  | 76    |
| 4.2    | 0.440  | 12    | 6.2    | 0.202  | 60    | 8.2    | 0.116  | 77    |
| 4.3    | 0.420  | 16    | 6.3    | 0.196  | 61    | 8.3    | 0.113  | 77    |
| 4.4    | 0.401  | 20    | 6.4    | 0.190  | 62    | 8.4    | 0.110  | 78    |
| 4.5    | 0.384  | 23    | 6.5    | 0.184  | 63    | 8.5    | 0.108  | 78    |
| 4.6    | 0.367  | 27    | 6.6    | 0.178  | 64    | 8.6    | 0.105  | 79    |
| 4.7    | 0.352  | 30    | 6.7    | 0.173  | 65    | 8.7    | 0.103  | 79    |
| 4.8    | 0.337  | 33    | 6.8    | 0.168  | 66    | 8.8    | 0.100  | 80    |
| 4.9    | 0.324  | 35    | 6.9    | 0.163  | 67    | 8.9    | 0.098  | 80    |
| 5.0    | 0.311  | 38    | 7.0    | 0.159  | 68    | 9.0    | 0.096  | 81    |
| 5.1    | 0.299  | 40    | 7.1    | 0.154  | 69    | 9.1    | 0.094  | 81    |
| 5.2    | 0.287  | 43    | 7.2    | 0.150  | 70    | 9.2    | 0.092  | 82    |
| 5.3    | 0.277  | 45    | 7.3    | 0.146  | 71    | 9.3    | 0.090  | 82    |
| 5.4    | 0.266  | 47    | 7.4    | 0.142  | 72    | 9.4    | 0.088  | 82    |
| 5.5    | 0.257  | 49    | 7.5    | 0.138  | 72    | 9.5    | 0.086  | 83    |
| 5.6    | 0.248  | 50    | 7.6    | 0.135  | 73    | 9.6    | 0.084  | 83    |
| 5.7    | 0.239  | 52    | 7.7    | 0.131  | 74    | 9.7    | 0.083  | 83    |
| 5.8    | 0.231  | 54    | 7.8    | 0.128  | 74    | 9.8    | 0.081  | 84    |
| 5.9    | 0.223  | 55    | 7.9    | 0.124  | 75    | 9.9    | 0.079  | 84    |

#### WYDOT 230.0 (Rev. 10-17)

# WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY MACROTEXTURE REPORT

Form T-211 Rev. (10-17)

| Resident Engineer: |                 | Engineer Na                       | me                       |                          | Town: Engineer Town      |                          |                           |                           |                              |
|--------------------|-----------------|-----------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|---------------------------|---------------------------|------------------------------|
| Contractor:        |                 | Contractor N                      | Vame                     |                          |                          | Tested By: Tester Name   |                           |                           |                              |
|                    |                 |                                   | Milled Pav               | vement                   |                          |                          | х                         | Chip Sealir               |                              |
|                    |                 | Test Sam                          | ple Size                 | iter to a                |                          | Agg                      |                           | (nominal ma               |                              |
|                    | <u>.</u>        | 100 mL                            | Х                        | 200 mL                   |                          |                          | ¾ inch                    | Х                         | 1/2 inch                     |
| Test<br>#          | Date<br>of Test | Station or<br>RM, Offset,<br>Lane | Diameter<br>D1<br>(inch) | Diameter<br>D2<br>(inch) | Diameter<br>D3<br>(inch) | Diameter<br>D4<br>(inch) | Diameter<br>Avg<br>(inch) | Macro<br>texture<br>Depth | Percent<br>Embedmen<br>Depth |
| 1                  | Law and a       | 1000                              | 10.8                     | 10.6                     | 10.9                     | 10.7                     | 10.75                     | 0.133                     | 73                           |
| 2                  | 07/11/17        | MP 5.62                           | 10.9                     | 10.8                     | 11.1                     | 11.0                     | 10.95                     | 0.128                     | 74                           |
| 3                  |                 |                                   | 10.6                     | 10.7                     | 10.5                     | 10.4                     | 10.55                     | 0.138                     | 72                           |
| -                  |                 |                                   |                          |                          | a - 1                    | Sub-Test                 | Average =                 | 0.133                     | 73                           |
| 1                  |                 | 1                                 | 9.5                      | 9.3                      | 9.4                      | 9.6                      | 9.45                      | 0.172                     | 66                           |
| 2                  | 07/12/17        | MP 6.53                           | 9.6                      | 9.8                      | 9.7                      | 9.4                      | 9.63                      | 0.169                     | 66                           |
| 3                  | 1               |                                   | 9.8                      | 9.7                      | 10.0                     | 9.9                      | 9.85                      | 0.159                     | 68                           |
|                    |                 |                                   | 1.11                     |                          |                          | Sub-Test                 | Average =                 | 0.167                     | 67                           |
|                    |                 |                                   |                          |                          |                          |                          |                           |                           |                              |
|                    |                 |                                   |                          |                          |                          |                          |                           |                           |                              |
| -                  |                 |                                   |                          | 1. — - V                 |                          | Sub Test                 | Average =                 |                           | -                            |

| Tested By: |           |              |             |             | Checked By    |               |              |           |
|------------|-----------|--------------|-------------|-------------|---------------|---------------|--------------|-----------|
| Date:      |           |              |             |             | Date          | :             |              |           |
| Percent    | Embedment | t Depth Base | d on 200 mL | of Test Mat | erial, Averag | e Diameter, a | and ½ inch a | aggregate |
| Average    | Macro     | Percent      | Average     | Macro       | Percent       | Average       | Macro        | Percent   |

| Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth | Average<br>Diameter<br>(inch) | Macro<br>texture<br>Depth<br>(inch) | Percent<br>Embedment<br>Depth |
|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------|
| 5.6                           | 0.496                               | 1                             | 7.6                           | 0.269                               | 46                            | 9.6                           | 0.169                               | 66                            |
| 5.7                           | 0.478                               | 4                             | 7.7                           | 0.262                               | 48                            | 9.7                           | 0.165                               | 67                            |
| 5.8                           | 0.462                               | 8                             | 7.8                           | 0.255                               | 49                            | 9.8                           | 0.162                               | 68                            |
| 5.9                           | 0.446                               | 11                            | 7.9                           | 0.249                               | 50                            | 9.9                           | 0.159                               | 68                            |
| 6.0                           | 0.432                               | 14                            | 8.0                           | 0.243                               | 51                            | 10.0                          | 0.155                               | 69                            |
| 6.1                           | 0.418                               | 16                            | 8.1                           | 0.237                               | 53                            | 10.1                          | 0.152                               | 70                            |
| 6.2                           | 0.404                               | 19                            | 8.2                           | 0.231                               | 54                            | 10.2                          | 0.149                               | 70                            |
| 6.3                           | 0.392                               | 22                            | 8.3                           | 0.226                               | 55                            | 10.3                          | 0.146                               | 71                            |
| 6.4                           | 0.379                               | 24                            | 8.4                           | 0.220                               | 56                            | 10.4                          | 0.144                               | 71                            |
| 6.5                           | 0.368                               | 26                            | 8.5                           | 0.215                               | 57                            | 10.5                          | 0.141                               | 72                            |
| 6.6                           | 0.357                               | 29                            | 8.6                           | 0.210                               | 58                            | 10.6                          | 0.138                               | 72                            |
| 6.7                           | 0.346                               | 31                            | 8.7                           | 0.205                               | 59                            | 10.7                          | 0.136                               | 73                            |
| 6.8                           | 0.336                               | 33                            | 8.8                           | 0.201                               | 60                            | 10.8                          | 0.133                               | 73                            |
| 6.9                           | 0.326                               | 35                            | 8.9                           | 0.196                               | 61                            | 10.9                          | 0.131                               | 74                            |
| 7.0                           | 0.317                               | 37                            | 9.0                           | 0.192                               | 62                            | 11.0                          | 0.128                               | 74                            |
| 7.1                           | 0.308                               | 38                            | 9.1                           | 0.188                               | 62                            | 11.1                          | 0.126                               | 75                            |
| 7.2                           | 0.300                               | 40                            | 9.2                           | 0.184                               | 63                            | 11.2                          | 0.124                               | 75                            |
| 7.3                           | 0.292                               | 42                            | 9.3                           | 0.180                               | 64                            | 11.3                          | 0.122                               | 76                            |
| 7.4                           | 0.284                               | 43                            | 9.4                           | 0.176                               | 65                            | 11.4                          | 0.120                               | 76                            |
| 7.5                           | 0.276                               | 45                            | 9.5                           | 0.172                               | 66                            | 11.5                          | 0.118                               | 76                            |

# IN - PLACE DENSITY TEST (SUBBASES AND BASES)

| Scope: | This method is used in determining the in-place density of granular material |
|--------|--|
|        | without the need to compact a moisture-density curve in the field.           |

Intent

# For Use: No field In-Place Density Test is needed if the:

- 1. Rock material, the No. 4 is over 40 percent retained or
- 2. Maximum aggregate size is over 2 inches

### Apparatus: 1. Sand cone apparatus, 1 gal jar and funnel

- 2. Containers with lids, suggest two concrete cylinder cans
- 3. Chisel and hammer
- 4. Rammer with guide,  $5\frac{1}{2}$  lb
- 5. Spoon or half round dish
- 6. Shovel
- 7. Square pans 15 inch, suggested
- 8. Drying stoves
- 9. Moisture tins
- 10. No. 4 screen
- 11. Wooden block, suggest 2 inch x 4 inch
- 12. Gram scale, sensitive to 0.1 g
- 13. 35 lb [15 kg] scale sensitive to 0.01 lb [5 kg]
- 14. Base plate optional
- 15. 2 inch screen
- 16. Standard sand
- 17. Clean canvas sample sacks

# Reference

Documents:AASHTO T 180Standard Method of Test for Moisture-Density Relations of Soils<br/>Using a 4.54-kg (10-lb) Rammer and a 457-mm (18-in.) DropWYDOT 212.0Sand Cone Method Field Density TestWYDOT 215.0In-Place Density and Moisture Content of Soil and Soil -<br/>Aggregate by Nuclear Methods (Shallow Depth)WYDOT T-112Soil Compaction Worksheet\*WYDOT T-113Weekly Report of Compaction of:<br/>EmbankmentWYDOT T-166Aggregate Analysis

\* Note: Use of weekly reports is optional

Note: For WYDOT personnel, contact WYDOT Field Services for information or sources for standard sand.

- Sample: A representative sample of granular material is taken during a *Sand Cone Method Field Density Test*, WYDOT 212.0. If a nuclear gauge is used, then follow the procedure as outlined in WYDOT 215.0, *In-Place Density and Moisture Content of Soil and Soil - Aggregate by Nuclear Methods (Shallow Depth)*, and take the material from under the Nuclear gauge to determine the percent of rock.
  - Note: Send at least 150 lb of aggregate to the Materials Program as soon as a representative sample can be obtained, but not less than two weeks before the aggregate is placed on the roadway. The Materials Program will then establish the maximum dry density and optimum moisture to be used in the field.

Sample sacks will be made of canvas weighing 30 to 50 lb, not to exceed 50 lb.

A completed Form T-166, Aggregate Analysis, be submitted with each sack.

- a. The maximum dry density needed for this test procedure is determined by AASHTO T 180, *Moisture Density Relations of Soils Using a 10 lb. (4.54 Kg) Rammer and 18 inch (457 mm) Drop.*
- b. Record the maximum dry density and optimum moisture as item "HH" and "GG" on Form T-112 as previously established by the Materials Program.
- Procedure: Laboratory Preparations
  - 1. Record the standard sand density as item "A" on Form T-112, *Soil Compaction Worksheet*, see WYDOT 211.0, *Standardization of Sand*. Also see example Form T-112 of this section.
  - 2. Calibrate the sand used to fill the funnel by filling the 1 gal jar with standard sand. Weigh the apparatus and sand. Invert the sand cone apparatus into a <u>flat</u> level pan, open the valve and let the sand run into the funnel until the sand has ceased to flow, close the valve, and weigh the sand in either the pan or the apparatus and remaining sand; either way will give you the amount of sand to fill the funnel. Care should be taken not to agitate the apparatus while the sand is moving, as this would rearrange the sand particles and give an erroneous answer. Repeat this two more times and average the weight. Record the average weight as item "E" on Form T-112. This weight should remain constant for each test as long as the standard density of sand remains the same.
  - 3. Fill the sand cone; 1 gal jar with standard sand, weigh the apparatus and sand. Record as item "B" on Form T-112.

4. Weigh an empty container and lid (concrete cylinder can) and record the weight as item "H" on Form T-112.

# Field Operation

- 1. Level off an area approximately 2  $ft^2$  to accommodate the sand cone, removing all loose material from the test area.
- 2. Place the sand cone in the cleared area and scribe an outline of the cone on the soil for a guide while digging the hole. Using the chisel and spoon, dig a test hole a minimum of 4 inches in diameter and deep enough to remove one lift of base material. Place base into a tared container with an air tight lid to prevent moisture loss. Remove all loose base from the hole. Take care not to disturb the sides of the hole when removing the material.
  - Note: A base plate may be used in place of scribing an outline of the cone on the soil. The base plate gives the advantage of a larger diameter hole especially when rock and/or thin lifts of gravel for surfacing or soils is encountered. If the base plate is used, it will be considered a part of the funnel and becomes part of the calibration of the funnel and entered as item "E" on Form T-112.
- 3. Invert the sand cone apparatus, placing the cone over the hole, open the valve all of the way and allow the sand to flow freely. Be careful not to agitate the apparatus or the surrounding ground while the sand is running. When the sand ceases to flow, close the valve and carefully remove the jar from the hole. Gather as much sand from the hole area as possible, placing the sand into a separate container to be reclaimed later.

# Laboratory Operation

- 1. Weigh the sand cone apparatus and the remaining sand. Record as item "C" on Form T-112.
- 2. Weigh the soil, rock, and container. Record as item "G" on Form T-112.
  - Note: Coarse is defined as material retained on the No. 4 screen. For this procedure, percent rock is used to describe the percent of coarse material in a sample.
- 3. Determine the moisture content of the entire sample of the material removed, from the hole. Record as item "R".

- 4. Using the 2 inch x 4 inch wooden block, separate soil and rock on the No.4 screen. Material remaining on the No. 4 screen is rock and must be free of soil or clay coatings. Weigh the rock retained and record as item "J" on Form T-112. Determine the percent rock as outlined on Form T-112, item "K".
- 5. Complete all computations up to and including item "T" on Form T-112.
- 6. Rock correction is used with material that has between 0 to 15% rock.

Percent Rock (to nearest whole number) =  $\frac{Percent Rock}{3}$ 

Report: Report weekly results on optional Form T-113, *Weekly Report for Compaction of Crushed Base*.

# DEAFTURET

# WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SOIL COMPACTION WORKSHEET

T-112

(Rev. 09-16)

|        |                                    |                              |                 |                           |                        | Field Tes   |                  | -                 |                  |         |             |        |                    |     | -              |
|--------|------------------------------------|------------------------------|-----------------|---------------------------|------------------------|---|------------------|-------------------|------------------|---------|-------------|--------|--------------------|-----|----------------|
|        |                                    | lo(s).: N##                  |                 |                           |                        | Station Sampled: STA 0+50<br>At: Resident Engineer's Town   |                  |                   |                  |         |             |        |                    | 2   |                |
|        | Submitte                           | d By: Resid                  | ent Enginee     | er                        |                        |   | At:              | Resid             | lent En          | iginee  | r's To      | wn     |                    |     |                |
|        |                                    | aken: 3 ft                   |                 | 1.00                      |                        | Net the comp  | : 2 ft - 8 ft    |                   |                  |         |             |        |                    |     |                |
| Secti  | on Represe                         | ented: STA (                 | D+00 to 0+1     | 100                       |                        | County: Resident Engineer's Town  |                  |                   |                  |         |             |        |                    |     |                |
|        | Date Sam                           | pled: XX/X                   | X/XX            |                           |                        | Date Rec  | eived:           | XX/X              | (X/XX            |         |             |        |                    | _   | -              |
|        |                                    |                              | Test            | t was made                | ×                      |   | day(s)           | ) after           | fill wa          | s plac  | ed.         |        |                    |     |                |
| A      | Density of S                       | tandard Sand                 | l, lb/ft³       |                           | 96.7                   |   |                  |                   | tent (R          | oadw    | ay)         | Wt. (  | of Water           |     | /t. of<br>y So |
|        |                                    |                              |                 |                           |                        |   | oil and<br>n, g  |                   | oiland<br>n,g    |         | reof<br>n,g | L      | - M, g             | 1.1 | - N,           |
| в      | Wt. of Appa                        | ratus and Sar                | nd. Ib          |                           | 12.91                  | - L -   | 781.7            | M                 | 744.0            | N       | 105.5       | P      | 37.7               | Q   | 63             |
| С      |                                    | ratus and Unu                |                 | b                         | 6.77                   |   | 1 m m            |                   | P/Q)             |         | 1.2 - T.C.  |        |                    | 5.9 | 1              |
| D      | Sand Used (                        |                              |                 |                           | 6.14                   | 1-25-   | 15-12-22         |                   | 10 × 100 0       | 12772   |             |        |                    | -   |                |
| E      |                                    | to Fill Funnel               | , lb            |                           | 3.45                   | s   | Wet De           | ensitv.           | lb/ft³ (         | (A x (* | 1))/F       |        | -                  | 1   | 41.6           |
| F      |                                    | Hole (D - E), I              | 5 MA 12         |                           | 2.69                   |   |                  |                   | & Rock           |         |             | 4.00   | 1                  | Not |                |
| ~      |                                    |                              |                 |                           |                        |   |                  | 1. 1. 1. 1. 1. T. | 0% Roc           |         |             |        |                    |     |                |
| G      | Wt. of Soil.                       | Rock and Cor                 | ntainer. Ib     |                           | 5.04                   |   |                  |                   |                  | .,      |             |        | -                  |     |                |
| H      |                                    | Container, Ib                |                 |                           | 1.10                   | Т   |                  | -                 | Dry D            | ensity  | / lb/ft³    |        |                    | -   |                |
| 1      | Wt. Soil and Rock (G - H), Ib 3.94 |                              |                 |                           | <u></u>                |   | ** S / (100 + R) |                   |                  |         |             | 133.7  |                    |     |                |
|        |                                    |                              |                 |                           |                        |   | P For            | 0% - 1            | K. Rock          |         |             | 8 * (K | all 👘              |     |                |
| J      | Wt. of Rock                        | (Retained on                 | No. 4), lb      |                           | 2.09                   |   | where.           | (103) 1           | sto nea          | rest v  | tiols m     | umboi  |                    | Not | Used           |
| ĸ      | % of Rock, (                       | J / I) x 100                 |                 |                           | 53.0                   |   | ** For           | 15% - 4           | 10% Roo          | ck, let | S = S >     | 100    |                    |     |                |
| v      | Wet Wit of S                       | Soil and Mold,               | lb              |                           |                        | 1   |                  | -                 |                  |         | -           | -      | _                  | -   |                |
| w      | Tare Wt. of I                      |                              | 27.             |                           |                        |   |                  | P                 |                  |         |             | 1      |                    | -   |                |
| Y      |                                    | Soil in 1/30 ft <sup>a</sup> | Mold (V - V     | V), Ib                    |                        |   |                  |                   |                  | 1       |             | -      |                    | -   |                |
| z      |                                    | of Soil, Ib/ft3,             |                 | - //                      | 10                     |   |                  |                   |                  |         | -           | 2      | - 3                | -   |                |
| ~ 1    |                                    |                              | ity of Soil, Ib | o/ft <sup>3</sup>         |                        |   |                  |                   |                  | -       |             |        |                    |     |                |
|        |                                    |                              | Z x 100         |                           |                        |   |                  |                   |                  |         |             |        |                    |     |                |
| -      | (100 -                             | + (AA or BB o                |                 | or EE or FF))             |                        |   |                  |                   |                  | 4.4     |             |        |                    |     |                |
| 1.7    |                                    |                              |                 |                           |                        |   |                  | 1                 | F                | 1       | 6           |        | 1                  | 1   |                |
| M      | L                                  | M                            | N               | P                         | Q                      |   |                  |                   | % Moistu<br>x 10 |         |             |        |                    |     |                |
| i      | Wet Soil                           | Dry Soil                     | Tare of         | Wt. of                    | Wt. of                 |   |                  |                   |                  |         |             |        |                    |     |                |
| s<br>t | and Tin, g                         | and Tin, g                   | Tin, g          | Water                     | Dry Soil               |   |                  |                   |                  |         |             |        |                    |     |                |
| u<br>r |                                    |                              | 200             | L - M, g                  | M - N, g               |   |                  |                   |                  |         |             |        |                    |     |                |
| e      |                                    |                              | -               |                           |                        | АА  | -                |                   |                  |         |             |        |                    |     |                |
| с      |                                    |                              |                 |                           | k                      | A COLUMN TO A C | B                | -                 |                  |         |             |        |                    |     |                |
| o<br>n |                                    |                              |                 |                           |                        | В   |                  | 1                 | CC C             |         |             | 1. L.  |                    |     |                |
| t<br>e |                                    | -                            |                 |                           |                        |   |                  |                   | ~                |         | DD          |        | _                  |     |                |
| n<br>t | ÷                                  |                              |                 |                           |                        |   |                  | _                 | _                |         |             | -      | EE                 | -   | _              |
| •      |                                    |                              |                 |                           |                        |   |                  | -                 |                  |         | -           |        | -                  | ſ   | FF             |
|        | Optimum Me<br>Plotted GG           | oisture %<br>* 8.3           |                 | Max Dry Der<br>Plotted HH | nsity, lb/ft³<br>135.8 | Roadv<br>Optim  | 10000            | isture            | % ( + or         | -)      |             |        | eld Comp<br>I)x100 |     |                |
|        | 0.000                              |                              |                 |                           |                        |   |                  |                   |                  |         |             |        |                    |     |                |

Tested By Tester Certification No. ### (This page intentionally left blank.)

# MIX DESIGN FOR STABILIZED BASE (FDR)

- Scope: This procedure describes the mix design procedure used to determine the optimum additive content for each blend of aggregate materials available.
- Use: This procedure is used to determine the optimum emulsion and lime and/or other additives for stabilized bases, most commonly for full depth reclamation operations.

# Apparatus: 1. <u>Jaw Crusher</u> able to produce material passing the No. 4 sieve requirements. A sledge may be used to reduce oversize particles to permit the material to be fed into the crusher

- 2. <u>Gyratory Compactor</u> calibrated for 6 inch diameter mold, including molds and ancillary equipment
- 3. <u>Marshall Stability/Flow Equipment</u> calibrated, including ancillary equipment
- 4. <u>Mechanical Mixer</u> equipped with bowls 10 inch to 12 inch in diameter
- 5. <u>Two ovens</u>; one forced draft oven capable of maintaining a temperature of  $104 \pm 5$  °F and another capable of maintaining a temperature of  $300 \pm 9$  °F
- 6. <u>Balance</u>, 5 kg capacity, accurate to 1 g
- 7. <u>Sieves</u>, U.S. Standard sizes, as specified
- 8. <u>Sample Splitter</u> suitable for splitting aggregates up to 1.25 inches
- 9. <u>Pans</u> approximately 10 inch diameter by 3 inch deep
- 10. <u>Trowels</u> and other <u>small tools</u>

### Reference

| Documents: | AASHTO T 166 | Standard Method of Test for Bulk Specific Gravity of<br>Compacted Hot Mix (HMA) Using Saturated Surface-Dry<br>Specimens         |
|------------|--------------|--|
|            | AASHTO T 180 | Standard Method of Test for Moisture-Density Relations of<br>Soils Using a 4.54-kg (10-lb) Rammer and a 457-mm (18-<br>in.) Drop |
|            | AASHTO T 209 | Standard Method of Test for Theoretical Maximum Specific<br>Gravity and Density of Hot Mix Asphalt (HMA)                         |
|            | AASHTO T 283 | Standard Method of Test for Resistance of Compacted Hot<br>Mix Asphalt (HMA) to Moisture-Induced Damage                          |
|            | ASTM D1452   | Standard Practice for Soil Exploration and Sampling by Auger Borings   |
|            | ASTM D2950   | Standard Test Method for Density of Bituminous Concrete in Place by Nuclear Methods  |
|            | ASTM D4867   | Standard Test Method for Effect of Moisture on Asphalt<br>Concrete Paving Mixtures   |
|            | WYDOT 214.0  | Moisture - Density Relations of Soils Method "C"   |
|            | WYDOT 414.0  | Marshall and Superpave Mix Design and Mix Volumetric Verification Procedure  |
|            | WYDOT 415.0  | Density Testing for Compacted Mix  |
|            | WYDOT 836.0  | Fine Aggregate Sand Equivalent   |

# Sampling and Processing:

Based on data from auger borings (ASTM D1452), cores (WYDOT 415.0), and/or other determinations (i.e. plans, core records, pavement records, FWD deflection data, etc.), determine if more than one mix design will be performed. In addition, FDR projects with more than a 2 inch difference in bituminous surface between sections, with varying base types, or significant addition of crushed base will require the necessity of separate mix designs.

Obtain uncontaminated materials of uniform quality that meet the requirements of the plans and specifications.

- 1. <u>Emulsion</u>. Provide a CSS-FDR emulsion sample, approximately 4 gallons per mix design, that meets the project requirements.
- 2 <u>Crushed Base</u>. Furnish crushed base, 60 pounds if specified, that meets the project requirements.
- 3. <u>Additive</u>. Determine the amount and type of additive, if any during the mix design. When an additive is required, the total amount in the mix will not exceed 1.5 percent by weight of material.
  - a. <u>Lime</u>. When lime is required, furnish 1 pound of lime that meets the project requirements. Use hydrated lime or commercial lime slurry, as shown in the plans.

Note: Usually addition of 1 percent lime is sufficient.

b. <u>Cement</u>. When cement is required, furnish 1 pound of hydraulic cement that meets the project requirements.

Note: Usually addition of 1 percent cement is sufficient.

c. <u>Fly Ash</u>. When fly ash is required, furnish 1 pound of fly ash that meets the project requirements.

If cores or slabs are received, determine the individual and average thickness values.

Crush the existing pavement (RAP) and any stabilized base materials to the gradation below before blending with the aggregate. Determine the washed gradation on the composite material. The composite material will include any or all of the existing base, the RAP, and/or virgin aggregates. Combine the materials in the proportions that are representative of the project depth and cross-section.

| Sieve Size | Gradation |  |  |  |  |
|------------|-----------|--|--|--|--|
| 1¼ inch    | 100       |  |  |  |  |
| 1 inch     | 90 to 100 |  |  |  |  |

Specimens prepared for mix design must have a maximum size passing the  $1\frac{1}{4}$  inch screen for all material components.

<u>Material Evaluation</u>: Determine the composite material washed gradation and sand equivalent and report. Determine the RAP dry and washed gradation and sand equivalent. Report the washed gradation and sand equivalent on the blend.

Perform Modified Proctor compaction according to WYDOT 214.0 to determine optimum moisture content (OMC) at peak dry density. Define OMC by a best-fit curve using a minimum of four points. Material containing 20 percent or more passing the No. 200 be mixed with the target moisture, sealed, and set aside a minimum of 12 hours. All other material be set aside a minimum of 3 hours. If a material contains less than 4 percent passing No. 200, then the additional curing is not required.

# 1. Selection of Water Content for Mix Design

- a. Determine the water content of the composite material, not including water in the emulsion in accordance with AASHTO T 180, WYDOT 214.0. Mix water at the target water content for material containing 20 percent or more passing the No. 200 sieve, seal and set aside for a minimum of 12 hours. All other material will be set aside for a minimum of 3 hours. For material having a significant amount of RAP or coarse material that does not produce a well-defined moisture density curve, establish the optimum moisture content (OMC) at 3 percent.
- b. Select the water content of specimens for the mix design, not including water in the emulsion, based on the following:

| * | If SE $\leq$ 30                | 60 to 75 percent of OMC |
|---|--------------------------------|-------------------------|
| * | If SE > 30                     | 45 to 65 percent of OMC |
| * | No. 200 < 4.0 percent          | OMC = 2.5 percent       |
| * | OMC established at 3.0 percent | OMC = 2.5 percent       |

Sand equivalent is based on SE from the composite sample

# 2. Preparation of Test Specimens

- a. Obtain an appropriate amount of composite material before the addition of water and emulsion to produce compacted samples at least  $70 \pm 5$  mm in height and 150 mm diameter or 100 mm diameter for AASHTO T 283, see Table 2 in the Special Provision for Stabilized Full Depth Reclamation.
- b. Mix the composite material specimens with the required amount of water for 60 seconds before the addition of emulsion. Allow the specimens sit sealed according to the same guidelines as used for the OMC specimens in Step 1.
- c. Samples have a weight before addition of water and emulsion to produce  $70 \pm 5$  mm tall compacted specimens (except for IDT testing).

- d. Select four emulsion contents that will bracket the design emulsion content. Typically 3 percent, 4 percent, 5 percent, and 6 percent are used, but other ranges or narrower bands (0.5 percent) may be designated.
- e. Produce the number of specimens for each test method in the laboratory according to the following table:

| Test                                 | Number of Specimens per Emulsion Content |
|--------------------------------------|--|
| Maximum Specific Gravity *           | 2  |
| Gyratory Compacted Stability         | 3  |
| Initial Gyratory Compacted Stability | 3  |
| Indirect Tensile Strength            | 6  |

\* Uncompacted

- f. Mix the composite material and emulsion in a mechanical mixer at room temperature for 60 seconds.
- g. Cure mixed specimens individually at 104 °F for 27 to 33 minutes. Cover loosely.
- h. If other materials are to be added, such as lime or cement, introduce them in a similar manner as they will be on the project. For example, if lime is incorporated a day or more before emulsion addition, then add it to the wet aggregate a day or more before mixing with emulsion. If lime is incorporated as a slurry, then add it as a slurry in the laboratory.

# **3.** Compaction and Curing

- a. Compact emulsion stabilized specimens in a Superpave gyratory compactor (SGC) at a vertical pressure of 600 kPa, an external angle of  $1.25^{\circ} \pm 0.02^{\circ}$  (internal angle of  $1.16^{\circ} \pm 0.02^{\circ}$ ), a mold of 6 inches diameter for 30 gyrations, and at room temperature. After the last gyration, apply 600 kPa pressure for 10 seconds. Do not heat the mold.
- b. Cure compacted emulsion stabilized specimens, in a forced draft oven at 104 °F for 40 to 48 hours (20 to 24 hours for ITS) and to a constant weight ( constant weight equals weight of core that does not change more than 0.05 percent when weighed at 2 hour intervals). After curing, allow the specimens to cool at room temperature for a minimum of 24 hours and a maximum of 30 hours.
- c. Cure specimens for initial stability at room temperature  $(76 \pm 10)$  for 20 to 24 hours.

d. Leave specimens for maximum specific gravity in loose form, not compacted, and test after cooling at room temperature for a minimum of 12 hours and a maximum of 24 hours.4. Volumetric Measurements

a. Determine and average the maximum specific gravities (AASHTO T 209) of two specimens at each emulsion content.

Note: Use the supplemental dry-back procedure.

- b. Determine and average the bulk specific gravities (AASHTO T 166) of all specimens at each emulsion content.
- c. <u>Stability and flow</u>. Once completed, the gyratory compacted stability and flow test results are used to calculate the Gyratory Quotient value (GQ). The GQ indicates mixture stiffness. (While stiff mixtures are desirable to resist permanent deformation, it is not desirable to have mixtures so stiff that they are likely to crack under heavy, repeated loads.)
  - 1. Prepare three specimens at each emulsion content in accordance with Sections 2 and 3.
  - 2. Test the dry samples for stability and flow using a 6 inch diameter stability breaking head.
  - 3. Calculate GQ by dividing the peak stability value by the flow value reached at the point of peak stability.
  - 4. For stability, report the average value of the three specimens for stability, flow, and GQ.
  - 5. Repeat Steps 4.c.1 through 4.c.4 for initial stability, reporting only the stability.
- d. Indirect Tensile Strength (ITS)
  - 1. Prepare six specimens according to Sections 2 and 3 at the selected emulsion content, half to be tested dry and the other half to be tested after moisture conditioning.
  - 2. <u>Dry Subset</u>. Test according to AASHTO T 283.
  - 3. <u>Conditioned Subset</u>. Test according to AASHTO T 283 excluding the vacuum saturation and freeze cycle. Place samples in a  $104 \pm 2$  °F water bath for  $24 \pm 1$  h. Remove and place specimens in a  $77 \pm 1$  °F water bath for  $2 h \pm 10$  min.

Continue testing according to AASHTO T 283 Section 11.

# 5. Emulsion Content Selection

a. Select a design emulsion content to produce a stabilized base mixture meeting the requirements of Table 1 in the Special Provision for Stabilized Full Depth Reclamation. If more than one emulsion content produces mixtures that meet the criteria, then select the emulsion content that produces a mixture with the highest cured stability that meets all other criteria.

# 6. Report

- a. Submit the mix design with a minimum of the following information on a modified Form E-46
  - 1. Project Information (Project Number, Project Name, Project, Resident Engineer, etc.)
  - 2. Penetration of the Emulsion Residue used in the Mix Design
  - 3. A general description of the materials received, their locations, and sampling procedure.
  - 4. Average thickness of bituminous materials (RAP), existing base, etc.
  - 5. Thickness to be reclaimed
  - 6. Washed gradation of the separate and blended material(s). If RAP was crushed in the laboratory, then report the gradation of the RAP and the combined washed gradation of the blend
  - 7. Sand equivalent value of the separate and blended materials
  - 8. Density and OMC of composite materials, un-stabilized, from Proctor compaction
  - 9. Moisture content used in mix design and the recommended Moisture Content for field control
  - 10. Range of emulsion contents tested
  - 11. Density, G<sub>mm</sub>, and air voids at each emulsion content (average values)
  - 12. Initial Stability after 24 hours (average values)
  - 13. Indirect tensile strength (ITS), dry (control sample), and wet (conditioned sample), at each emulsion content (average values)
  - 14. Criteria values for each emulsion content tested
  - 15. Design emulsion content as a percent, in gallons per square yard, and in gallons per foot (with assumed width reported)
  - 16. Initial Stability
  - 17. Final Cured Stability
  - 18. Final Cured Flow
  - 19. Gyratory Quotient

# VERIFICATION AND CERTIFICATION OF HIGH SPEED INERTIAL PROFILER

| Scope:     | This procedure describes verification and certification of high speed inertial profiler (HSIP) before use on plant mix and concrete pavements. Each HSIP requires periodic verification and annual certification prior to construction season. Each HSIP operator must be certified. |  |  |  |  |
|------------|--|--|--|--|--|
| Use:       |  | This section describes verification and certification procedures for HSIP prior to measuring surface variation, analyzing profile, and evaluating pavement smoothness. |  |  |  |
| Apparatus: | <ol> <li>HSIP</li> <li>Distance Mea</li> </ol>   | suring Instrument (DMI)  |  |  |  |
| Reference  |  |  |  |  |  |
| Documents: | AASHTO M 328   | Standard Specification for Inertial Profiler   |  |  |  |
|            | AASHTO R 56  | Standard Practice for Certification of Inertial Profiling<br>Systems   |  |  |  |
|            | AASHTO R 57  | Standard Practice for Operating Inertial Profiling Systems   |  |  |  |
|            | ASTM E 867   | Standard Terminology Relating to Vehicle-Pavement<br>Systems   |  |  |  |
|            | ASTM E 950   | Standard Test Method for Measuring the Longitudinal<br>Profile of Traveled Surfaces with an Accelerometer<br>Established Internal Profiling Reference                  |  |  |  |
|            | ASTM E 1926  | Standard Practice for Computing International Roughness<br>Index of Roads from Longitudinal Profile Measurements   |  |  |  |
|            | ASTM E 2560  | Standard Specification for Data Format for Pavement Profile  |  |  |  |
|            | WYDOT 414  | WYDOT Standard Specifications  |  |  |  |
|            | WYDOT 415  | WYDOT Standard Specifications  |  |  |  |
|            | WYDOT 402.0  | Pavement Profile Analysis  |  |  |  |
|            | WYDOT 403.0  | Pavement Smoothness Evaluation   |  |  |  |
|            | WYDOT SS-400A  | Supplementary Specification for Amendments to Division 400   |  |  |  |
|            | WYDOT SS-400B  | Supplementary Specification for Plant Mix Pavement<br>Surface Variation, Profile and Smoothness  |  |  |  |
|            | WYDOT T-515 IPV  | • •  |  |  |  |

#### WYDOT 401.0 (Rev. 10-18) Procedure:

- 1. Verification minimum frequency; weekly and once prior to certification,
  - a. verify DMI accuracy according to AASHTO R 56, Section 8.4,
  - b. perform AASHTO R 57, including:
    - 1. block test (height sensor check),
    - 2. bounce test (vehicle suspension rebound),
  - c. accelerometer; per manufacturer's recommendations prior to each project; report settings/adjustments to WYDOT,
  - maintaining log (test results, software changes, etc); at minimum, must include data shown on WYDOT Form T-515 IPV (example included in this section),
  - e. having necessary repairs/adjustments/upgrades.
- 2. Certification -

Perform according to AASHTO R 56; comply with following:

- a. Equipment:
  - calibration comply with verification requirements above (Step 1); for concrete pavement, profiler must use approved line lasers, minimum three (3) inch wide footprint,
  - have current (valid) annual certification from Wyoming Materials Technician Certification (WMTC) Program
- b. Operator -must:
  - 1. be proficient in operation of profiler, and
  - 2. have current (valid) 3-year certification from Wyoming Materials Technician Certification (WMTC) Program.
- c. Test Section (reference profile) -WYDOT selects site(s) for certification testing; includes the following:
  - 1. Roughness test section, typically smooth, 30-75, ),
    - a. relatively straight and level (no significant grade, grade change, horizontal curvature nor superelevation),
    - b. perform three (3) closed loop data collection runs using reference profiler; each wheel path in the intended direction of travel.
  - 2. DMI test section, minimum length (0.1 mile + proper)

lead-in and safe stopping distances, before and after),

- a. relatively straight and level (no significant grade, grade change, horizontal curvature nor superelevation),
- b. painted with a dot at least every 20 feet in wheel paths,
- c. perform three (3) closed loop data collection runs using reference profiler; each wheel path in the intended direction of travel.

NOTE: For closed loop data collection:

i. determine cross-correlation value for closed loop run in each wheel path; use Profile Viewer and Analysis (ProVAL) software program (http://www.roadprofile.com) developed for Federal Highway Administration (FHWA); use following parameters:

| Parameter  | Value            |
|--|------------------|
| Height sensor spacing, inch [mm]                 | 70 ±1 [1778 ±25] |
| Sample interval (relative elevations), inch [mm] | 1.0 [25] max     |
| Long wavelength (high pass filter), feet [m]     | 300 [91] max     |

minimum cross-correlation value of 95 to accept each wheel path; if less than 95, repeat three (3) closed loop data collection runs,

- ii. use IRI (plant mix) or PI (concrete) from third run for each 0.1 mile section for each wheel path as reference value for certification; reference values not shared with participant/operator.
- d. Evaluation (contractor's HSIP):

Perform according to AASHTO R 56, Sections 8.2.3 and 8.3;

1. Analyze test data using ProVAL to determine crosscorrelations of filtered data to establish repeatability and accuracy of HSIP; filter data using parameters noted in table above; provide flash/thumb drive or email containing raw data files in **.ppf** format to WYDOT for analysis; media not returned to operator (contractor), 2. Certify HSIP (as acceptable) when the following criteria are satisfied:

| Property<br>(each run, each wheel path) | Score<br>(minimum) |
|---|--------------------|
| Repeatability                           | 0.92               |
| Accuracy, average                       | 0.90               |

Issue certificate for HSIP. Certificate includes:

- i. Serial Number,
- ii. VIN number,
- iii. Make and model,
- iv. Height sensor serial numbers,
- v. Accelerometer serial numbers,
- vi. Certification date, and
- vii. Expiration date.

Certification expires on May 31<sup>st</sup> of following year; list of certified profilers available on WYDOT website.

# e. Suspension

(contractor's HSIP fails subsequent verification):

- 1. WYDOT selects test section per Item c above with following exceptions:
  - i. Contractor's HSIP performs three (3) runs; provide flash/thumb drive containing raw data files in **.ppf** format to WYDOT; media not returned to contractor,
  - ii. Compare results of contractor's HSIP as follows:

| Average Difference<br>IRI, plant mix or PI, concrete;<br>each 0.1 mile section<br>(inch/mile) | Certification Status<br>(contractor HSIP) |  |
|---|---|--|
| $\leq 6.0$  | Retain                                    |  |
| > 6.0   | Allow 3 additional runs                   |  |
| <b>Re-evaluation</b> (after a   | dditional runs)                           |  |
| $\leq 6.0$  | Retain                                    |  |
| > 6.0   | Suspended                                 |  |

- iii. Repair and/or adjust/calibrate HSIP by the manufacturer,
- iv. At contractor's option, recertify HSIP after repairs, etc, prior to next annual certification; contractor pays all costs associated with recertification.



### WYOMING DEPARTMENT OF TRANSPORTATION HIGH SPEED INERTIAL PROFILER WORKSHEET

Form T-515 IPV (Rev. 10-18)

| Project No.(s):     | N216XXX             | Test Date:        | 7/1/2016               |
|---------------------|---------------------|-------------------|------------------------|
| Engineer(s):        | Resident Engineer   | Prime Contractor: | Prime Contractor       |
| Route:              | US 20/26, ML34      | Location:         | Natrona - Powder River |
| Beginning MP:       | 30.06               | Ending MP:        | 39.60                  |
| Profile Contractor: | Profiler Contractor | Software Used:    | ICC                    |
| Vehicle Info:       | 4208                | Operator:         | John Smith             |

|    | Height Sensor Check - Left |         |       |         |       |         |       |         |       |
|----|----------------------------|---------|-------|---------|-------|---------|-------|---------|-------|
|    | Base Plate                 | 1.00-in | Δh    | 2.00-in | Δh    | 0.25-in | Δh    | 0.50-in | Δh    |
| 1  | 0.246                      | 1.255   | 1.005 | 2.265   | 2.015 | 0.504   | 0.254 | 0.755   | 0.505 |
| 2  | 0.251                      | 1.265   | 1.015 | 2.259   | 2.009 | 0.499   | 0.249 | 0.749   | 0.499 |
| 3  | 0.252                      | 1.253   | 1.003 | 2.241   | 1.991 | 0.479   | 0.229 | 0.744   | 0.494 |
| 4  | 0.250                      | 1.241   | 0.991 | 2.251   | 2.001 | 0.501   | 0.251 | 0.746   | 0.496 |
| 5  | 0.248                      | 1.249   | 0.999 | 2.247   | 1.997 | 0.511   | 0.261 | 0.744   | 0.494 |
| 6  | 0.250                      | 1.252   | 1.002 | 2.243   | 1.993 | 0.498   | 0.248 | 0.741   | 0.491 |
| 7  | 0.252                      | 1.248   | 0.998 | 2.258   | 2.008 | 0.496   | 0.246 | 0.739   | 0.489 |
| 8  | 0.250                      | 1.251   | 1.001 | 2.259   | 2.009 | 0.485   | 0.235 | 0.745   | 0.495 |
| 9  | 0.249                      | 1.241   | 0.991 | 2.254   | 2.004 | 0.489   | 0.239 | 0.748   | 0.498 |
| 10 | 0.248                      | 1.251   | 1.001 | 2.246   | 1.996 | 0.492   | 0.242 | 0.738   | 0.488 |
| VG | 0.250                      |         | 1.001 |         | 2.003 |         | 0.246 |         | 0.496 |

0.01 inch Allowable Pass

#### Fail ×

# Height Sensor Check - Right

| 1.1 | Base Plate | 1.00-in | Δh    | 2.00-in | ∆h    | 0.25-in | Δh    | 0.50-in | Δh    |
|-----|------------|---------|-------|---------|-------|---------|-------|---------|-------|
| 1   | 0.250      | 1.248   | 0.998 | 2.275   | 2.025 | 0.474   | 0.224 | 0.745   | 0.495 |
| 2   | 0.251      | 1.243   | 0.993 | 2.219   | 1.969 | 0.499   | 0.249 | 0.746   | 0.496 |
| 3   | 0.249      | 1.253   | 1.003 | 2.241   | 1.991 | 0.490   | 0.240 | 0.743   | 0.493 |
| 4   | 0.250      | 1.247   | 0.997 | 2.351   | 2.101 | 0.501   | 0.251 | 0.738   | 0.488 |
| 5   | 0.252      | 1.251   | 1.001 | 2.243   | 1.993 | 0.489   | 0.239 | 0.736   | 0.486 |
| 6   | 0.249      | 1.262   | 1.012 | 2.233   | 1.983 | 0.498   | 0.248 | 0.748   | 0.498 |
| 7   | 0.251      | 1.250   | 1.000 | 2.158   | 1.908 | 0.501   | 0.251 | 0.751   | 0.501 |
| 8   | 0.250      | 1.242   | 0.992 | 2.289   | 2.039 | 0.485   | 0.235 | 0.733   | 0.483 |
| 9   | 0.248      | 1.261   | 1.011 | 2.234   | 1.984 | 0.488   | 0.238 | 0.749   | 0.499 |
| 10  | 0.249      | 1.257   | 1.007 | 2.286   | 2.036 | 0.482   | 0.232 | 0.738   | 0.488 |
| AVG | 0.250      | 1       | 1.001 | 1       | 1.999 |         | 0.242 |         | 0.493 |

0.01 inch Allowable Pass

X Fail

#### **DMI Check**

| Test       | Run 1         | ΔD         | Run 2         | ΔD        | Run 3     | ΔD  | Avg ∆D  |
|------------|---------------|------------|---------------|-----------|-----------|-----|---------|
| 1          | 1001.6        | 1.6        | 1000.2        | 0.2       | 999.5     | 0.5 | 0.76667 |
| f Test 1 o | utside allowa | ble differ | ence, calibra | te and ru | n Test 2. |     |         |
| 2          |               |            |               |           |           |     | 2       |
| f Test 2 o | utside allowa | ble differ | ence, calibra | te and ru | n Test 3. |     |         |
|            |               |            |               |           |           |     |         |

#### **PAVEMENT PROFILE ANALYSIS**

- Scope: This procedure explains profile analysis of concrete and plant mix pavement surfaces (i.e., reduction or processing of raw elevation profile data). Pavement surfaces are measured from a moving plane of reference and elevation data is processed to provide a filtered or adjusted profile. Profile measurements agree with actual elevations within predetermined precision and accuracy.
- Use: Use procedure to locate surface defects (e.g., bumps, dips, etc) on new or rehabilitated pavement. Distance between inertial plane of reference of profiler and traveled pavement surface is measured to detect changes in elevation of pavement surface. Procedure is based upon ASTM E 950 which allows profile measurements at different longitudinal distance intervals (Classes 1, 2, 3, or 4) with associated vertical resolution. WYDOT requires Class 1 for longitudinal sampling and vertical measurement resolution ( $\leq 1$  inch [25 mm],  $\leq 0.005$  inch [0.1 mm], respectively).

## Apparatus: 1. High Speed Inertial Profiler (HSIP)

- 2. Computer, integral or external to profiler
- 3. Software program (ProVAL)

#### Reference

| Documents: | AASHTO M 328<br>AASHTO R 56 | Standard Specification for Inertial Profiler<br>Standard Practice for Certification of Inertial Profiling |
|------------|-----------------------------|---|
|            |                             | Systems   |
|            | AASHTO R 57                 | Standard Practice for Operating Inertial Profiling Systems  |
|            | ASTM E 867                  | Standard Terminology Relating to Vehicle-Pavement<br>Systems  |
|            | ASTM E 950                  | Standard Test Method for Measuring the Longitudinal<br>Profile of Traveled Surfaces with an Accelerometer |
|            |                             | Established Internal Profiling Reference  |
|            | ASTM E 1170                 | Standard Practices for Simulating Vehicular Response to   |
|            |                             | Longitudinal Profiles of Traveled Surfaces  |
|            | ASTM E 1926                 | Standard Practice for Computing International Roughness   |
|            |                             | Index of Roads from Longitudinal Profile Measurements   |
|            | ASTM E 2560                 | Standard Specification for Data Format for Pavement   |
|            |                             | Profile   |
|            | WYDOT 414                   | WYDOT Standard Specifications   |
|            | WYDOT 415                   | WYDOT Standard Specifications   |
|            | WYDOT 401.0                 | Verification and Certification of High Speed Inertial Profiler  |

| WYDOT 403.0     | Pavement Smoothness Evaluation                         |
|-----------------|--|
| WYDOT SS-400A   | Supplementary Specification for Amendments to Division |
|                 | 400  |
| WYDOT SS-400B   | Supplementary Specification for Plant Mix Pavement     |
|                 | Surface Variation, Profile and Smoothness:             |
| WYDOT T-515 IPV | High Speed Inertial Profiler Worksheet                 |
| WYDOT T-515 SR  | Smoothness Testing Summary Report                      |

Procedure: 1. Verification of HSIP -Perform according to WYDOT 401.0.

- 2. Prepare roadway (contractor)
  - a. Remove loose material and debris, which can interfere with/cause incorrect surface measurements; move anything, especially with a reflective surface, at least 20 feet from roadway; remove all obstacles, including equipment.
  - b. Place photo-triggering devices (cones, wands with reflective tape, reflective tape on roadway, etc) at appropriate locations described in SS-400A and SS-400B.
    - 1. The engineer must approve placement of triggering devices, and
    - 2. After approval of trigger locations, mark locations on pavement using spray paint; mark locations by outlining corners of cone (allows for accurate verification and re-testing).
  - c. Ensure all personnel on-site are aware of testing.
  - d. Allow sufficient start-up (typically 500 feet minimum) and safe stopping distances for required vehicle/profiler speed.
- 3.) Perform profile analysis according to following table (contractor):

File name format according to AASHTO R 56, Sections 8.3.1.1 through 8.3.1.5 except 4th character is '**P**' signifying profile analysis.

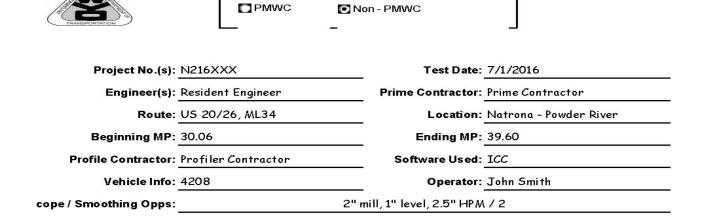
| Concrete Paven  | nent  | Plant Mix Par                  | vement         |  |  |
|---|---|--------------------------------|----------------|--|--|
| a. Measure surface variation of w   | heel paths using HSIP   |                                |                |  |  |
| (allow system to achi   | (allow system to achieve operational stability per manufacturer's recommendations |                                |                |  |  |
| then collect raw profile data at appropriate roadway speed).                    |   |                                |                |  |  |
| b. Submit flash/thumb drive to engineer; raw profile data files in .ppf format. |   |                                |                |  |  |
| c. Process/filter raw profile data (  | c. Process/filter raw profile data (post-run) using following parameters:         |                                |                |  |  |
| Short Wavelength (lo  | w pass filter) = 2.00 fe  | et [0.60 m]                    |                |  |  |
| Long Wavelength (hig  | gh pass filter) = 300 fe  | et [91 m]                      |                |  |  |
| Cut-off Wavelength (  | 3rd order Butterworth   | filter) = $24$ inch [610 mm    | .]             |  |  |
| d. Process profile data to produce  | simulated 25-foot pro   | filograph output.              |                |  |  |
| e. Review profile for all road segn   | ments, beginning to en  | d; determine repair location   | on(s) (surface |  |  |
| variation exceeds maximum all   | lowable pavement para   | ameter).                       |                |  |  |
| Perform 'Must-Grind' analysis:  |   |                                |                |  |  |
| -Full section including bridge appr   | oaches excluding  | Table 2, SS-4                  | 400B           |  |  |
| bridge deck   |   | Type I                         |                |  |  |
| -Bumps/Dips Threshold   | ,   | Type II                        |                |  |  |
| Table 414.4.12.2-1 (new paven   |   | Type II                        |                |  |  |
| Table 415.4.2-1 (repair existing  |   |                                |                |  |  |
| f. Calculate pavement parameter (   | · · · ·   | 1.1 mile; use ProvAL sof       | tware).        |  |  |
| PI (Profile Inde  | ,   |                                |                |  |  |
| Full section excluding b  | ridge deck  |                                |                |  |  |
| Use the following parameters:   |   |                                |                |  |  |
| Blanking Band, max = $0.10$ inch [2]  | 9.5 mm]   | IRI (International Rou         | <b>o</b> ,     |  |  |
| Re-center, min $= 0.10$ mile [0.  | -   | Full section excluding         | g bridge deck  |  |  |
| Scallop:  |   |                                |                |  |  |
| Height, min = $0.03$ inch [0.75 r   | nm]   | <i>Note</i> : ProVAL calculate |                |  |  |
| Width, $min = 2.00$ feet [0.60 m  |   | or average of both             | wheel paths.   |  |  |
| Rounding increment, $max = 0.0$   |   |                                |                |  |  |
| Segment length, max = $528$ feet [1]  |   |                                |                |  |  |
| Lane width in feet  | _   |                                |                |  |  |
| g. If repairs verified for two (2)  | SS-400A;  | g. If no repairs               |                |  |  |
| consecutive runs, perform   | Section 414   | necessary, profile             |                |  |  |
| corrective actions and re-run   | (new pavement),   | analysis is complete. If       | SS-400B        |  |  |
| steps e thru f. Repeat until no   | Section 415   | repairs necessary, re-         |                |  |  |
| repairs necessary.  | (repair existing)   | run steps e thru f.            |                |  |  |
| h. Submit signed reports to WYD   | OT (see report example  | les in WYDOT 403.0)            |                |  |  |

NOTE: Define a segment as a continuous paved length that is the width of the land and approximately 0.1 mi [0.16 km] long.

WYDOT 402.0 (Rev. 10-18)

# WYOMING DEPARTMENT OF TRANSPORTATION SMOOTHNESS TESTING SUMMARY REPORT

Form T-515 SR (Rev. 10-18)



#### **IRI Data Summary**

| Run:                | 1      | 2      | 3      |
|---------------------|--------|--------|--------|
| IRI <sub>i</sub> :_ | 45.89  | 46.01  | 45.78  |
| StDev:              | 5.74   | 5.40   | 5.86   |
| Tested Length:      | 100743 | 100738 | 100748 |

I attest the above is valid for the project listed and free from known errors.

| Prepared By: P  | inted Name: <b>John Smith</b> | Signature: | John Smíth |  |
|-----------------|-------------------------------|------------|------------|--|
|                 |                               |            |            |  |
| Submitted By: P | inted Name: Mary Davis        | Signature: | Mary Davis |  |

#### Attach this form to top of spreadsheet calculations

# **PAVEMENT SMOOTHNESS EVALUATION**

- Scope: This procedure explains smoothness evaluation of concrete and plant mix pavement surfaces. Pavement surfaces are measured using a high speed inertial profiler (HSIP). Surface profile is reported as Profile Index, PI, for concrete pavement and International Roughness Index, IRI, for plant mix pavement. Example forms and reports, with explanatory notes, are included.
  Use: Use procedure to determine smoothness pay adjustments for new or rehabilitated pavement surfaces after profile analysis is completed (contractor corrective actions).
  Apparatus: 1. High Speed Inertial Profiler (HSIP)
  2. Computer, integral or external to profiler
  - 3. Software program (ProVAL)

Reference

| Reference               |  |
|-------------------------|--|
| Documents: AASHTO M 328 | Standard Specification for Inertial Profiler                   |
| AASHTO R 56             | Standard Practice for Certification of Inertial Profiling      |
|                         | Systems  |
| AASHTO R 57             | Standard Practice for Operating Inertial Profiling Systems     |
| <b>ASTM E 867</b>       | Standard Terminology Relating to Vehicle-Pavement Systems      |
| <b>ASTM E 950</b>       | Standard Test Method for Measuring the Longitudinal            |
|                         | Profile of Traveled Surfaces with an Accelerometer             |
|                         | Established Internal Profiling Reference                       |
| ASTM E 1170             | Standard Practices for Simulating Vehicular Response to        |
|                         | Longitudinal Profiles of Traveled Surfaces                     |
| ASTM E 1926             | Standard Practice for Computing International Roughness        |
|                         | Index of Roads from Longitudinal Profile Measurements          |
| ASTM E 2560             | Standard Specification for Data Format for Pavement Profile    |
| WYDOT 414               | WYDOT Standard Specifications                                  |
| WYDOT 415               | WYDOT Standard Specifications                                  |
| WYDOT 401.0             | Verification and Certification of High Speed Inertial Profiler |
| WYDOT 402.0             | Pavement Profile Analysis                                      |
| WYDOT SS-400A           | Supplementary Specification for Amendments to Division 400     |
| WYDOT SS-400B           | Supplementary Specification for Plant Mix Pavement Surface     |
|                         | Variation, Profile and Smoothness                              |
| WYDOT T-515 IPV         | High Speed Inertial Profiler Worksheet                         |
| WYDOT T-515 M           | Smoothness Assessment Report                                   |
| WYDOT T-515 SR          | Smoothness Testing Summary Report                              |
|                         | $\sim$ $\sim$ $\sim$   |

Procedure: 1. Ensure profile analysis is completed according to WYDOT 402.0.
2. Perform smoothness evaluation according to following table (contractor):

File name format according to AASHTO R 56, Sections 8.3.1.1 through 8.3.1.5 except 4th character is 'E' signifying smoothness evaluation.

#### Note (for Plant Mix Pavement):

Upon receipt of Form T-515 SR, *Smoothness Testing Summary Report*, and original Spreadsheet Summary as prepared by the HSIP operator and submitted by the contractor, the engineer will check for discrepancies in data; examples of Form T-515 SR and Spreadsheet Summary are included in this section.

If the engineer has any questions, submit data to WYDOT Materials Program for review.

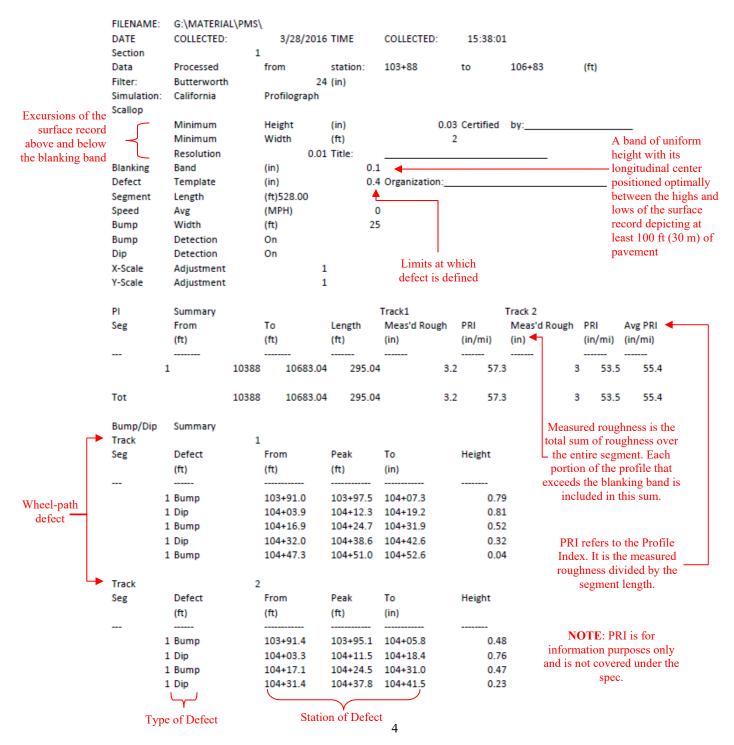
|  | (Rev. 10-18)                                      |  |  |  |
|--|---|--|--|--|
| Concrete Pavement  | Plant Mix Pavement                                |  |  |  |
| a. Measure surface variation of wheel paths using HSI                            |   |  |  |  |
| (allow system to achieve operational stability per manufacturer's recommendation |   |  |  |  |
| then collect raw profile data at appropriate                                     | e roadway speed).                                 |  |  |  |
| b. Repeat step a twice; total of 3 runs  |   |  |  |  |
| c. Submit flash/thumb drive to engineer; raw profile da                          | ata files in <b>.ppf</b> format.                  |  |  |  |
| d. Process/filter raw profile data (post-run) using follow                       | wing parameters:                                  |  |  |  |
| Short Wavelength (low pass filter) = $2.00$                                      | feet [0.60 m]                                     |  |  |  |
| Long Wavelength (high pass filter) = $300$                                       |   |  |  |  |
| Cut-off Wavelength (3rd order Butterwort   | th filter) = $24$ inch [ $610$ mm]                |  |  |  |
| e. Calculate pavement parameter (every road segment;                             | 0.1 mile; use ProVAL software).                   |  |  |  |
| PI (Profile Index)   | IRI (International Roughness Index);              |  |  |  |
| Full section excluding bridge deck   | Full section excluding Bridge Deck                |  |  |  |
| Use the following parameters:  |   |  |  |  |
|  | Note: ProVAL calculates 'MRI'; 'mean'             |  |  |  |
| Blanking Band, $max = 0.10$ inch [2.5 mm]  | or average of both wheel paths.                   |  |  |  |
| Re-center, min $= 0.10$ mile $[0.16$ km]   | 1. Calculate average for full length of           |  |  |  |
| Scallop:   | project pavement (per SS-400B):                   |  |  |  |
| Height, $min = 0.03$ inch [0.75 mm]  | i. IRI,   |  |  |  |
| Width, $min = 2.00$ feet [0.60 m]  | ii. Standard Deviation,                           |  |  |  |
| Rounding increment, $max = 0.01$ inch [0.25 mm]                                  | iii. Length.                                      |  |  |  |
| Segment length, max = $528$ feet [161 m]   | 2. Record values on Form T-515 SR;                |  |  |  |
| Lane width in feet   | sign and submit to engineer.                      |  |  |  |
| f. Engineer calculates pay adjustment/assessment for p                           |   |  |  |  |
|  | SS-400B;  |  |  |  |
|  | Complete Form T-515 M as follows:                 |  |  |  |
|  | 1. Copy data from Form T-515 SR,                  |  |  |  |
|  | 2. Calculate and record:                          |  |  |  |
| SS-400A, Section 414;  | Average (all 3 runs);                             |  |  |  |
|  | i. IRI,   |  |  |  |
| All pay adjustments, pay potentials, etc,  | ii. Standard deviation,                           |  |  |  |
| are based upon individual wheel paths;   | iii. Total surface area.                          |  |  |  |
| individual segments (0.1 mile sections);   | 3. Calculate/record (for surface type):           |  |  |  |
| total by summing all segments.   | i. Chart x-Value,                                 |  |  |  |
|  | ii. Chart y-Value,<br>(i.e., \$ Change per Area), |  |  |  |
|  | iii. Total Pay Assessment (+/-).                  |  |  |  |
|  | 4. Review and sign form; see example              |  |  |  |
|  | form in this section.                             |  |  |  |
|  |   |  |  |  |

NOTE: Define a segment as a continuous paved length that is the width of the land and approximately 0.1 mi [0.16 km] long.

#### Example 'MUST-GRIND' Analysis/Report

#### (for Concrete Pavement)

#### SIMULATED PROFILEOGRAPH REPORT OF PAVEMENT SMOOTHNESS



#### Explanatory Notes, Forms, and Reports (for Plant Mix Pavement):

- Spreadsheet Summary (example included in this section); prepared by the HSIP operator and submitted by the contractor:
  - a. 'As Collected' Section -

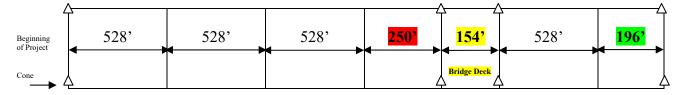
Data includes all measurements (surface variation) including exempted sections. Data is exact duplicate of measurement output from HSIP. Examples of North and South bound mainline HSIP data output are included.

b. 'Modified' Section -

Data includes all measurements (surface variation) <u>excluding exempted sections</u>. Exempted (removed) sections are highlighted and reason for exemption is noted. At far right is column labeled "WT IRI" or Weighted IRI; calculated as distance multiplied by IRI.

- 1. Exempt Sections;
  - i. HSIP generates data in 0.1 mile sections. The only time a section will not be 0.1 mile is when a trigger is set prior to an exempt section. A 'short' section indicates each trigger. In diagram below and example spreadsheet summary, several 528 foot (0.1 mile) sections are followed by a 'short' or trigger section (e.g., 250 ff, 196 ft, 425 ft, 149 ft, 229 ft, etc) with exempt section immediately following. As example in diagram below, the trigger or 'short' section is 250 ff followed by the exempt section of 154 feet, which is a bridge deck. The next section after the bridge deck is 528 feet, showing resumption of normal data sampling interval.
  - ii. The 'short' section prior to the trigger is less than 50 ft in length.

Graphically:



## Example HSIP Data Output

### (for Plant Mix Pavement)

| FILENAME:<br>DATE<br>OPERATOR:<br>ROUTE:<br>SEGMENT<br>SPEED | Y:\PMS\Sarah\<br>COLLECTED:<br>John<br>HWY 212<br>LENGTH:<br>LIMIT: | 7/20/2018<br>Smith<br>HDRLANE: | -     | IRI.P01<br>COLLECTED:<br>Laramie<br>East(+) | 11:38:33 |         |
|--|---|--------------------------------|-------|---|----------|---------|
| Feet   | IN/MI   |                                |       |   |          |         |
| Rough  | _   |                                |       |   |          |         |
| From   | То  | Dist                           | IRI 1 | IRI 2                                       | Avg      | Message |
|  | 528.02  | 528                            | 43.5  | 38.9  | 41.2     | (R) (S) |
| 528.02   |   |                                |       |   |          | (K) (3) |
| 1055.99  |   |                                |       |   |          |         |
| 1584.01  |   |                                |       |   |          |         |
| 2111.97  | 2639.99   | 528                            | 24.3  | 24.5  | 24.4     |         |
| 2639.99  | 3168.01   | 528                            | 17.3  | 20.5  | 18.9     |         |
| 3168.01  | 3695.98   | 528                            | 22.1  | 23.9  | 23       |         |
| 3695.98  | 3 4224  | 528                            | 20.3  | 18.2  | 19.3     |         |
| 4224   | 4752.02   | 528                            | 25.7  | 24.6  | 25.1     |         |
| 4752.02  | 5279.99   | 528                            | 24.3  | 24.2  | 24.2     |         |
| 5279.99  | 5808.01   | 528                            | 29.9  | 26.9  | 28.4     |         |
| 5808.01  | 6335.97   |                                |       | 18.3  |          |         |
| 6335.97  | 6863.99   | 528                            | 23.6  | 20.8  | 22.2     |         |
| 6863.99  |   |                                |       |   |          |         |
| 7392.01  |   |                                |       |   |          |         |
| 7919.98  |   |                                |       |   |          |         |
| 8448   |   |                                |       |   |          |         |
| 8976.02  |   |                                |       |   |          |         |
| 9503.99  |   |                                |       |   |          |         |
| 10032.01<br>10559.97   |   |                                |       |   |          |         |
| 10535.57   |   |                                | 236.5 |   |          | (2)     |
| 10758.07   |   |                                |       |   |          |         |
| 11286.09   |   |                                |       |   |          | (3)     |
| 11814.05   |   |                                |       |   |          |         |
| 12342.07   |   |                                |       |   |          |         |
| 12870.04   |   |                                |       |   |          |         |
| 13398.06   | 13926.08  | 528                            | 27.1  | 26.9  | 27       |         |
| 13926.08   | 14454.05  | 528                            | 30.9  | 27.4  | 29.2     |         |
| 14454.05   | 14982.07  | 528                            | 21    | 25.9  | 23.4     |         |
| 14982.07   | 15510.09  | 528                            | 26.8  | 23.6  | 25.2     |         |
| 15510.09   | 16038.05  | 528                            | 26.1  | 25.3  | 25.7     |         |
| 16038.05   | 16566.07  | 528                            |       |   | 23.6     |         |
| 16566.07   | 17094.04  | 528                            | 19.7  | 18.8  | 19.2     |         |
|  |   |                                |       |   |          |         |
| C  | 17094.04  | 17094                          | 34.1  | 33.8  | 33.9     |         |

## **Example Spreadsheet Summary**

## (Plant Mix Pavement)

| eet         | IN/MI    |       |       |       |       |         |          |         |       |             |        |      |         |         |
|-------------|----------|-------|-------|-------|-------|---------|----------|---------|-------|-------------|--------|------|---------|---------|
| s Collected |          |       |       |       |       |         | Modified |         |       |             |        |      |         |         |
| rom         | То       | Dist  | IRI 1 | IRI 2 | Avg   | Message | From     | То      | Dist  | IRI 1       | IRI 2  | Avg  | WT IRI  | Message |
|             |          |       |       |       |       |         |          |         |       |             |        |      |         |         |
| 0           |          | 528   |       | 38.9  |       | (R) (S) | 0        |         | 528   | 43.5        | 38.9   |      |         |         |
| 528.02      | 1055.99  | 528   | 20.3  | 20.4  | 20.3  |         | 528.02   |         | 528   | 20.3        | 20.4   |      | 10718.4 |         |
| 1055.99     | 1584.01  | 528   | 24.4  | 22.7  | 23.6  |         | 1055.99  | 1584.01 | 528   | 24.4        |        |      | 12460.8 |         |
| 1584.01     | 2111.97  | 528   | 20.5  | 19.9  | 20.2  |         | 1584.01  | 2111.97 | 528   | 20.5        | 19.9   |      | 10665.6 |         |
| 2111.97     | 2639.99  | 528   | 24.3  | 24.5  | 24.4  |         | 2111.97  | 2639.99 | 528   | 24.3        |        |      | 12883.2 |         |
| 2639.99     |          | 528   |       | 20.5  | 18.9  |         | 2639.99  | 3168.01 | 528   | 17.3        |        |      | 9979.2  |         |
| 3168.01     | 3695.98  | 528   | 22.1  | 23.9  | 23    |         | 3168.01  |         | 528   | 22.1        | 23.9   |      | 12144   |         |
| 3695.98     |          | 528   | 20.3  | 18.2  | 19.3  |         | 3695.98  | 4224    | 528   | 20.3        | 18.2   |      | 10190.4 |         |
| 4224        |          | 528   |       | 24.6  | 25.1  |         | 4224     |         | 528   | 25.7        | 24.6   |      |         |         |
| 4752.02     | 5279.99  | 528   | 24.3  | 24.2  | 24.2  |         | 4752.02  | 5279.99 | 528   | 24.3        |        |      | 12777.6 |         |
| 5279.99     | 5808.01  | 528   | 29.9  | 26.9  | 28.4  |         | 5279.99  | 5808.01 | 528   | 29.9        | 26.9   | 28.4 | 14995.2 |         |
| 5808.01     | 6335.97  | 528   | 21.6  | 18.3  | 19.9  |         | 5808.01  | 6335.97 | 528   | 21.6        | 18.3   |      | 10507.2 |         |
| 6335.97     | 6863.99  | 528   | 23.6  | 20.8  | 22.2  |         | 6335.97  | 6863.99 | 528   | 23.6        |        |      | 11721.6 |         |
| 6863.99     |          | 528   | 46    | 35.5  | 40.7  |         | 6863.99  | 7392.01 | 528   | 46          |        |      | 21489.6 |         |
| 7392.01     |          | 528   | 27.7  | 24.7  | 26.2  |         | 7392.01  |         | 528   | 27.7        | 24.7   |      | 13833.6 |         |
| 7919.98     |          | 528   | 25.7  | 22.1  | 23.9  |         | 7919.98  | 8448    | 528   | 25.7        | 22.1   |      | 12619.2 |         |
| 8448        | 8976.02  | 528   | 28.3  | 23.9  | 26.1  |         | 8448     | 8976.02 | 528   | 28.3        | 23.9   | 26.1 | 13780.8 |         |
| 8976.02     | 9503.99  | 528   | 26.3  | 26.5  | 26.4  |         | 8976.02  | 9503.99 | 528   | 26.3        | 26.5   | 26.4 | 13939.2 |         |
| 9503.99     | 10032.01 | 528   | 26.5  | 26.6  | 26.6  |         | 9503.99  | 10032   | 528   | 26.5        |        |      | 14044.8 |         |
| 10032.01    | 10559.97 | 528   | 32.3  | 35.8  | 34    |         | 10032    | 10560   | 528   | 32.3        | 35.8   | 34   | 17952   |         |
| 10559.97    | 10585.73 | 26    | 60.7  | 53    | 56.8  |         |          |         | Leng  | th under 50 | ) Feet |      |         | exempt  |
| 10585.73    | 10758.07 | 172   | 236.5 | 289.4 | 262.9 |         |          |         |       | Bride Deck  | t.     |      |         | exempt  |
| 10758.07    | 11286.09 | 528   | 43.2  | 40.2  | 41.7  | (S)     | 10758.1  | 11286.1 | 528   | 43.2        | 40.2   | 41.7 | 22017.6 | (S)     |
| 11286.09    | 11814.05 | 528   | 31.5  | 25.4  | 28.5  |         | 11286.1  | 11814.1 | 528   | 31.5        | 25.4   | 28.5 | 15048   |         |
| 11814.05    | 12342.07 | 528   | 22.6  | 20.5  | 21.5  |         | 11814.1  | 12342.1 | 528   | 22.6        | 20.5   | 21.5 | 11352   |         |
| 12342.07    | 12870.04 | 528   | 27.2  | 25.6  | 26.4  |         | 12342.1  | 12870   | 528   | 27.2        | 25.6   | 26.4 | 13939.2 |         |
| 12870.04    | 13398.06 | 528   | 29.9  | 24    | 27    |         | 12870    | 13398.1 | 528   | 29.9        | 24     | 27   | 14256   |         |
| 13398.06    | 13926.08 | 528   | 27.1  | 26.9  | 27    |         | 13398.1  | 13926.1 | 528   | 27.1        | 26.9   | 27   | 14256   |         |
| 13926.08    | 14454.05 | 528   | 30.9  | 27.4  | 29.2  |         | 13926.1  | 14454.1 | 528   | 30.9        | 27.4   | 29.2 | 15417.6 |         |
| 14454.05    | 14982.07 | 528   | 21    | 25.9  | 23.4  |         | 14454.1  |         | 528   | 21          | 25.9   | 23.4 | 12355.2 |         |
| 14982.07    | 15510.09 | 528   | 26.8  | 23.6  | 25.2  |         | 14982.1  | 15510.1 | 528   | 26.8        | 23.6   | 25.2 | 13305.6 |         |
| 15510.09    | 16038.05 | 528   | 26.1  | 25.3  | 25.7  |         | 15510.1  | 16038.1 | 528   | 26.1        | 25.3   | 25.7 | 13569.6 |         |
| 16038.05    | 16566.07 | 528   | 24.1  | 23.2  | 23.6  |         | 16038.1  | 16566.1 | 528   | 24.1        | 23.2   | 23.6 | 12460.8 |         |
| 16566.07    | 17094.04 | 528   | 19.7  | 18.8  | 19.2  |         | 16566.1  | 17094   | 528   | 19.7        | 18.8   | 19.2 | 10137.6 |         |
|             | 47004.5  | 4705  |       |       |       |         |          |         |       |             |        |      | 40000   |         |
| 0           | 17094.04 | 17094 | 34.1  | 33.8  | 33.9  |         |          | Σ       | 16896 |             |        | Σ    | 439824  |         |
|             |          |       |       |       |       |         |          |         |       | Run 1       |        |      |         |         |
|             |          |       |       |       |       |         |          |         |       | IRI =       | 26.03  |      |         |         |
|             |          |       |       |       |       |         |          |         |       | Std Dev =   | 5.96   |      |         |         |
|             |          |       |       |       |       |         | 1        |         |       | Length =    | 16896  |      |         |         |

# WYOMING DEPARTMENT OF TRANSPORTATION SMOOTHNESS TESTING SUMMARY REPORT

Form T-515 SR (Rev. 10-18)

| Project No.(s):        | N216XXX             | Test Date:                  | 7/1/2016               |
|------------------------|---------------------|-----------------------------|------------------------|
| Engineer(s):           | Resident Engineer   | Prime Contractor:           | Prime Contractor       |
| Route:                 | US 20/26, ML34      | Location:                   | Natrona - Powder River |
| Beginning MP:          | 30.06               | Ending MP:                  | 39.60                  |
| Profile Contractor:    | Profiler Contractor | Software Used:              | ICC                    |
| Vehicle Info:          | 4208                | Operator:                   | John Smith             |
| cope / Smoothing Opps: |                     | 2" mill, 1" level, 2.5" HPM | /2                     |

#### **IRI Data Summary**

| Run:                | 1      | 2      | 3      |
|---------------------|--------|--------|--------|
| IRI <sub>i</sub> :_ | 45.89  | 46.01  | 45.78  |
| StDev:_             | 5.74   | 5.40   | 5.86   |
| Tested Length:      | 100743 | 100738 | 100748 |

I attest the above is valid for the project listed and free from known errors.

| Printed Name: John Smith               | Signature: John Smíth   |
|--|-------------------------|
| Submitted By: Printed Name: Many Davis | Signature: Marri Darris |
| Submitted By: Printed Name: Mary Davis | Signature: Mary Davis   |

#### Attach this form to top of spreadsheet calculations

#### WYOMING DEPARTMENT OF TRANSPORTATION Form T-515 M (Rev. 10-18) SMOOTHNESS ASSESSMENT REPORT PMWC Non - PMWC Project No.(s): N216XXX Test Date: 7/1/2016 Engineer(s): Resident Engineer Prime Contractor: Prime Contractor Route: US 20/26, ML34 Location: Natrona - Powder River Beginning MP: 30.06 Ending MP: 39.60 Profile Contractor: Profiler Contractor Software Used: ICC Vehicle Cert. #: 4208 **Operator:** John Smith Scope / Smoothing Opps: 2" milling, 1" leveling, 2.5" HPM / 2 Average IRI (in/mi): Results: 45.89 Avg Std Dev of IRI: 5.67 Chart Input Value (X): 50.14333333 \$ Change Per (yd<sup>2</sup>): \$ 0.30 Total Surface Area (yd<sup>2</sup>): 134324 Total Pay Assessment: \$ 40,297.20 **IRI Data Summary** Run: 1 2 3 45.89 45.78 IRIi: 46.01 StDev: 5.74 5.40 5.86 **Tested Length:** 100743 100738 100748 Lane Width: 12 12 12 Total Surface Area = 134324 134317 134331 Prepared By: Printed Name: Signature: Checked By: Printed Name: Signature: Engineer: Resident Engineer Signature

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#### SAMPLING MIX

- Scope: This procedure is adopted from AASHTO T 168. This procedure involves sampling mix after it has been processed through the plant. It describes sampling from a haul truck, windrow, augers at the paver, and the roadway surface after placement.
  - Note: The term "mix" will be used to reference hot plant mix, recycled hot plant mix, warm plant mix, etc.
  - CAUTION: This procedure may present considerable risks if conducted in an unsafe manner. Due care must be used at all times. This procedure may involve hazardous materials, operations, and equipment. It is your responsibility to establish appropriate safety practices.
- Use: This procedure is used to obtain representative samples of mix before it is compacted. Samples may be used for quality control, quality acceptance, and verification of mix volumetrics and voidless unit weight. An authorized WYDOT inspector will be present for sampling.
- Apparatus: Ensure all tools and equipment are clean and dry before sampling.
  - Scoop, 4 inch wide x 8 inch long x 1<sup>1</sup>/<sub>2</sub> inch deep OR square nosed shovel, approximate blade size of 9 inch wide x 11 inch long x 2 inch deep
  - 2. Cylinder cans, suggest 6 inch in diameter x 12 inch tall, with lids
  - 3. Protective garments, to keep mix or heated surfaces from burning skin
  - 4. Funnel or similar device to minimize material loss Funnel top width should be at least 3 inch wider than the cylinder can, (Figure 1 of this section), suggested
  - 5. Sampling platform or ladder for truck sampling
  - 6. Round or square pan, approximately 15 inch diameter and 3<sup>1</sup>/<sub>2</sub> inch deep for sampling from paver augers

| Reference  |              |  |
|------------|--------------|--|
| Documents: | AASHTO T 168 | Standard Method of Test for Sampling Bituminous Paving |
|            |              | Mixtures   |
|            | WYDOT 401    | WYDOT Standard Specifications                          |
|            | WYDOT 411.0  | Transporting Mix Samples                               |
|            | WYDOT 419.0  | Voidless Unit Weight Verification and Field Adjustment |

Procedure: Sampling should be random and representative of the entire mix. (Refer to *WYDOT Standard Specifications* Section 401.) Be sure that the sampling area is safe. The point of sampling will be designated during the pre-construction or pre-paving meeting. It is essential that samples be collected the same way every time. Avoid sampling the initial or final few tons delivered to improve the chance of getting a representative sample. The field mix sample will consist of three samples as described in WYDOT 419.0; typically nine cylinder cans for volumetric verification, divided as follows;

One sample, three cylinders to be tested by the contractor

One sample, three cylinders submitted to WYDOT, and

One sample, three cylinders retained by WYDOT as a referee sample.

- 1. Sampling from Windrows
  - a. When sampling from a windrow, select a location in the middle third of a truck load. Note the truck type.
  - b. Remove the top 2 inches to 4 inches of mix. This is done by carefully inserting a clean, dry square nosed shovel into the top center portion of the windrow, then placing the removed material aside. Avoid flattening the mix since this may cause segregation.
  - c. Insert the shovel into the cleared space at approximately a 45 degree angle. Push the shovel into the windrow to about 75 percent of the shovel head length within about 3 inches of the bottom of the windrow, whichever is less. Avoid contaminating the sample with the underlying material.
  - d. When the shovel is full, lift it straight up and out of the windrow. Keep the shovel level.
  - e. Transfer the material from the shovel into a cylinder can with the funnel placed on top. Collect enough mix to fill the cylinder can, generally one shovel-full per cylinder.
    - Note: The intent is to collect a representative sample of adequate quantity. If a cylinder is not full, another cylinder should be provided. Likewise, if a shovel full is more than a cylinder, do not overfill; split into two cylinders.

2. Sampling from Trucks

Be sure that the sampling area is safe. Tell the haul truck driver that you are sampling.

- Note: In addition to regular protective garments, protective foot wear while standing in the mix is strongly recommended. Be careful while in the truck box, staying at least one foot away from the truck box sides.
- a. For smaller trucks, particularly smaller end-dump trucks, visually divide the load into four quarters. Remove the top 2 inches to 4 inches from a quadrant and place the removed material aside. One sample, two to three cylinder cans, should represent a quadrant.
- b. When larger trucks are loaded, piles of mix are placed in several locations in the truck box. Excavate with the shovel at least two transverse trenches approximately 4 inches to 6 inches deep. The trenches should cross the truck bed at each pile. One sample, two to three cylinder cans, should represent each transverse trench.
  - 1. Collect the sample by inserting the shovel into the trench or cleared quadrant at an approximate 45 degree angle.
  - 2. When the shovel head is about 75 percent of the way into the mix, slowly lift the shovel straight up and out of the material.
  - 3. Keep the shovel level and retain as much material as possible. Empty the material from the shovel into a cylinder can with a funnel placed on top. Collect enough mix to fill each cylinder can. Place the lid(s) on top.
- 3. Sampling from Paver Augers

#### CAUTION: This procedure may present considerable risks if conducted in an unsafe manner. Use due care at all times.

Note: Ensure adequate flow before obtaining samples.

Observe the paver augers from the center slat conveyors to both sides of the screed. The amount of material carried in the augers should be consistent. The depth of material in the augers should be in the middle of the auger shaft or slightly higher for its entire length. The augers should be operating smoothly, not surging, and creating a consistent head of material.

Observe the paver speed, inconsistent speed results in fluctuating material flow. The paver hopper between truck loads should be partially full. The mix should be maintained near or above the bottom of the flow gates.

**Be sure the paver operator knows you are sampling.** Try to sample the approximate middle third of a truck load.

- a. Sample as close as possible to the end of the auger guard, directly below the flow sensor or next to the paver wheel or track.
- b. Place a flat bottom scoop or square nosed shovel on the existing surface parallel to the direction of motion of the paver.
- c. Allow the mix to flow into the scoop or shovel without moving the scoop or shovel.
- d. When the scoop or shovel is full, lift the scoop or shovel up and toward you slowly, trying to maintain all material on the scoop or shovel.
- e. Empty the scoop directly into a cylinder can. Collect enough material to fill the cylinder cans.
- 4. Sampling from the Roadway behind the Paver
  - a. Select a random area as directed by the engineer where the mixture appears uniform and displays no visible segregation.
  - b. Notify the paver personnel that you are getting a sample.
  - c. Obtain the sample at minimum of one foot from the edge of the mixture being placed. If mix leveling is being placed, obtain the sample from the thickest depth possible. Select an area large enough to fill one cylinder can.

- d. Subsequent samples should come from the same proximity as the first sample.
  - 1. Outline the sample area with a square shovel.
  - 2. Remove all the material (including fines) in the sample area.
  - 3. Transfer the material from the shovel into a cylinder can with the funnel placed on top.

Be careful not to pick up any of the underlying material, such as tack. Care should be taken not to disturb the sampling area any more than necessary to obtain the representative sample. Extreme care should be taken to obtain all the fine and coarse particles and to minimize segregation in the sample.

Immediately after obtaining the sample, the contractor will fill the sampled area with loose mix obtained from the paver hopper or the material transfer (live bottom) stream. The mix for filling the sampled area may be obtained prior to sampling. After filling the area, the contractor should smooth out the area with a rake before rolling.

Transport: Transport samples to the testing facility in accordance with WYDOT 411.0.

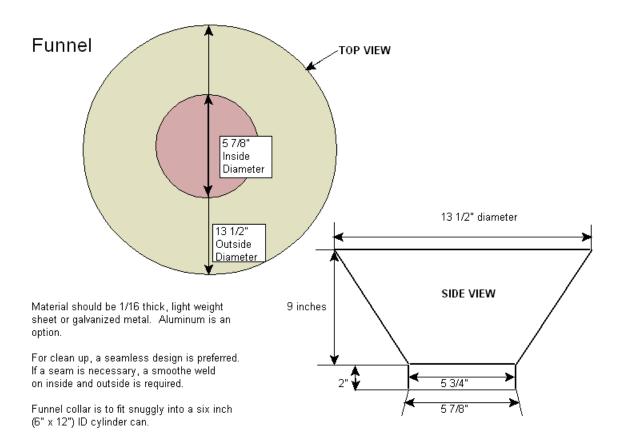


Figure 1. Funnel Diagram

#### TRANSPORTING MIX SAMPLES

- Scope: This procedure describes transporting mix (hot plant mix, recycled hot plant mix, warm plant mix) samples from the sampling site to a testing facility. It is intended to minimize temperature loss from mix sampled in the field according to WYDOT 410.0. Temperature loss of approximately 1 °F per minute can be expected when following this procedure.
- Use: This procedure is to be used for handling times less than 45 minutes. For travel times greater than 45 minutes, reheating will be required according to WYDOT 412.0. Mix samples will be in a workable state until subsequent testing is done in accordance with WYDOT 414.0. This procedure reduces reheating time for mix samples.
- Apparatus: 1. Five gallon buckets with lids, lined on the sides, bottom, and top with loosely placed, paper backed fiberglass or semi-ridged 6 inch ID insulation
  - 2. Insulated safety gloves
  - 3. Cylinder cans, 6 inch in diameter x 12 inch, with lids

#### Reference

| Documents: | WYDOT 410.0 | Sampling Mix   |
|------------|-------------|--|
|            | WYDOT 412.0 | Reheating Mix Samples                                |
|            | WYDOT 413.0 | Moisture Content of Mix                              |
|            | WYDOT 414.0 | Marshall and Superpave Mix Design and Mix Volumetric |
|            |             | Verification Procedure                               |

- Procedure: Obtain the sample following procedure WYDOT 410.0. The lid should be on the cylinder can. Carefully put the cylinder can with lid into the insulated five gallon bucket. Place the top piece of insulation on top of the cylinder lid. Secure the insulated lid on the five gallon bucket.
  - Note: To reduce handling of the hot cylinder can, place the cylinder inside the insulated bucket prior to sampling.

At the testing facility, determine the sample temperature. If the temperature loss is less than 50  $^{\circ}$ F, immediately obtain a sample for the moisture content of the mixture. Determine the moisture content of the mix in accordance with WYDOT 413.0. The moisture content of the mix cannot be obtained from a sample that has cooled more than 50  $^{\circ}$ F.

WYDOT 411.0 (Rev. 01-15)

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#### **REHEATING MIX SAMPLES**

- Scope: This procedure describes reheating (hot plant mix, recycled hot plant mix, warm plant mix) mix samples in a testing facility.
- Use: This procedure is used to attain appropriate temperatures of field sampled mix prior to volumetric verification testing or voidless unit weight verification testing.
- Apparatus: Ventilated oven capable of maintaining temperature for tests to be performed.

Reference

| Documents: | AASHTO T 308             | Standard Method of Test for Determining the Asphalt<br>Binder Content of Hot Mix Asphalt (HMA) by the Ignition<br>Method |
|------------|--------------------------|--|
|            | WYDOT 401<br>WYDOT 414.0 | WYDOT Standard Specifications<br>Marshall and Superpave Mix Design and Mix Volumetric<br>Verification Procedure          |

Procedure: Place the appropriate quantity of the sample into a preheated oven that is set at the appropriate reheating temperature.

The reheating temperatures should be determined from the following table according to the asphalt binder grade used in the sample being reheated.

| PG 58-28       | 280 °F                    |
|----------------|---------------------------|
| PG 64-22       | 285 °F                    |
| PG 64-28       | 290 °F                    |
| PG 70-28       | 300 °F                    |
| PG 76-28       | 310 °F                    |
| Warm Plant Mix | CONTACT MATERIALS PROGRAM |

The Materials Program will provide the appropriate reheating temperatures for asphalt binder not included in the table above or for warm plant mix.

Heat the sample until the sample reaches a uniform temperature throughout.

For ignition oven sample temperatures, reference AASHTO T 308.

WYDOT 412.0 (Rev. 01-15)

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#### MOISTURE CONTENT OF MIX

- Scope: This procedure determines the moisture content of a sample of mix (hot plant mix, recycled hot plant mix, warm plant mix) by evaporation.
- Use: This is a procedure to determine whether the amount of water in the mix exceeds the specified amount.

#### Apparatus: 1. Scale capable of 0.0001 lb [0.1 g] accuracy

- 2. Heat source, such as an electric or gas hot plate, electric heat lamps, or a ventilated convection oven capable of maintaining the temperature surrounding the sample at  $230 \pm 9$  °F
- 3. Insulated safety gloves
- 4. Cylinder cans, 6 inch in diameter x 12 inch tall, with lids
- 5. Round or square batch pan, approximately 15 inch diameter or square x  $3\frac{1}{2}$  inch deep
- 6. Round sample pan for use in oven, 12 inch diameter x 3 inch deep
- 7. Flat bottomed scoop, approximately 4 inch wide x 8 inch long 1<sup>1</sup>/<sub>2</sub> inch deep

#### Reference

| Documents: | AASHTO T 168 | Standard Method of Test for Sampling Bituminous Paving  |
|------------|--------------|---|
|            |              | Mixtures  |
|            | WYDOT 410.0  | Sampling Mix  |
|            | WYDOT 411.0  | Transporting Mix Samples                                |
|            | WYDOT T-158F | Mix Verification of Plant Produced Bituminous Plant Mix |
|            |              | Pavement  |

- Procedure: Perform this before substantial heat loss occurs
  - 1. Obtain sample of the mix.

Note: Follow AASHTO T 168 or WYDOT 410.0 for sampling locations.

- 2. Transport samples according to WYDOT 411.0.
- 3. Empty the sample into the batch pan.
  - a. Weigh the sample pan.
  - b. Using a hot scoop, place 1 to 3 lb in the sample pan. Weigh the pan and sample.
  - c. Place the sample in the heat source and dry thoroughly. Reweigh the pan and sample. The sample is dry when 5 minutes of additional heating causes less than 0.1% additional weight loss.

WYDOT 413.0 (Rev. 09-16)

> Very rapid heating may cause some particles to explode, resulting in some particle loss. If a source of heat other than the temperature controlled oven is used, stir the sample during drying to accelerate the operation and prevent localized overheating.

Calculations: Calculate the total moisture content as follows:

| b |
|---|
| b |
| b |
| b |
| b |
|   |
|   |

Report: Report the results on Form T-158F.

# MARSHALL AND SUPERPAVE MIX DESIGN AND MIX VOLUMETRIC VERIFICATION PROCEDURE

- Scope: This procedure describes the use of the Marshall or the Superpave apparatus and techniques for two purposes. It describes the mix design procedure including the batching calculations needed to prepare a job mix formula (JMF). In addition, it describes how the Marshall or the Superpave apparatus and mix design procedures are used to verify that construction mixes conform to the volumetric specifications. Included are the mix design volumetric calculations and examples.
- Use: This procedure will be used either to generate mix designs or to check the conformance of construction mixes to the job mix formula and mix volumetric control limits. This method is applicable only to asphalt paving mixtures containing aggregates with nominal maximum sizes of 1 inch or less.

In general, the contractor is responsible for submitting a construction mix. The laboratory and personnel performing mix design testing must be accredited. After the contractor has submitted the mix design and split samples, if required, to the engineer, the engineer will review the mix design for completeness and compliance. Once the engineer has ensured that the mix design meets the contract requirements, the mix design and any associated samples will be submitted to the Materials Program.

#### Reference

Documents:

| Asphalt Institute MS-2 | Mix Design Methods for Asphalt Concrete and Other Hot       |
|------------------------|---|
|                        | Mix Types   |
| AASHTO M 320           | Standard Specification for Performance-Graded Asphalt       |
|                        | Binder  |
| AASHTO M 323           | Standard Specification for Superpave Volumetric Mix         |
|                        | Design  |
| AASHTO R 30            | Standard Practice for Mixture Conditioning of Hot Mix       |
|                        | Asphalt (HMA)   |
| AASHTO R 35            | Standard Practice for Superpave Volumetric Design for Hot   |
|                        | Mix Asphalt (HMA)   |
| AASHTO T 11            | Standard Method of Test for Materials Finer than 75-µm      |
|                        | (No. 200) Sieve in Mineral Aggregates by Washing            |
| AASHTO T 27            | Standard Method of Test for Sieve Analysis of Fine and      |
|                        | Coarse Aggregates   |
| AASHTO T 84            | Standard Method of Test for Specific Gravity and Absorption |
|                        | of Fine Aggregate   |
| AASHTO T 85            | Standard Method of Test for Specific Gravity and Absorption |
|                        | of Coarse Aggregate   |
| AASHTO T 100           | Standard Method of Test for Specific Gravity of Soils       |
| AA51110 I 100          | Sumuma memora of Tesi for specific Oravity of sous          |

| AASHTO T 164               | Standard Method of Test for Quantitative Extraction of                          |
|----------------------------|---|
|                            | Asphalt Binder from Hot Mix Asphalt (HMA)                                       |
| AASHTO T 166               | Standard Method of Test for Bulk Specific Gravity of                            |
|                            | Compacted Hot Mix Asphalt (HMA) Using Saturated                                 |
|                            | Surface-Dry Specimens   |
| AASHTO T 209               | Standard Method of Test for Theoretical Maximum Specific                        |
|                            | Gravity and Density of Hot Mix Asphalt (HMA)                                    |
| AASHTO T 228               | Standard Method of Test for Specific Gravity of Semi-Solid<br>Asphalt Materials |
| AASHTO T 245               | Standard Method of Test for Resistance to Plastic Flow of                       |
| AASIIIO I 245              | Bituminous Mixtures Using Marshall Apparatus                                    |
| AASHTO T 248               | Standard Method of Test for Reducing Samples of Aggregate                       |
| AASHIO I 240               |   |
| A A SUTO T 260             | to Testing Size   |
| AASHTO T 269               | Standard Method of Test for Percent Air Voids in Compacted                      |
|                            | Dense and Open Asphalt Mixtures   |
| AASHTO T 283               | Standard Method of Test for Resistance of Compacted Hot                         |
|                            | Mix Asphalt (HMA) Mixtures to Moisture-Induced Damage                           |
| AASHTO T 304               | Standard Method of Test for Uncompacted Void Content of                         |
|                            | Fine Aggregate  |
| AASHTO T 308               | Standard Method of Test for Determining the Asphalt Binder                      |
|                            | Content of Hot Mix Asphalt (HMA) by the Ignition Method                         |
| AASHTO T 312               | Standard Method of Test for Preparing and Determining the                       |
|                            | Density of Hot Mix Asphalt (HMA) by Means of the                                |
|                            | Superpave Gyratory Compactor  |
| ASTM D5821                 | Standard Test Method for Determining the Percentage of                          |
|                            | Fractured Particles in Coarse Aggregate   |
| AI SP-2                    | Superpave Mix Design  |
| WYDOT 114.2                | WYDOT Standard Specifications   |
| WYDOT 401                  | WYDOT Standard Specifications   |
| WYDOT 803                  | WYDOT Standard Specifications   |
| WYDOT 410.0                | Sampling Mix  |
| WYDOT 411.0                | Transporting Mix Samples  |
| WYDOT 417.0                | Precision Statements for Comparing Contractor QA Results                        |
|                            | to WYDOT Verification Results   |
| WYDOT 419.0                | Voidless Unit Weight Verification and Field Adjustment                          |
| WYDOT 803.0                | Aggregate Sampling and Quantity   |
| WYDOT 804.0                | Aggregate Sampling  |
| WYDOT 805.0                | Sample Splitting by Mechanical Splitter   |
| WYDOT 810.0                | Soundness of Aggregate by Use of Sodium Sulfate or                              |
| WID01010.0                 | Magnesium Sulfate   |
| WYDOT 812.0                | Liquid Limit Test   |
|                            | •   |
| WYDOT 813.0<br>WYDOT 814.0 | Plastic Limit Test & Plasticity Index   |
|                            | Sieve Analysis of Combined Aggregate  |
| WYDOT 817.0                | Determining the Percentage of Fractured Faces in Coarse                         |
| WWDOT 010 0                | Aggregate   |
| WYDOT 818.0                | LA Abrasion Resistance (LAR)  |

| WYDOT 824.0  | Fine Aggregate Angularity                               |
|--------------|---|
| WYDOT 835.0  | Percentage of Flat and Elongated Particles in Coarse    |
|              | Aggregate   |
| WYDOT 836.0  | Fine Aggregate Sand Equivalent                          |
| WYDOT E-46   | Hot Plant Mix Job Mix Formula                           |
| WYDOT E-46A  | Hot Plant Mix Job Mix Formula (Non-QAQC)                |
| WYDOT T-158  | Bituminous Pavement Mix Design                          |
| WYDOT T-158F | Mix Verification of Plant Produced Bituminous Plant Mix |
|              | Pavement  |

#### **Mix Design Procedure**

- 1. For Superpave mix designs, follow AASHTO R 35, AASHTO R 30, and AASHTO T 312, except where the following procedure differs;
- 2. Sample the aggregate for mix designs according to WYDOT 803.0.

Typically, aggregate samples for the mix design are obtained when aggregate production hits the 25 percent mark. To ensure that the gradation used for the construction mix design is representative of the material produced, ensure that the samples are representative of the average gradation of the quality control samples. If the differences exceed the allowable difference in WYDOT 417.0, re-sample the stockpile and re-run the mix design. Submit the average quality control gradation from the stockpile, the mix design gradation, and the comparison results with the mix design. Ensure that the gradation samples submitted with the mix design for the mix design verification are split samples that were obtained at the same time as the samples for the mix design.

For recycled hot plant mix (RHPM) mix designs ensure that the samples are representative of the materials to be used during construction, Section 803.5.3 *WYDOT Standard Specifications*. RAP is a variable material; the sampling program is critical to identifying the properties typical of the RAP. Sampling procedures used to produce the RAP samples for the mix design must accurately represent the production milling. Take RAP samples from the pavement that is typical of the entire project. It is advisable to review core data that represents the length of the project before selecting sampling locations. RAP classification is necessary to prepare a representative mix design; a representative mix design is necessary to produce target gradation goals and achieve volumetric and density requirements. Careful sampling along with an informed selection of the target RAP gradation and asphalt content go a long way towards making construction consistent and producing a high-quality, durable pavement.

3. Determine the gradation of the coarse and fine aggregates used in the mix material according to WYDOT 814.0. The coarse material is material that is retained on a No. 4 sieve, or above. These separated materials are used in the mix design. They are generally separated on the <sup>3</sup>/<sub>4</sub> inch, <sup>1</sup>/<sub>2</sub> inch, <sup>3</sup>/<sub>8</sub> inch, and the No. 4 sieves. The fine material, material passing the No. 4 screen, is analyzed for gradation according to WYDOT 814.0, but

further separation for mix design batching is not required. Do this for all the aggregates used in the mix design.

Note: For some Superpave mix designs, batching the JMF gradation may be necessary to produce repeatable results. When this is determined to be necessary, indicate this on form E-46.

For RHPM, split each sack of RAP to ensure that the sample is representative of the entire sack. Split the material sampled from each sack according to WYDOT 805.0. Conduct an analysis of the sampled RAP's gradations and asphalt content, the sampling procedures, and any other factors that may influence the properties of the production milled RAP. Information about sampling, sampling locations, sampling methods, the production milling process, and data from cores should be reviewed.

- a. Determine the asphalt content and aggregate gradation of each of the RAP sacks with a chemical extraction (AASHTO T 164). Calculate an average gradation and asphalt content for the RAP samples.
- b. Average the extracted gradation samples from each sack to get an average RAP gradation.
- c. Select a target RAP gradation using the information described in the previous paragraph. Often this will be the same as the average of the RAP samples. It is important that the selected target gradation and asphalt content is close to the RAP gradation and asphalt content achieved during production. This selection is critical to the creation of a mix design that will work well in the field.
  - 1. Select a target RAP gradation and asphalt content that is representative of the anticipated production milled RAP based on information from the milled RAP samples, the cores, and any other factors that may influence the gradation or asphalt content of the production milled RAP.
- 4. Determine the Liquid Limit (LL), Plastic Limit (PL), and Plasticity Index (PI) of all fine aggregate fractions and sources using WYDOT 812.0 and WYDOT 813.0.
- 5. Determine the Bulk Specific Gravity of the fine and coarse aggregate for all fractions and sources using AASHTO T 84 and AASHTO T 85.
- 6. Determine the Los Angeles Abrasion Resistance (LAR) according to WYDOT 818.0.
- 7. Determine the aggregate soundness (MgSO<sub>4</sub>), if necessary, according to WYDOT 810.0.
- 8. Determine the Fractured Faces (WYDOT 817.0), the Fine Aggregate Angularity (WYDOT 824.0), and the Flat and Elongated Particles, 1:5 (WYDOT 835.0).
- 9. Multiply the percentage of each aggregate type (bin split percentage) by the percentage passing for each sieve size. Add these values for each sieve size. These summed values

must fall within the Wide Band Specifications for mix designs (Table 803.5.5-1 *WYDOT Standard Specifications*) and within the established Narrow Band Specifications (Table 401.4.13-1 and subsection 2.1 of 401.4.13.3.2 *WYDOT Standard Specifications*) or the Job Mix Formula and Control Limits for construction mixes.

For RHPM mix designs, the combined target RAP gradation multiplied by the RAP bin split percentage from the plans when combined with the virgin JMF must fall within the Wide Band Specifications (Table 803.5.5-1 *WYDOT Standard Specifications* and plans). The Narrow Band Specifications are applied to the virgin aggregate gradation.

#### A. Batching Calculations & Examples

1. Combined Aggregate Gradations and Bin Splits

Combine the aggregate at the selected proportions (bin split percentages) for each individual sample to be compacted. In Table A1 that follows, three bin splits representing three stockpiles are to be used.

Note: The percentage (%) of each split is a starting point when developing a Job Mix Formula (JMF). Experience to achieve a gradation within specification limits is a matter of trial and error and reasoning. The No. 4 is a good starting point, normally.

| Sieve Size                       | Wide Band<br>Specifications |     | C   | Stockpile<br>Coarse<br>n Splits | Fine | Filler                |
|----------------------------------|-----------------------------|-----|-----|---------------------------------|------|-----------------------|
|                                  | Min                         | Max | 55% | 35%                             | 10%  | Combined<br>Gradation |
| 1 inch                           | 100                         |     | 100 | 100                             | 100  | 100                   |
| <sup>3</sup> / <sub>4</sub> inch | 90 100                      |     | 97  | 100                             | 100  | 98                    |
| <sup>1</sup> / <sub>2</sub> inch | 55                          | 90  | 41  | 99                              | 100  | 67                    |
| No. 4                            | 45                          | 85  | 8   | 98                              | 96   | 48                    |
| No. 8                            | 30                          | 65  | 2   | 70                              | 72   | 33                    |
| No. 30                           | 5                           | 30  | 1   | 28                              | 33   | 14                    |
| No. 200                          | 2                           | 7   | 0.8 | 8.8                             | 16.2 | 5.1                   |

 Table Al. Combined Aggregate

Table Al is an example of the calculations used to establish whether a particular combination of aggregates falls within the Wide Band Specifications. Nominal

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maximum and maximum size are controlled by the crushing operations and mix design specifications.

Table A1 from the percent passing gradation shown is a <sup>3</sup>/<sub>4</sub> inch nominal maximum requirement, Table 803.5.5-1 WYDOT Standard Specifications.

Note: Aggregate gradation Wide Band is based on the nominal maximum size of the aggregate. The nominal maximum size is one size larger than the first sieve to retain more than 10 percent.

Maximum size is one sieve size larger than the nominal maximum size operations to provide an optimal mix design.

Combined gradations are calculated by multiplying the bin splits by the percentages passing each sieve. For example, on the No. 4 sieve, the combined gradation percentage passing is calculated as follows:

$$\mathbf{P} = \mathbf{A}\mathbf{a} + \mathbf{B}\mathbf{b} + \mathbf{C}\mathbf{c} \dots$$

Where:

P = Percent of combined aggregates passing a given sieve

- A, B, C, ... = Percent of material passing a given sieve for the individual aggregates
- a, b, c,  $\dots$  = Proportion or Bin Split, of individual aggregates used in the combination, where the total = 100%

Example, No. 4:

$$(8 \times 55\%) + (98 \times 35\%) + (96 \times 10\%) = 48\%$$

Note: The combined gradation percentages are rounded to the nearest whole number.

Since all the combined gradation percentages passing are within the wide band specifications, this is an acceptable bin split for these stockpile gradations.

Simply getting the gradations within the wide band specifications does not necessarily mean a successful mix design will be achieved. Stockpile gradations and bin splits should be controlled during the crushing and mix design operations. Judgment and experience are needed to select and crush to an aggregate mixture that will result in a successful mix design.

#### 2. Aggregate Quantities

Combine the aggregate at the bin splits determined in Table A1. Typically enough aggregate and lime will be combined to produce nine Marshall pats and three maximum specific gravity tests samples. The quantity of material needed for each of the maximum specific gravity tests is determined according to AASHTO T 209, Section 7, Table 1 (also below).

| 1.0010 1.0111100000            | mipre 21202         |
|--------------------------------|---------------------|
| Nominal Maximum Aggregate Size | Minimum Sample Size |
| $1\frac{1}{2}$ inch or greater | 4,000 g             |
| $\frac{3}{4}$ inch to 1 inch   | 2,500 g             |
| $\frac{1}{2}$ inch or smaller  | 1,500 g             |

A Marshall mix design normally requires enough material to evaluate three different asphalt contents (three Marshall specimens and one maximum specific gravity at asphalt content). Compacted Marshall pats results should yield specimens of  $2.5 \pm 0.05$  inch in height by 4 inch diameter, usually 1,200 g as per AASHTO T 245.

$$(1200 \text{ g x } 9) + (2500 \text{ g x } 3) = 18,300 \text{ g}$$

If 18,300 g of aggregate are to be used and the bin split is 55% coarse, 35% fine, and 10% filler, the following quantity from each bin would be added:

| Coarse: | 10,065 g |
|---------|----------|
| Fine:   | 6,405 g  |
| Filler: | 1,830 g  |

#### 3. Lime Quantity

Add lime at the selected rate to the dry aggregate and completely combine by stirring, distributing it throughout the aggregate. The lime percentage is expressed as a percentage of the dry weight of the aggregate. The minimum amount of lime is indicated in the Materials & Rates in the plans and is incorporated as per Section 401.1.16.1 WYDOT Standard Specifications.

Calculate the weight of lime to be added by multiplying the dry aggregate weight by the lime percentage addition rate. For example, with 1.0% lime and 19,000 g of dry aggregate, the lime addition of 190 g and is calculated as follows:

$$W_L = \frac{W_L x(W_S)}{100} = \frac{1.0 x (19,000)}{100} = 190 \text{ g}$$

| Where: | $P_{L}$ | = | Percentage of lime, %   |
|--------|---------|---|-------------------------|
|        | $W_{s}$ | = | Dry aggregate weight, g |
|        | $W_L$   | = | Lime weight, g          |

4. Water Quantity

> Add water at a specified water to lime ratio, expressed by weight. Add the water to evenly coat the material.

> Note: While doing a Job Mix Formula (JMF), a ratio of 3:1 (three parts water to This is based on Section 401.4.13.2 WYDOT one part lime) is used. Standard Specifications.

> Calculate the weight of water to add by multiplying the weight of lime by the water:lime ratio. For example, with 190 g of lime and a water:lime ratio of 3:1, the water addition rate of 570 g is calculated as follows:

$$W_W = R_W : {}_L x(W_L) = \frac{3}{1} x (190) = 570 g$$

Where: R<sub>W:L</sub>

 $W_W$ 

Wı

Water weight, g = = Water:lime ratio Lime weight, g =

5. Asphalt Quantity

> Oven dry the aggregate/lime mixture to drive off the water. Place the batched pans in the oven and heat to a temperature not to exceed 50 °F above the mixing temperature shown in Table 2 of this section.

> Add asphalt to the dry aggregate. The asphalt quantity is a percentage of the total mix weight, including the lime weight but not the water weight. Select at least three different trial asphalt contents, but none below 4.50% asphalt.

> Typically three Marshall pats and one Maximum Specific Gravity sample will be prepared at each of three asphalt contents. If one third of an aggregate and lime mixture containing 19,000 g of aggregate and 190 g of lime is mixed with 5.50% asphalt, the asphalt to be added, 372 g, is calculated as follows:

$$W_{b} = \frac{1}{3} (W_{s} + W_{L}) \frac{P_{b}}{100 - P_{b}}$$

$$W_b = \frac{1}{3} (19,000 + 190) \frac{5.5}{100 - 5.5} = 372 \text{ g}$$

Where:

W<sub>b</sub> = Asphalt weight, g = Asphalt content, % Pb Dry aggregate, g Ws =

6. Mixing and Compacting

> Use the asphalt binder type shown in the plans from the intended supplier. If a change to the asphalt binder type has been approved by the engineer, use the approved asphalt binder type.

> Mix and compact the Marshall pats according to AASHTO T 245 and Superpave pucks according to AASHTO R 30, with the following modifications:

> Determine the mixing and compaction temperatures for the laboratory mix design from Table 2:

|          | Laboratory Temperatures |     |  |  |  |  |
|----------|-------------------------|-----|--|--|--|--|
|          | Mixing Compaction       |     |  |  |  |  |
|          | °F                      | °F  |  |  |  |  |
| PG 58-28 | 305                     | 280 |  |  |  |  |
| PG 64-22 | 310                     | 285 |  |  |  |  |
| PG 64-28 | 315                     | 290 |  |  |  |  |
| PG 70-28 | 325                     | 300 |  |  |  |  |
| PG 76-28 | 335                     | 310 |  |  |  |  |

**Table 2. Mixing and Compacting Temperatures** 

Mixing and compaction temperatures should be determined for the asphalt grade to be supplied to the project. For example, if a PG 64-28 asphalt is to be utilized, the mixing temperature will be 315 °F and the compaction temperature will be 290 °F.

The Materials Program will provide the appropriate mixing and compaction temperatures for asphalt grades not included in Table 2.

Replace Subsection 3.4.3 with the following:

**3.4.3** Cure the specimen in accordance with AASHTO R 30 Subsection 7.1.

The design number of gyrations, N<sub>des</sub>, is established by the class of mix shown in the plans and Table 401.4.13-2 *WYDOT Standard Specifications* "Marshall and Superpave Plant Mix Properties".

The number of blows applied to each side of the Marshall pats is established by the class of mix shown in the plans and Table 401.4.13-2 Table 401.4.13-2 *WYDOT Standard Specifications* "Marshall and Superpave Plant Mix Properties".

#### B. Maximum Specific Gravity

- 1. Oven dry the batched aggregate lime mixture to drive off the water. Place the batched pans in the oven and heat to a temperature not to exceed 50 °F above the mixing temperature as shown in Table 2 of this section.
- 2. Add asphalt to the dry aggregate. The asphalt quantity is a percentage of the total mix weight, including the lime weight but not the water weight. Use the selected trial asphalt contents. None should be below 4.50% asphalt.
- 3. Mix and cure the maximum specific gravity samples in the same manner as for the Marshall pats.
- 4. Determine the maximum specific gravity according to AASHTO T 209, using the mix prepared as described above rather than a sample obtained as described in AASHTO T 209, Section 7.1.

#### C. Bulk Specific Gravity

- 1. Determine the bulk specific gravity of the Marshall pats according to AASHTO T 166.
- 2. Calculate the bulk specific unit weight by multiplying the bulk specific gravity by 62.4 to get the unit weight in pounds per cubic foot (pcf).

#### **D.** Volumetric Calculations and Examples

- 1. Perform the necessary calculations described as follows and report the derived values on Forms T-158 and E-46.
  - Variables: The variables here generally follow those used in the Asphalt Institute's publication MS-2, *Mix Design Methods for Asphalt Concrete and Other Hot Mix Types.*
  - $P_{1}, P_{2,...}, P_{n}$  = Weight percentages of the individual aggregate portions, bin splits

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- P<sub>mm</sub> = Total loose mixture percentage as percentage by total weight of mixture which equals 100%
  - $P_{b}$  = Percentage asphalt (asphalt content) as a percentage of the total mixture weight including the lime weight but not the water weight
- $P_{ba}$  = Absorbed asphalt by weight percentage of the dry aggregate
- $P_{be}$  = Effective asphalt content as a weight percentage of the total mixture not including the water weight
- $P_s$  = Aggregate percentage by total weight of the mixture including the weight of the lime but not the water weight
- $G_{sb}$  = Bulk specific gravity of the total aggregate
- $G_1, G_2, G_n$  = Bulk specific gravities of the individual aggregate portions as determined by AASHTO T 84 & AASHTO T 85
  - Maximum specific gravity of the total mix, sometimes referred to as the
  - $G_{mm} =$  Voidless unit weight (VUW), or the Rice specific gravity, as determined by AASHTO T 209
  - $G_{mb}$  = Bulk specific gravity of the compacted mixture as determined by AASHTO T 166
  - $G_{Se}$  = Effective specific gravity of the aggregate
  - $G_{\rm b}$  = Specific gravity of the asphalt, obtained from the refinery invoice or loading certificate

 $V_a$  = Air voids, percentage, in the compacted mixture by volume

VMA = Voids in mineral aggregate ( $V_{ma}$ )

VFA = Voids filled with asphalt ( $V_{fa}$ )

 $V_b$  = The volume percentage of the effective asphalt

 $PP_i$  = Percentage passing the individual sieve

- $SAF_i$  = Surface area factor individual sieve
- SA = Surface area of the aggregate in  $ft^2/lb$
- F.T. = Film thickness in  $\mu$ m
- D/A = Dust to asphalt ratio

**Equations**:

a. 
$$G_{sb} = \frac{P_1 + P_2 + P_n}{\frac{P_1}{G_1} + \frac{P_2}{G_2} + \dots + \frac{P_n}{G_n}} =$$
 bulk specific gravity of the total aggregate

b. 
$$G_{mm} = \frac{P_{mm}}{\frac{P_s}{G_{se}} + \frac{P_b}{G_b}} = \text{maximum specific gravity (no air voids)}$$

c. 
$$V_a = 100 \times \frac{G_{mm} - G_{mb}}{G_{mm}} = air voids$$

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d. 
$$G_{se} = \frac{P_{mm} - P_b}{\frac{P_{mm}}{G_{mm}} - \frac{P_b}{G_b}} = \text{effective gravity of aggregate}$$

e. 
$$P_{ba} = 100 \text{ x} \frac{G_{se} - G_{sb}}{G_{sb} G_{se}} G_b = \text{absorbed asphalt}$$

f. 
$$P_s = 100 - P_b = aggregate percentage$$

g. 
$$P_{be} = P_b - \frac{P_{ba}}{100} \times P_s = \text{effective asphalt}$$

h. VMA = 
$$100 - \frac{G_{mb} \times P_s}{G_{sb}}$$
 = voids in mineral aggregate (V<sub>ma</sub>)

i. 
$$VFA = \frac{100 \text{ x } (VMA - V_a)}{VMA} = \text{ voids filled with asphalt } (V_{fa})$$

j. 
$$V_b = \frac{P_{be} \times G_{mb}}{G_b} = \text{effective asphalt volume}$$

k. SA = 
$$\sum_{i=1}^{8} \frac{(PP_i) x (SAF_i)}{100}$$
 = aggregate surface area

| Where: |           | Surface area in ft <sup>2</sup> /lb               |
|--------|-----------|---|
|        |           | Percentage passing the i <sup>th</sup> sieve      |
|        | $SAF_i =$ | Surface area factor for the i <sup>th</sup> sieve |

2. Surface area is calculated by multiplying the percentage passing each indicated sieve by the surface area factor from the table below then dividing by 100. Sum these products to get the total surface area. Using the values not in parentheses gives the surface area in  $ft^2/lb$ .

| Total Percent Passing Sieve              | Maximum<br>Size | No. 4 | No. 8 | No. 16 | No. 30 | No. 50 | No. 100 | No. 200 |
|--|-----------------|-------|-------|--------|--------|--------|---------|---------|
| Surface Area Factor, ft <sup>2</sup> /lb | 2               | 2     | 4     | 8      | 14     | 30     | 60      | 160     |

Table 3 SURFACE AREA FACTORS, SAF;

Note: Surface area factors shown are applicable only when all the above listed sieves are used in the sieve analysis.

Surface Area Factor for coarse aggregate (plus No. 4 sieves combined) =  $2 \text{ ft}^2/\text{lb}$ 

If the surface area is calculated using the surface area factors, use equation below;

Equation m: F.T. ( $\mu$ m) =  $\frac{P_{be} \times 304,800}{G_b \times (62.4) \times SA \times (100)}$  = film thickness

Equation n: 
$$\frac{D}{A} = \frac{PP \text{ No. 200}}{P_{be}} = \text{dust to asphalt ratio}$$

Example Data Values for Calculations:

#### Table 4 Test Values

| $G_1 =$    | 2.650 | (from AASHTO T 84 & T 85)                      |
|------------|-------|--|
| $G_2 =$    | 2.550 | (from AASHTO T 84 & T 85)                      |
| $G_{mm} =$ | 2.450 | (from AASHTO T 209)                            |
| $G_{mb} =$ | 2.300 | (from AASHTO T 166)                            |
| $G_b =$    | 1.030 | (from refinery invoice or loading certificate) |

Table 5 Gradation Percents Passing (PP) (from AASHTO T 27)

| PP max | PP <sub>No.4</sub> | PP <sub>No.8</sub> | PP <sub>No. 16</sub> | PP <sub>No. 30</sub> | PP <sub>No. 50</sub> | PP No. 100 | PP No. 200 |
|--------|--------------------|--------------------|----------------------|----------------------|----------------------|------------|------------|
| 100    | 51                 | 41                 | 32                   | 24                   | 17                   | 10         | 4.8        |

| Selected Values: | $P_1 =$    | 60%  | = | (percentage from Bin 1) |
|------------------|------------|------|---|-------------------------|
|                  | $P_2 =$    | 40%  | = | (percentage from Bin 2) |
|                  | $P_b =$    | 6%   | = | (asphalt content)       |
|                  |            |      |   |                         |
| Known Value:     | $P_{mm} =$ | 100% |   |                         |

Example Calculated Values: Substituting the data values for the variables in the equations from above are example calculations:

From Equation a.: 
$$G_{sb} = \frac{60 + 40}{\frac{60}{2.650} + \frac{40}{2.550}} = 2.609 = \text{bulk specific gravity}$$

From Equation b.: 
$$G_{mm} = \frac{100}{\frac{94}{2.686} + \frac{6}{1.030}} = 2.450 = maximum specific gravity$$

From Equation c.:
 
$$V_a = 100 \times \frac{2.450 - 2.300}{2.450} = 6.1\% = air voids$$

 From Equation d.:
  $G_{se} = \frac{100 - 6}{\frac{100}{2.450} - \frac{6}{1.030}} = 2.686 = effective gravity of aggregate

 From Equation e.:
  $P_{ba} = 100 \times \frac{2.686 - 2.609}{(2.609) \times (2.686)} \times 1.030 = 1.132 = absorbed asphalt

 From Equation f.:
  $P_{s} = 100 - 6.00 = 94.00\% = aggregate$  percentage

 From Equation g.:
  $P_{be} = 6.00 - \frac{1.132}{100} \times 94.00 = 4.94\% = effective asphalt

 From Equation h.:
  $VMA = 100 - \frac{(2.300) \times (94.00)}{2.609} = 17.1\% = voids in mineral aggregate (V_{ma})

 From Equation i.:
  $VFA = \frac{100 (17.13 - 6.12)}{17.13} = 64\% = voids filled with asphalt (V_{fa})$$$$$ 

From Equation j.: 
$$V_b = \frac{(4.94)x(2.300)}{1.030} = 11.03\% = \text{effective asphalt volume}$$

From Equation k: = aggregate surface area

$$SA = \frac{(100 \times 2) + (51 \times 2) + (41 \times 4) + (32 \times 8) + (24 \times 14) + (17 \times 30) + (10 \times 60) + (4.8 \times 160)}{100} = 29.36 \frac{ft^2}{lb}$$

Note: SAF: Surface Area Factor from Table 3. PP: Percent passing from Table 5.

From Equation m: F.T. ( $\mu$ m) =  $\frac{4.94 \times 304,800}{1.030 \times 62.4 \times 29.36 \times 100} = 8 \ \mu$ m = film thickness

Note: Film thickness is not required for mixes containing RAP.

Equation n: 
$$\frac{D}{A} = \frac{PP \text{ No.200}}{P_{be}} = \frac{4.8}{4.94} = 1.0 = \text{dust to asphalt ratio}$$

#### Marshall Mix Design Procedure (continued)

10. Select the target asphalt content at which all volumetric properties meet the specified properties.

At the target asphalt content selected, determine the TSR (tensile strength ratio) in accordance with AASHTO T 283 with the following modification:

6.6 After extraction from the molds, store the test specimens for 23 to 25 hours at room temperature, 60 °F to 86 °F.

Include the optional freeze-thaw conditioning as described in AASHTO T 283 in this method.

- 11. Develop an equation to represent the Asphalt Content vs. Voidless Unit Weight (VUW) line using the following procedure. The VUW for construction control purposes will be determined using this equation. Adjustment to the VUW during construction will also utilize this equation as described in WYDOT 419.0.
  - a. Calculate the effective specific gravity,  $G_{se}$ , for each asphalt content tested. The equation is included as equation "d", above.
  - b. Determine the average effective specific gravity and the difference of each effective specific gravity from the average. If the difference is greater than 0.025, that test and the corresponding asphalt content is considered to be an outlier and will not be used to define the equation. If there are two values greater than 0.025, this indicates that there is testing error and the tests related to the virtual specific gravity calculation must be verified and this procedure re-run with the new values;
  - c. Determine the equation for all remaining asphalt content points and corresponding voidless unit weights using the following best fit line equation:

$$VUW_p = (m x TAC) + b$$

Where:

VUW = Predicted VUW at the recommended asphalt content TAC = Recommended asphalt content b = VUW<sub>avg</sub> - (m x TAC<sub>avg</sub>)

(TAC<sub>1</sub> x VUW<sub>1</sub> + TAC<sub>2</sub> x VUW<sub>2</sub> +....+ TAC<sub>n</sub> x VUW<sub>n</sub>) - (n x TAC<sub>avg</sub> x VUW<sub>avg</sub>)

$$m = \frac{1}{(TAC_1^2 + TAC_2^2 + ... + TAC_n^2) - (n \times TAC_{avg}^2)}$$

n = Number of test results evaluated
 TAC<sub>avg</sub> = Average of all asphalt contents, minus any outlier
 VUW<sub>av</sub> = Average of all voidless unit weight values minus any outlier

- d. Record the predicted  $VUW_P$  and TAC on Forms T-158 and E-46.
- 12. Determine the target Voidless Unit Weight for the recommended design asphalt content using the VUW<sub>p</sub> equation.
- 13. Determine whether the actual Voidless Unit Weight is an outlier following the following procedure:
  - a. Calculate the difference between the target VUW and the actual VUW at the target asphalt content. The actual VUW may be interpolated if the target asphalt content was not one of the three trial asphalt contents. Interpolation will use the two closest results.
  - b. If the difference between the target VUW and the actual VUW is within 0.5 pcf, continue to number 14.
  - c. If the difference between the target VUW and the actual VUW exceeds 0.5 pcf, the mix design volumetric values must be re-calculated using the target VUW.
    - 1. If the re-calculated mix design volumetric values do not meet the specifications, adjust the target asphalt content following from number 9 thru 12 until a mix design meeting all applicable specifications is obtained; or,
    - 2. If an acceptable mix design cannot be met by adjusting the target asphalt content, adjustment to the aggregate gradation may be required and a new mix design done.
- 14. Record the target asphalt content and the target VUW on Forms T-158 and E-46. Submit the complete mix design to the WYDOT engineer, including all trial asphalt contents and corresponding results. Refer to the completed Form T-158; ensure that the E-46 has been signed by the contractor, mix design representative, and Resident Engineer before submittal to the Materials Program.

# **Construction Mix Volumetric Verification:**

1. Sample the hot plant mix material according to WYDOT 410.0, to obtain three full cylinder cans of material for Marshall mix verifications and five full cylinder cans of material for Superpave mix verifications. Transport the samples according to WYDOT 411.0.

- 2. Determine the maximum specific gravity according to AASHTO T 209, using the mix obtained as described above rather than a lab-mixed sample as described in AASHTO T 209, Section 7.1.
- 3. Determine the total and effective asphalt contents and gradation. Determine and apply a correction factor in accordance with AASHTO T 308 if the Ignition Method is utilized.

Note: For recycle hot plant mix, chemical extractions may provide more reliable asphalt content and gradation results.

- 4. Heat samples to the temperature at which the mix design specimens were compacted. (Table 2 of this section.)
- 5. Mix and compact the Superpave pucks with the  $N_{des}$  gyrations used during design and calculate density at  $N_{des}$  and the Marshall pats according to AASHTO T 245 with the following modifications:

Replace Subsection 3.3.1 with the following:

**"3.3.1** The samples will be obtained according to WYDOT 410.0 and transported according to WYDOT 411.0."

After splitting, place specimens of the proper size to prepare a compacted specimen 2.5 inch  $\pm$  0.05 inch in height, about 2.6 lb, in appropriate pans for reheating. Reheat using the compaction temperature used during the mix design procedure.

Replace Subsection 3.4.3 with the following:

"**3.4.3** No further curing is needed."

The number of blows applied to each side of the Marshall pats is established by the class of mix shown in the plans and Section 401.4.13-2 *WYDOT Standard Specifications* "Marshall and Superpave Plant Mix Properties".

- 6. Determine the bulk specific gravity of the Marshall pats or the Superpave pucks according to AASHTO T 166. Calculate the VUW by multiplying the bulk specific gravity by 62.4 for pounds per cubic foot (pcf). Field adjustments to the VUW will be in accordance with WYDOT 419.0.
- 7. Determine which calculations are needed for the current application, perform the necessary calculations, and report the results in accordance with Section Subsection 3 of 401.4.7.3 *WYDOT Standard Specifications*, on Form T-158F.

At a minimum, report with the project information (project number, contractor, consultant, aggregate type, mix properties, level of control, aggregate source, asphalt type and source, extraction method, etc.) along with the following information:

#### WYDOT 414.0 (Rev. 10-18)

Sample number, date sampled, station sampled, total extracted asphalt content, effective asphalt content, compacted density, Voidless Unit Weight, Air Voids, VMA, Stability where applicable, Extracted Gradation, Dust to Effective Asphalt, Film Thickness when specified, and comments. Comments are intended to address action taken to address out-of-specification material, sampling issues, paired samples, etc.

8. Provide the engineer **and** the Materials Program with the volumetric results using Form T-158F. The Materials Program will incorporate the volumetric results into the permanent project file. Form T-158F may be emailed to both the engineer and the Materials Program. Submit the proposed JMF on Form E-46.



#### WYOMING DEPARTMENT OF TRANSPORTATION BITUMINOUS PAVEMENT MIX DESIGN

T-158 (09-16)

| Proi          | iect No.:               | ERP Pojec                 |                     | FUMINOUS F<br>Lab N        | O.: Lab #              |                    |                    | gregate: Pi       | t Names                   |                 |
|---------------|-------------------------|---------------------------|---------------------|----------------------------|------------------------|--------------------|--------------------|-------------------|---------------------------|-----------------|
| Asphalt       |                         | Source                    |                     | For Use /<br>lass & Gradii | As: As pe<br>ng: Class | r plans<br>& Grade | S                  | ource(s): Re      | efinery Na<br>esident Eng | me<br>jineer    |
| Sample        | D                       |                           | Veights, gra        |                            | Volume,                | C                  | Density,           | Height,           | Stability,                | Flow, 0.0       |
| No.           | P <sub>b</sub>          | Air<br>1186.1             | SSD<br>1190.4       | Wet<br>683.1               | cc<br>507.3            | G <sub>mb</sub>    | lb/ft <sup>3</sup> | inches<br>2.5     | lbf<br>3451               | in<br>12        |
| 1             | 4.5                     | 1197.8                    | 1190.4              | 688.8                      | 512.5                  | 2.338              | 145.89<br>145.83   | 2.5               | 3451                      | 12              |
| 3             | P <sub>be</sub><br>2.98 | 1197.8                    | 1196.1              | 684.3                      | 511.8                  | 2.337              | 145.20             | 2.5               | 6560                      | 11              |
| D/A 1.54      | and they are a          |                           | 9.74 V <sub>A</sub> |                            | VTOTAL                 | 2.334              | 145.64             | VMA               | VFA                       | Va              |
| µm 5.98       |                         |                           | 560 6.7             |                            | 91.18                  | 2.001              | 110.01             | 15.60             | 43.41                     | 8.83            |
| Sample        |                         |                           | Veights, gra        |                            |                        | 1                  | Density,           | Height,           | Stability,                | Flow, 0.0       |
| No.           | Pb                      | Air                       | SSD                 | Wet                        | Volume,<br>cc          | G <sub>mb</sub>    | lb/ft <sup>3</sup> | inches            | lbf                       | in              |
| 4             | 5.0                     | 1198.4                    | 1200.6              | 692.8                      | 507.8                  | 2.360              | 147.26             | 2.5               | 3597                      | 13              |
| 5             | Pbe                     | 1199.6                    | 1200.5              | 690.3                      | 510.2                  | 2.351              | 146.70             | 2.5               | 3614                      | 13              |
| 6             | 3.57                    | 1194.6                    | 1196.4              | 689.5                      | 506.9                  | 2.357              | 147.08             | 2.5               | 3620                      | 12              |
| D/A 1.29      |                         | /, lb/ft <sup>a</sup> 158 | 8.18 V <sub>A</sub> |                            | VTOTAL                 | 2.356              | 147.01             | VMA               | VFA                       | Va              |
| µm 7.17       | 7                       | G <sub>mm</sub> 2.5       | 535 8.2             | 0 84.75                    | 92.95                  |                    |                    | 15.25             | 53.70                     | 7.06            |
| Sample        |                         |                           | Veights, gra        | ms                         | Volume,                | -                  | Density,           | Height,           | Stability,                | Flow, 0.0       |
| No.           | Pb                      | Air                       | SSD                 | Wet                        | CC                     | G <sub>mb</sub>    | lb/ft <sup>3</sup> | inches            | lbf                       | in              |
| 7             | 6.0                     | 1185.8                    | 1186.6              | 690.4                      | 496.2                  | 2.390              | 149.14             | 2.5               | 3505                      | 15              |
| 8             | Pbe                     | 1196.7                    | 1197.2              | 697.3                      | 499.9                  | 2.394              | 149.39             | 2.5               | 3424                      | 16              |
| 9             | 4.74                    | 1195.9                    | 1196.5              | 699.0                      | 497.5                  | 2.404              | 150.01             | 2.5               | 3411                      | 15              |
| D/A 0.9       |                         |                           | 5.19 V <sub>A</sub> | C VAGGR                    | VTOTAL                 | 2.396              | 149.51             | VMA               | VFA                       | Va              |
| µm 9.5        | 1                       |                           | 487 11.0            |                            | 96.35                  |                    |                    | 14.72             | 75.14                     | 3.66            |
| Sample<br>No. | P <sub>b</sub>          | V<br>Air                  | Veights, gra<br>SSD | ms<br>Wet                  | Volume,<br>cc          | G <sub>mb</sub>    | Density,<br>lb/ft³ | Height,<br>inches | Stability,<br>lbf         | Flow, 0.0<br>in |
|               | Pbe                     |                           |                     |                            | 1                      |                    |                    |                   |                           |                 |
| D/A           | VUW                     | /, lb/ft <sup>s</sup>     | VA                  |                            | V <sub>TOTAL</sub>     |                    |                    | VMA               | VFA                       | Va              |
| μm            |                         | G <sub>mm</sub>           | 10023               |                            |                        |                    |                    | 1200              |                           |                 |
| Sample<br>No. | P <sub>b</sub>          | V<br>Air                  | Veights, gra<br>SSD | ms<br>Wet                  | Volume,<br>cc          | G <sub>mb</sub>    | Density,<br>lb/ft³ | Height,<br>inches | Stability,<br>Ibf         | Flow, 0.0<br>in |
|               | Pbe                     |                           |                     |                            |                        |                    |                    |                   |                           |                 |
| D/A           | VUV                     | /, Ib/ft <sup>a</sup>     | VA                  | c V <sub>AGGR</sub>        | V <sub>TOTAL</sub>     |                    |                    | VMA               | VFA                       | Va              |
|               |                         | G <sub>mm</sub>           |                     |                            |                        |                    |                    |                   |                           |                 |

 $P_b$  = asphalt content by weight;  $P_{be}$  = effective asphalt content;  $G_{mb}$  = bulk specific gravity of paving mixture;  $G_{mm}$  = maximum specific gravity of paving mixture; VUW = maximum density of paving mixture;  $V_{AC}$  = volume of asphalt, %;  $V_{AGGR}$  = volume of aggregate, %;  $V_{TOTAL}$  = total volume, %; VMA = voids in mineral aggregate, %; VFA = voids filled with asphalt, %; Va = air voids;  $G_{sb}$  = bulk specific gravity of aggregate;  $G_{sa}$  = apparent specific gravity of aggregate;  $G_b$  = specific gravity of asphalt

#### WYOMING DEPARTMENT OF TRANSPORTATION MIX VERIFICATION OF PLANT PRODUCED BITUMINOUS PLANT MIX PAVEMENT 2003/2010 Specification

T-158F (10-18)

| roject No. | : 1803146              |                      |        |       | 2      |       | Cons      | sultant: |          |            |                         |            | _         | Cor       | tractor:           | Simon                |              |                   |        |
|------------|------------------------|----------------------|--------|-------|--------|-------|-----------|----------|----------|------------|-------------------------|------------|-----------|-----------|--------------------|----------------------|--------------|-------------------|--------|
| Location   | : Creston Jct          | - Rawli              | ns (CL | West) | 2      | Ag    | gregat    | e Type:  | II       |            |                         |            | <u></u>   | Aspha     | lt Type:           |                      |              |                   |        |
| Engineer   | : Spenny               |                      |        |       | _      | Aggı  | regate \$ | Source:  | N. Raw   | lins Qr    | 'Y                      |            | _         | Asphalt   | Source:            |                      |              |                   |        |
| Material   | : RHPM                 |                      |        |       | _      | A     | ggrega    | te Size: | 1/2"     |            |                         |            |           | PG Binde  | r Grade:           | 76-28                | ŝ.           |                   |        |
| Class      | : II-S                 |                      |        |       | -      | Lev   | vel of C  | ontrol:  | 2        |            |                         |            | _ P       | G Binder  | Source:            | Peak                 |              |                   |        |
| Quantity   | : 52,420               |                      |        |       | _      | # Te  | ests Re   | quired:  | 35       |            |                         |            |           |           |                    |                      |              |                   |        |
|            |                        | 1¼ IN                | 1 IN   | 34 IN | 1⁄2 IN | % IN  | No. 4     | No. 8    | No. 30   | No.<br>200 | TAC<br>% <sup>(1)</sup> | VUW<br>pcf | VMA<br>%  | VFA %     | Mix<br>Moist.<br>% | Film<br>Thick.<br>µm | D/A<br>Ratio | Air<br>Voids<br>% | DENSIT |
|            | Design                 |                      |        | 100   | 95     | 79    | 44        | 25       | 10       | 3.9        | 5.70                    | 155.0      | 14.2      | 70        |                    | 8                    | 1.1          | 4.3               | 148.8  |
| Single Tes | st Control, +/-        | jmf                  | jmf    | jmf   | jmf    | jmf   | jmf       | jmf      | jmf      | jmf        | ± 0.25                  |            | Section   | 401.4.13. | 3.1 Table          | es 401.4             | .13-2 and    | 1401.4.1          |        |
| Desig      | n Tolerances           |                      |        | 100   | 90-100 | 74-84 | 36-46     | 20-28    | 7-13     | 2.0-7.0    | 5.45 - 5.95             |            | 13.0-17.0 | 65-78     | 0.5 max.           | 6-12                 | 0.8-1.4      | 3.0-5.0           |        |
|            | <b>8</b>               |                      | 12     |       |        |       | 2         | 018 P    | aving Se | eason      |                         |            |           |           |                    | *                    |              |                   |        |
| TEST #     | Date                   |                      |        |       |        | ļ     |           |          | ļ        |            | 1                       |            |           |           | <u> </u>           |                      |              |                   |        |
| 40 ML      | 7/24/18                |                      |        | 100   | 97     | 83    | 48        | 29       | 14       | 6.9        | 5.50                    | 155.4      | 13.7      | 75        | ļ                  | 8                    | 1.6          | 3.5               | 150.0  |
| 41 ML      | 7/25/18                |                      |        | 100   | 95     | 82    | 47        | 29       | 13       | 6.6        | 5.47                    | 155.0      | 13.6      | 78        | ļ                  | 8                    | 1.5          | 3.1               | 150.2  |
| 42 ML      | 7/26/18                |                      |        | 100   | 95     | 81    | 46        | 28       | 14       | 6.7        | 5.53                    | 155.9      | 13.6      | 75        |                    | 8                    | 1.6          | 3.5               | 150.4  |
| 43 ML      | 7/26/18                |                      |        | 100   | 95     | 81    | 47        | 29       | 14       | 6.9        | 5.52                    | 155.3      | 13.6      | 77        |                    | 8                    | 1.5          | 3.3               | 150.2  |
| 44 ML      | 7/31/18                |                      |        | 100   | 95     | 82    | 46        | 28       | 13       | 6.6        | 5.27                    | 156.0      | 13.5      | 73        |                    | 8                    | 1.6          | 3.8               | 150.1  |
| 45 ML      | 8/1/18                 |                      |        | 100   | 95     | 80    | 44        | 29       | 13       | 6.2        | 5.54                    | 155.8      | 13.7      | 75        |                    | 8                    | 1.4          | 3.5               | 150.3  |
| 46 ML      | 8/1/18                 |                      |        | 100   | 95     | 82    | 45        | 28       | 13       | 6.2        | 5.47                    | 154.9      | 13.9      | 77        | 1                  | 9                    | 1.4          | 3.3               | 149.8  |
| 47 ML      | 8/7/18                 |                      |        | 100   | 96     | 83    | 48        | 29       | 13       | 6.1        | 5.37                    | 154.5      | 14.1      | 76        | 1                  | 9                    | 1.3          | 3.5               | 149.2  |
| 48 ML      | 8/7/18                 |                      |        | 100   | 96     | 83    | 47        | 29       | 13       | 6.7        | 5.48                    | 155.1      | 13.7      | 77        |                    | 8                    | 1.5          | 3.2               | 150.1  |
| 49 ML      | 8/8/18                 |                      |        | 100   | 96     | 81    | 47        | 29       | 14       | 6.4        | 5.39                    | 154.8      | 14.1      | 75        |                    | 8                    | 1.4          | 3.6               | 149.3  |
| 50 ML      | 8/8/18                 |                      |        | 100   | 96     | 82    | 47        | 29       | 13       | 6.0        | 5.39                    | 155.6      | 13.9      | 72        | -                  | 8                    | 1.4          | 3.9               | 149.5  |
|            |                        |                      |        |       |        |       |           |          |          |            |                         |            |           |           | 1                  |                      |              |                   |        |
|            | Average <sup>(1)</sup> |                      |        | 100   | 96     | 82    | 47        | 29       | 13       | 6.5        | 5.45                    | 155.3      | 13.8      | 75        |                    | 8                    | 1.5          | 3.5               | 149.9  |
|            | Std. Dev (1)           | <sup>(1)</sup> inclu |        | 0.0   | 0.7    | 1.0   | 1.2       | 0.5      | 0.5      | 0.32       | 0.083                   | 0.49       | 0.21      | 1.8       |                    | 0.4                  | 0.10         | 0.24              |        |

Consultant Comments:

Submitted By: DENNISS

DOT Recommendation:

WYDOT Entered By: <u>GRAEBER</u> WYDOT Review By: 18-080 Mix Design Laboratory #:

# 8

#### WYOMING DEPARTMENT OF TRANSPORTATION HOT PLANT MIX JOB MIX FORMULA

E-46 (Rev. D9-16)

| Project Number:   |   |   |           |  |  | and the second s | XX/XX/XX   |                |   |  | -  |
|---|---|---|-----------|--|--|--|--|----------------|---|--|--|
|   | ERP Projec  |   |           |  |  | are the state of the second second   | Company No   | and the second |   | _  | -0   |
| Resident Engineer:  |   |   |           |  |  |  | Company No   | me             |   |  | - 1  |
| Engineer's Town:  | Town Name   | 8   |           |  | Class, Aggr<br>Level of Control,   | and the second se  |  |                |   |  | - C  |
|   | % PASSING   | % PASSING                                 | % PASSING | % PASSING  | COMB. VIRGIN   | JMF  | JMF LIM  | TTS            | RAP   | COMB.  | WIDE BAND  |
| SIEVE SIZE  | BIN #1  | BIN#2                                     | BIN#3     | BIN#4  | %  | 96   | % PASSI  |                | GRAD.   | GRAD.  | % PASSING  |
| 11/2 inch   |   | (   |           |  |  |  |  |                |   | 1.1  |  |
| 1 inch  | 100   |   |           |  | 100  | 100  | 100  |                |   |  | 100  |
| 3/4 inch  | 97  |   |           |  | 99   | 99   | 90-10  | 00             |   |  | 90-100   |
| 1/2 inch  | 46  | 100                                       |           |  | 85   | 85   | 80-9   | 0              |   |  | 55-90  |
| 3/8 inch  | 12  | 86  | 100       | ) · · · · · · · · · · · · · ·  | 73   | 73   | 68-7   | 8              |   | ()   | 65-85  |
| No. 4   | 2   | 3   | 83        | 1  | 49   | 49   | 44-5   | 4              | 1   |  | 30-65  |
| No. 8   | 1   | 2   | 53        |  | 31   | 31   | 27-3   | 5              |   |  | 20-50  |
| No. 16  | 1   | 2   | 35        |  | 21   | 21   |  |                | 7   |  |  |
| No. 30  | 1   | 2   | 24        |  | 14   | 15   | 121  | 8              | 1   |  | 530  |
| No. 50  | 1   | 1   | 17        |  | 10   | 10   |  |                | 0   | -  |  |
| No. 100   | 1   | 1   | 13        |  | 6  | 8  |  |                | 1   |  |  |
| No. 200   | 0.4   | 0.5                                       | 8.8       |  | 5,3  | 5.3  | 3,0-7  | 0              | 1   |  | 2-7.   |
| firgin material was con<br>BIN #  | nbined at the fo<br>SIZ   |   | ents (%): | SOURCE   |  | Gs   | Abs.   | 2              | DEPC  | ENT (%)  |  |
| 1   | Size & Ad   |   | 1         | Pit Name   |  | 2.591  | 1.6%   | 1              |   | 28   | 1  |
| 2   | Size & Ad   |   | -         | Pit Name   | e  | 2.570  | 2.0%   | 1              |   | 14   |  |
| 3   | Size & Ad   | gregate                                   | 1         | Pit Name   | e  | 2.552  | 2.3%   |                |   | 58   |  |
|   |   |   |           |  |  | -  |  |                |   |  |  |
| Average extracted a<br>(IF AVAILIBLE)   | ısphalt content   | hined using:<br>of the RAP<br>Penetration |           | %<br>A   | ined virgin gradat<br>verage Viscosity<br>GN PROPERT   |  |  | % RAP          |   |  |  |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacture  | Average<br>Average<br>310 °F<br>315 °F<br>Company Nam   | of the RAP<br>Penetration                 |           | %<br>MIX DESI<br>Lab Compa<br>T-160  | verage Viscosity   | <b>TES</b><br>290<br>145,1<br>151,3  | pcf or kg/m²<br>pcf or kg/m²<br>lbf  |                | rshall Blows o  | r #Gyration<br>Air Void<br>VM2<br>VF2  | s 4,0<br>15.0  |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacture<br>phalt Grade (AC or PG)<br>Design Asphalt Contem   | Average<br>310 T<br>315 T<br>Company Nam<br>t 6,10 %  | of the RAP<br>Penetration                 |           | %<br>MIX DESI<br>Lab Compa<br>T-16<br>T-209                                | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability  | T <b>IES</b><br>290<br>145,1<br>151,3  | pcf or kg/m³   |                | rshall Blows o  | Air Void<br>VM#<br>VF#<br>m T hickness   | s 4.0<br>A 15.0<br>A 73<br>10                              |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacture<br>phalt Grade (AC or PC)<br>Design Asphalt Contem<br>fective Asphalt Contem   | 310 T<br>310 T<br>315 T<br>Company Nam<br>- 6.10 %<br>- 4.85 %  | of the RAP<br>Penetration                 |           | %<br>MIX DESI<br>Lab Compa<br>T-16<br>T-209                                | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)  | TES<br>290<br>145.1<br>151.3<br>1.1  | pcf or kg/m³   | #Ma            | rshall Blows o<br>Fill                                      | Air Void<br>VMA<br>VFA<br>m Thickness<br>TSF   | s 4.0<br>15.0<br>73<br>10<br>8<br>81                       |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufactures<br>phalt Grade (AC or PG)<br>Design Asphalt Contem<br>fective Asphalt Contem  | sphalt content<br>Average<br>310 T<br>315 T<br>Company Nam<br>6.10 %<br>4.85 %<br>1.025   | of the RAP<br>Penetration                 |           | %<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe                   | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.G.  | <b>ES</b><br>290<br>145.1<br>151.3<br>1.1<br>2.545   | pcforkg/m²<br>lbf  | #Ma            | rstell Blows o<br>Fib<br>Combined Virg                      | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>jin Agg. S.G                               | x 4.0<br>15.0<br>73<br>10<br>x 81<br>2,569                 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacturen<br>phalt Grade (AC or PC)<br>Design Asphalt Contem<br>ffective Asphalt Contem   | 310 T<br>310 T<br>315 T<br>Company Nam<br>4. 4.85 %<br>1.025<br>2.603   | of the RAP                                |           | % A<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe                 | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)  | TES<br>290<br>145.1<br>151.3<br>1.1<br>2.545   | pcf or kg/m³   | #Ma            | rshall Blows o<br>Fili<br>Combined Virg<br>San              | Air Void<br>VMA<br>VFA<br>m Thickness<br>TSF   | x 4.0<br>15.0<br>73<br>10<br>x 81<br>2.569<br>t 71         |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacture<br>ohalt Grade (AC or PG)<br>Design Asphalt Content<br>fective Asphalt Content<br>Sphalt Specific Gravity<br>Coarse Age. S.G<br>Additive (Line/other<br>Fine Age. Angularity   | sphalt content           Average1           310         F           315         F           Company Nam           6.10         %           1.025         %           1.025         %           1.025         %           4.85         %           1.025         %           4.83         %  | of the RAP<br>Penetration                 | %Add      | %<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe                   | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.G.<br>LA Abrasion Loss  | <b>TES</b><br>290<br>145,1<br>151,3<br>1.1<br>2.545<br>21<br>96<br>96  | pcforkg/m²<br>lbf<br>%   | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>jin Agg. S.G<br>d Equivalen                | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacture<br>halt Grade (AC or PG)<br>Design Asphalt Content<br>fective Asphalt Content<br>Sphalt Specific Gravity<br>Coarse Age. S.G<br>Additive (Line/other<br>Fine Age. Angularity  | 310 T<br>315 T<br>Company Nam<br>6.10 %<br>1.025<br>2.603<br>1.0 %  | of the RAP<br>Penetration                 | %Add      | %<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe                   | Average Viscosity<br>GN PROPERI<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.G.<br>LA Abrasion Loss<br>Fractured Faces (1)<br>Fractured Faces (2)  | <b>TES</b><br>290<br>145,1<br>151,3<br>1.1<br>2.545<br>21<br>96<br>96  | pof or kg/m <sup>4</sup><br>lhf<br>%   | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Asphalt Manufactures<br>blat Grade (AC or PG)<br>Design Asphalt Content<br>fective Asphalt Content<br>Sephalt Specific Gravity<br>Coarse Ags. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I   | sphalt content<br>Average<br>310 T<br>315 T<br>Company Nam<br>4 6.10 %<br>4.85 %<br>7.1.025<br>2.603<br>9.1.0 %<br>48 %<br>2.2.603<br>9.1.0 %<br>2.48 %   | of the RAP<br>Penetration                 | %Add      | % A<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe<br>I<br>Ignitic | Average Viscosity<br>GN PROPERI<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.G.<br>LA Abrasion Loss<br>Fractured Faces (1)<br>Fractured Faces (2)  | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcforkg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br><b>Location</b> :  | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufactures<br>blatt Grade (AC or PG)<br>Design Asphalt Conten<br>fective Asphalt Conten<br>Sphalt Specific Gravity<br>Coarse Ags. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I  | sphalt content<br>Average<br>310 T<br>Company Nam<br>6,10 %<br>1,025<br>2,603<br>0,10 %<br>48 %<br>2,2603<br>0,10 %<br>48 %<br>2,2603<br>0,0 %<br>48 %<br>2,48 %  | of the RAP<br>Penetration                 | %Add      | % A<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe<br>I<br>Ignitic | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Fine Agg. S.G.<br>LA Abrasion Loss<br>Firat tured Faces (2)<br>on Oven Correction | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcforkg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br><b>Location</b> :  | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufactures<br>halt Grade (AC or PG)<br>Design Asphalt Contem<br>fective Asphalt Contem<br>sphalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I<br>nsultant AMRL AA   | sphalt content<br>Average<br>310 T<br>Company Nam<br>6,10 %<br>1,025<br>2,603<br>0,10 %<br>48 %<br>2,2603<br>0,10 %<br>48 %<br>2,2603<br>0,0 %<br>48 %<br>2,48 %  | of the RAP<br>Penetration                 | %Add      | % A<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe<br>I<br>Ignitic | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Fine Agg. S.G.<br>LA Abrasion Loss<br>Firat tured Faces (2)<br>on Oven Correction | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcforkg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br><b>Location</b> :  | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufactures<br>halt Grade (AC or PG)<br>Design Asphalt Contem<br>fective Asphalt Contem<br>sphalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I<br>nsultant AMRL AA   | sphalt content<br>Average<br>310 T<br>Company Nam<br>6,10 %<br>1,025<br>2,603<br>0,10 %<br>48 %<br>2,2603<br>0,10 %<br>48 %<br>2,2603<br>0,0 %<br>48 %<br>2,48 %  | of the RAP<br>Penetration                 | %Add      | % A<br>MIX DE SI<br>Lab Compa<br>T-16<br>T-20<br>Dust/Effe<br>I<br>Ignitic | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Fine Agg. S.G.<br>LA Abrasion Loss<br>Firat tured Faces (2)<br>on Oven Correction | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcforkg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br><b>Location</b> :  | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacturen<br>halt Grade (AC or PG)<br>Design Asphalt Content<br>Ective Asphalt Content<br>Sphalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I<br>nsultant AMRL AA<br>COMMENTS:   | 310         T           315         T           Company Nam         10           4.85         %           2.603         %           1.025         2.603           2.848         %           2.848         %           2.848         %           2.8470         Accret   | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PROPERT<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Fine Agg. S.G.<br>LA Abrasion Loss<br>Firat tured Faces (2)<br>on Oven Correction | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcf or kg/m <sup>2</sup><br>lhf<br>%<br>%<br><b>Location</b> :   | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>halt Grade (AC or PG)<br>Design Asphalt Content<br>ective Asphalt Content<br>coarse Age. S.G<br>Additive (Lime/other<br>Fine Age. Angularity<br>Proposed I<br>nsultant AMRL AA<br>COMMENTS:  | sphalt content<br>Average1<br>310 T<br>315 T<br>Company Nam<br>   | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PR OPER I<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.C.<br>LA Abrasion Loss<br>Fractured Faces (2)<br>on Oven Correction<br>dix Asphalt Accre      | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcf or kg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br>Location:<br>Paving Sub:   | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IP AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asp halt Manufacturen<br>halt Grade (AC or PG)<br>Design Asp halt Content<br>Sphalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Line/other<br>Fine Agg, Angularity<br>Proposed I<br>nsultant AMIRL AA<br>COMMENTS:  | sphalt content<br>Average 1<br>315 7<br>Company Nam<br>6.10 %<br>1.025<br>2.603<br>1.0 %<br>7 48 %<br>Paving Date: 2<br>SHTO Accred   | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PR OPER I<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.C.<br>LA Abrasion Loss<br>Fractured Faces (2)<br>on Oven Correction<br>dix Asphalt Accre      | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pef or kg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br>Location:<br>Paving Sub:<br>Email:   | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IP AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asp halt Manufacturen<br>halt Grade (AC or PG)<br>Design Asp halt Content<br>fective Asp halt Content<br>sophalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Lime/other<br>Fine Agg. Angularity<br>Proposed I<br>nsultant AMRL AA<br>COMMENTS:  | sphalt content<br>Average 1<br>315 %<br>Company Nam<br>6,10 %<br>1,025 %<br>7,1,025 %<br>2,603<br>1,0 %<br>48 %<br>Paving Date: 2<br>SHTO Accred  | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PR OPER I<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.C.<br>LA Abrasion Loss<br>Fractured Faces (2)<br>on Oven Correction<br>dix Asphalt Accre      | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcf or kg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br>Location:<br>Paving Sub:   | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Asp halt Manufacture<br>halt Grade (AC or PG)<br>Design Asp halt Content<br>sphalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I<br>nsultant AMRL AA<br>COMMENTS:   | sphalt content<br>Average 1<br>315 %<br>Company Nam<br>6,10 %<br>1,025 %<br>7,1,025 %<br>2,603<br>1,0 %<br>48 %<br>Paving Date: 2<br>SHTO Accred  | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PR OPER I<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.C.<br>LA Abrasion Loss<br>Fractured Faces (2)<br>on Oven Correction<br>dix Asphalt Accre      | <b>TES</b> 290 145,1 151,3 1.1 2.545 21 96 96  | pcf or kg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br>Location:<br>Paving Sub:<br>Email:<br>Phone #:                                     | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacturen<br>halt Grade (AC or PG)<br>Jesgn Asphalt Content<br>ective Asphalt Content<br>sphalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I<br>nsultant AMRL AA<br>COMMENTS:<br>Consultant:<br>Email:<br>Phone #<br>Date              | sphalt content<br>Average1<br>310 T<br>Company Nam<br>6.00 %<br>1.025<br>2.603<br>0.0 %<br>48 %<br>Paving Date: 2<br>   | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PR OPER I<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.C.<br>LA Abrasion Loss<br>Fractured Faces (2)<br>on Oven Correction<br>dix Asphalt Accre      | TES<br>290<br>145,1<br>151,3<br>1,1<br>2,545<br>21<br>96<br>96<br>96<br>96   | pef or kg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br>Location:<br>Email:<br>Phone #:<br>Date:<br>lent Engineer:                         | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Lab Mix Temperature<br>Asphalt Manufacture<br>ohalt Grade (AC or PG)<br>Design Asphalt Content<br>fective Asphalt Specific Gravity<br>Coarse Agg. SG<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I<br>onsultant AMRL AA<br>COMMENTS:<br>Consultant:<br>Email:<br>Phone #<br>Date<br>Prime Contractor:         | sphalt content<br>Average1<br>310 T<br>315 T<br>Company Nam<br>   | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PR OPER I<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.C.<br>LA Abrasion Loss<br>Fractured Faces (2)<br>on Oven Correction<br>dix Asphalt Accre      | TES<br>290<br>145,1<br>151,3<br>1,1<br>2,545<br>21<br>96<br>96<br>96<br>96   | pef or kg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br>Location:<br>Location:<br>Email:<br>Phone #:<br>Date:<br>Lent Engineer :<br>Email: | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |
| Average extracted a<br>(IF AVAILIBLE)<br>Field Mix Temperature<br>Asphalt Manufactures<br>phalt Grade (AC or PG)<br>Design Asphalt Content<br>flective Asphalt Content<br>flective Asphalt Content<br>Asphalt Specific Gravity<br>Coarse Agg. S.G<br>Additive (Line/other<br>Fine Agg. Angularity<br>Proposed I<br>on sultant AMRL AA<br>COMMENTS:<br>Consultant:<br>Email:<br>Phone #<br>Date: | sphalt content<br>Average 1<br>310 T<br>315 T<br>Company Nam<br>6.10 %<br>4.485 %<br>2.603<br>1.0 %<br>7.485 %<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603<br>2.603 | of the RAP<br>Penetration                 | %Add      | % MIX DE SI Lab Compa T-16 T-20 Dust/Effe I I I I I I I Hot N              | Average Viscosity<br>GN PR OPER I<br>action Temperature<br>6 Density @ Design<br>9 Density @ Design<br>Marshall Stability<br>Marshall Stability<br>Marshall Stability<br>Marshall Flow<br>ctive Asphalt (D/A)<br>Fine Agg. S.C.<br>LA Abrasion Loss<br>Fractured Faces (2)<br>on Oven Correction<br>dix Asphalt Accre      | TES<br>290<br>145,1<br>151,3<br>1,1<br>2,545<br>21<br>96<br>96<br>96<br>96   | pef or kg/m <sup>2</sup><br>lhf<br>%<br>%<br>%<br>Location:<br>Email:<br>Phone #:<br>Date:<br>lent Engineer:                         | #Ma            | rshall Blows o<br>Fik<br>Combined Virg<br>San<br>Flat & Elc | Air Void<br>VM4<br>VF4<br>m Thickness<br>TSF<br>gin Agg. S.G<br>d Equivalen<br>mgated (1:5 | s 4.0<br>15.0<br>73<br>10<br>8<br>81<br>2.569<br>t 71<br>2 |

WYDOT 414.0 (Rev. 10-18)



#### WYOMING DEPARTMENT OF TRANSPORTATION HOT PLANT MIX JOB MIX FORMULA (NON-QCQA)

E-46A (Rev. 09-16)

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| Project Number:    | ERP Number     |  |
|--------------------|----------------|--|
| Project Name:      | ERP Name       |  |
| Resident Engineer: | Engineers Name |  |
| Engineer's Town:   | Town Name      |  |

Date Submitted: XX/XX/XXX Contractor: Company Name Consultant: Company Name Class, Aggregate Type:

Level of Control, Gradation:

| SIEVE SIZE       | % PASSING<br>BIN #1 | % PASSING<br>BIN #2 | % PASSING<br>BIN #3 | % PASSING<br>BIN #4 | COMB VIRGIN | JMF<br>% | JMF LIMITS<br>% PASSING | RAP<br>CRAD.                          | COMB.<br>GRAD.                        | WIDE BAND<br>% PASSING                |
|------------------|---------------------|---------------------|---------------------|---------------------|-------------|----------|-------------------------|---------------------------------------|---------------------------------------|---------------------------------------|
| 11/2" [37.5 mm]  | 1 mar 1 mar 1 mar   | 1-1-1-1             |                     |                     | 1           | +        |                         | , *                                   | -                                     | 10                                    |
| 1" [25 mm]       | 100                 | 1                   |                     | 1                   | 100         | 100      | 100                     | 1 Q                                   |                                       | 100                                   |
| 3/4" [19 mm]     | 97                  | E                   |                     |                     | 99          | 99       | 90-100                  | · · · · · · · · · · · · · · · · · · · | · · · · · · · · · · · · · · · · · · · | 90-100                                |
| 1/2" [12.5 mm]   | 46                  | 100                 | 18. IN              |                     | 85          | 85       | 80-90                   |                                       | ·                                     | 55-90                                 |
| 3/8" [9.5 mm]    | 12                  | 86                  | 100                 |                     | 73          | 73       | 68-78                   | 1                                     | 1                                     | 45-85                                 |
| No . 4 [4.75 mm] | 2                   | 3                   | 63                  | 1                   | 49          | 49       | 44-54                   | 1                                     |                                       | 30-65                                 |
| No . 8 [2.36 mm] | 1                   | 2                   | 53                  | 1                   | 31          | 31       | 27-35                   | 1                                     |                                       | 20-50                                 |
| No. 16 [1.18 mm] | 1                   | 2                   | 35                  | i 11                | 21          | 21       |                         | 1                                     |                                       | · · · · · · · · · · · · · · · · · · · |
| No. 30 [600 µm]  | 1                   | 2                   | 24                  | -                   | 14          | 15       | 12-18                   | . D                                   | 1                                     | 5-30                                  |
| No. 50 [300 µm]  | 1                   | 1. A; III           | 17                  | C                   | 10          | 10       |                         | )                                     | 1                                     | 1                                     |
| No. 100 [150 µm] | 1                   | 1                   | 13                  | (                   | 8           | 8        |                         | 1                                     | 1                                     |                                       |
| No. 200 [75 µm]  | 0.4                 | 0.5                 | 8.8                 | (                   | 5.3         | 5.3      | 3.0-7.0                 |                                       |                                       | 2.0-7.0                               |

The virgin material was combined at the following percents (%):

| BIN # | SIZE             | SOURCE   | PERCENT (%) |
|-------|------------------|----------|-------------|
| - 4   | Size & Aggregate | Pit Name | 28          |
| 2     | Size & Aggregate | Pit Name | 14          |
| 3     | Size & Aggregate | Pit Name | 58          |

| Compaction Temperature                 |       | 200             | 9E                         |
|--|-------|-----------------|----------------------------|
| Asp halt Supplier                      | Con   | pany Name       | -                          |
| Asphalt Grade (AC or PG)               |       | Grade           |                            |
| Pit name or T-146 Number               | _     |                 |                            |
| A.V.G. Gradation                       | 50    | % of Total Item | n Crushed To Date          |
|  | AGGRE | GATE PROPE      | ERTIES                     |
| Sand Equivalent                        | 71    | %               | Polish Resistant 90 * %    |
| Fractured Faces (1)                    | 96    | %               | LA Abrasion Loss 10 %      |
| Fractured Faces (2)                    | 96    | %               | Flat & Elongated (1:5) 2.0 |
| Plastic Index                          | NP    | %               | Soundness (MgSO4) 4 %      |
| Additive (Lime/Other)                  | 1.0   | %               |                            |
| Proposed Paving Date:                  | -     |                 |                            |
| OMMENTS: * Insoluble Residue           |       |                 |                            |
| or work to the a rest to rest to rest. |       |                 |                            |
|  |       |                 |                            |

|                   | Signatures:        |   |
|-------------------|--------------------|---|
| Consultant:       | Paving Sub:        |   |
| Email:            | Email:             |   |
| Phone #:          | Phone #:           |   |
| Date:             | Date:              | ; |
| Prime Contractor: | Resident Engineer: |   |
| Email:            | Email:             |   |
| Phone #:          | Phone #:           |   |
| Date:             | Date:              |   |
|                   |                    |   |

## DENSITY TESTING FOR COMPACTED MIX

Scope: This procedure describes the sequence of testing used to determine the In-Place Density of compacted mix. Included are the Coring Operation, Nuclear Density Correlation, Core Specimen testing with calculations for waxed and non-waxed specimens Specific Gravities and In-Place Density.

#### Apparatus: 1. Coring machine

- 2. Electronic scale readable to 0.1 gram; equipped with a suitable suspension apparatus and holder to permit weighing the specimen while suspended from the center of the bottom of the scale
- 3. Wire brush
- 4. Wet saw/chisel
- 5. Wire basket with a suspension wire of the smallest practical size to minimize any possible effects of a variable immersed length (i.e., buoyancy)
- 6. Container for water; 5 gal minimum, equipped with an overflow outlet for maintaining a constant water level
- 7. Towels
- 8. Nuclear testing device (if using)
- 9. Convection oven
- 10. Tank heater

| Reference |
|-----------|
|-----------|

| Reference  |                 |   |
|------------|-----------------|---|
| Documents: | AASHTO T 166    | Standard Method of Test for Bulk Specific Gravity of<br>Compacted Hot Mix Asphalt (HMA) Using Saturated |
|            |                 | Surface-Dry Specimens   |
|            | AASHTO T 275    | Standard Method of Test for Bulk Specific Gravity of  |
|            |                 | Compacted Hot Mix Asphalt (HMA) Using   |
|            |                 | Paraffin-Coated Specimens   |
|            | WYDOT 401.4.7.5 | WYDOT Standard Specifications   |
|            | WYDOT 401.4.8   | WYDOT Standard Specifications   |
|            | WYDOT 215.0     | In-Place Density and Moisture Content of Soil and   |
|            |                 | Soil-Aggregate by Nuclear Methods (Shallow  |
|            |                 | Depth)  |
|            | WYDOT 417.0     | Precision Statements for Comparing Contractor QA  |
|            |                 | Results to WYDOT Verification Results   |
|            | WYDOT 418.0     | Recommended Procedure For Nuclear Density   |
|            |                 | Gauge Correlation (Bituminous Pavements)  |
|            | WYDOT 800.0     | Random Number Selection for Density and   |
|            |                 | Gradation Testing   |
|            | WYDOT T-108     | Asphalt Base/Pavement Density Report  |
|            |                 | - V - 1   |

Sampling: Sample locations will be randomly selected by the engineer representative using a table of random numbers in accordance with WYDOT 800.0 or a random number generator, staying one foot away from the pavement ribbon edge as determined by

the engineer (per section 2.2 of 401.4.7.5 of *WYDOT Standard Specifications*). If the surface texture of the test site is excessively open, or for some reason the surface will not allow testing at the pre-identified location, another location should be selected by the engineer, staying as close as possible to the original location.

Pavement sampling will be accomplished with a coring machine. If a nuclear testing device is to be used, it will be for informational purposes only. All quality assurance (QA) testing will be performed for mix in-place density on cores. The correlation, WYDOT 418.0, should be performed as soon as possible after pavement compaction begins, usually during evaluation of the test strip. Correlation is made by comparing the density obtained using the nuclear device to the density obtained from the core. Correlation is needed because of influences of surface textures, material weight below the compacted test lift and the aggregate composition within the compacted test lift.

Replace section 4.2 of AASHTO T 166 with the following:

4.2 Determine bit diameter based on the nominal maximum size of the aggregate being tested. Nominal maximum size is one size larger than the first sieve to retain more than 10 percent. If the nominal size of the aggregate is 1 inch or less, a 4 inch diameter drill bit or larger should be used.

Locate the test locations using the random number procedure in WYDOT 800.0

The procedure for running correlation is to place the nuclear device onto the randomly selected test site before the core is drilled and mark the outline of the nuclear device on the pavement. Take the average of two one-minute readings and record on Form T-108. On multi-lift pavement, a correlation should be run for each lift as described in WYDOT 418.0.

- Coring: After the finish rolling has been completed and the mat has cooled to ambient temperature, cores can be taken. If for some reason, cores are needed from the hot pavement, the area to be cored may be cooled. Blocks of dry ice or ice may be used until the internal temperature has cooled to at least 130 °F to sufficiently ensure that the sample is not distorted, bent, cracked, or has any change in its physical condition.
  - Note: The contractor or his representative will obtain all cores in the presence of a WYDOT inspector.

If the core is damaged, then a new core will be drilled as close as possible to the original location.

Collect two cores (contractor's acceptance (QA) and WYDOT's verification (QC)) at each location in the presence of a WYDOT inspector. Mark a sample number on each core for identification later. The WYDOT inspector will keep the WYDOT's core in his/her control at all times. The contractor will separate lifts of

WYDOT cores in the presence of the WYDOT inspector. Refer to Section 401.4.8 of WYDOT Standard Specifications and WYDOT 417.0 Precision Statements for Comparing Contractor QA Results to WYDOT Verification Results Table 2 for Verification and Acceptance Procedures.

Backfill the core hole made from the coring operation with Hot Plant Mix. Compact the Hot Plant Mix with a tamping bar or an equivalent method. If Hot Plant Mix is not available, a ready mix concrete or fast set grout product may be used in lieu of Hot Plant Mix. Fill the core holes prior to the next lift placement or prior to seasonal shutdown, whichever is sooner.

### Preparation

of Samples: Bring the core sample to room temperature at  $77 \pm 9$  °F and clean off any foundation material such as; prime coat, soil, crushed base, or cement treated base. A stiff wire brush may facilitate cleaning.

Separate any lifts from the compacted test lift during construction of multi-lift pavements. Separation by the use of a wet saw is preferred. Care should be taken to not damage the core. The top and/or bottom of each core should then be clean of any material not part of the compacted test lift such as seal coat, tack coat, plant mix wearing course, or any foreign material such as striping tape, etc.

Insure the sample number is legible on each core for identification later. Record on Form T-108 the sample number for each test specimen taken. When correlating the nuclear tests, both cores and nuclear readings will have the same number, with the nuclear test number having a letter i.e. "N" added. When the nuclear testing device has been correlated, the continuous count will be with numbers only. Record on Form T-108: date sampled, station sampled, section represented, lane taken, distance from centerline, and core thickness of the compacted test lift only. Refer to example Form T-108 of this section.

Note: Record test specimen thickness to the nearest <sup>1</sup>/<sub>4</sub> inch measured and an average from three locations on the core.

### Non-Waxed

Procedure: Use only individual weights from the desired lift for density determination. Record the core test sample weight (mass) to the nearest gram on Form T-108.

1. Weigh the core after the core has been immersed in water at  $77 \pm 1.8$  °F for three to five minutes. Designate this weight as "E" on Form T-108. Each specimen will be immersed and weighed individually.

To avoid error, use the same scale to obtain all weights.

Note: Assure water level stays at optimum over flow level.

2. Weigh the Saturated Surface Dry core (SSD) in air. Designate this weight (mass) as "B" on Form T-108.

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Remove the immersed core sample from the water. Using a damp towel blot the core until saturated surface dry (SSD), as quickly as possible not to exceed 5 seconds. Weigh the core in air on the same scale as Step 1.

A damp towel is considered when no water can be wrung from it.

Note: Any water that seeps from the test specimen during weighing is considered part of that saturated specimen (SSD).

Early in the pavement operation, check the first cores to determine if waxing is necessary (more than 2 percent absorption by volume). Continual absorption checks should be made throughout the project duration. If one core of a lot must be waxed, all cores in that lot must be tested using the wax procedure.

- Note: Allow corelok with approved calibration. Corelok may be used upon engineer's acceptance of a method and calibration process.
- 3. Weigh the completely dried core sample in air. Designate this weight (mass) as "A" on Form T-108.

During testing, WYDOT and the contractor will dry the cores in a convection oven to a constant weight (mass) with a nondestructive method.

Note: If desired, the sequence of testing operation may be changed. For example, first the dry weight "A" can be obtained and then the weight in water "E" and then the saturated surface dry weight "B". If the sequence of testing is changed and the dried core weight "A" is taken first, the core must be carefully dried in an oven at a temperature not to exceed  $125 \pm 5$  °F so as to not cause any distortion or disintegration of the core. Drying is not complete until a constant weight is obtained (constant weight equals weight of core and does not change more than 0.05 percent when weighed at 2 hour intervals). Drying the core rapidly using excessive heat will damage the core.

Cores with visible moisture on the surface will take at least several hours to dry at 125 °F. Drying is not complete until a constant weight is obtained (i.e., weight of core changes by 0.05 percent or less between two hour intervals at this drying temperature). Turning and/or flipping the core specimen while drying may help to expose any trapped moisture.

Calculation: Calculating for dry weight;

 $\frac{(\text{Wet Weight-Dry Weight})}{(\text{Dry Weight})} \times 100 = \text{calculating for drying to } 0.05 \% \text{ or less.}$ 

Calculating Specific Gravity;

SG = 
$$\frac{A}{(B-E)}$$
 = non-waxed core

Example Calculating unit weight, lb/ft<sup>3</sup>

Note: Form T-108 is formulated for calculating lb/ft<sup>3</sup>, to compare to the Nuclear Unit Weight.

non-waxed core UW =  $\frac{A}{(B-E)} \times Cd$ 

Where:

- SG = Specific Gravity; round to three places past the decimal A = Mass of sample in air after drying, g
  - A = Mass of sample in an arter drying, g
  - B = Mass of saturated surface dry (SSD) sample in air, g
  - E = Mass of sample in water (wet weight), g
- Cd = 62.4 for English units lb/ft<sup>3</sup>
- $UW = Unit Weight in lb/ft^3$

Calculating for percent Density;

$$\frac{UW}{VUW} \times 100 =$$
 Percent Density

Where:  $VUW = Voidless Unit Weight from the mix design, lb/ft^3$ 

Note: Find the volume of water absorbed by the core, in percent, to determine if cores should be waxed. If more than two percent water is found, use the waxed procedure.

Calculating for percent of water absorbed;

$$\frac{B-A}{B-E} \ge 100 = \text{Percent Water Absorbed}$$
Where:  

$$A = \text{Mass of sample in air after drying, g}$$

$$B = \text{Mass of saturated surface dry (SSD) sample in air, g}$$

$$E = \text{Mass of sample in water (wet weight), g}$$

Waxed

Procedure: This method is performed on samples with open or interconnected voids or on samples that have absorbed over 2 percent by volume as determined by steps 1 through 3

previously listed.

1. Weigh the completely dried core sample in air. Designate this weight (mass) as "A" on Form T-108.

The only procedure that can be used in running a wax density tests is in the order shown. Early in the pavement operation, check the first cores (as shown above) to determine if waxing is necessary and continual checks should be made throughout the project duration.

2. Put wax into a pan to be melted, have another pan full of water being heated. Place the pan with wax into the pan of hot water. To melt the wax, do not use direct heat from any kind of burner. The warm wax is ready when it is approximately 10° F above melting. Dip the core into the wax and cover all surfaces. It may be necessary to brush on melted wax to fill any pinholes left on the surface. Do not use too much wax. Allow 30 minutes to cool before weighing.

Weigh the waxed sample in air. Designate this weight (mass) as "B" on Form T-108.

3. Weigh the waxed sample immersed in water at  $77 \pm 1.8$  °F. Designate the weight (mass) as "E" on Form T-108.

Each specimen will be immersed and weighed individually.

Use the same scale as used to find the weight in air.

Note: Form T-108 is formulated for calculating lb/ft<sup>3</sup>, to compare to the Nuclear Unit Weight.

Calculation: Calculate Specific Gravity;

$$SG = \frac{A}{(B-E) - \frac{(B-A)}{D}}$$

Example calculating unit weight, lb/ft<sup>3</sup>

Waxed Core UW = 
$$\frac{A}{(B-E)-\frac{(B-A)}{D}} \times Cd$$

| Where: | SG = | Specific Gravity; round to three places past the decimal               |
|--------|------|--|
|        | A =  | Mass of sample in air after drying, g                                  |
|        | B =  | Mass of waxed core sample (SSD) sample in air, g                       |
|        | D =  | Specific gravity of the wax; round to four places past the             |
|        |      | decimal for weights  |
|        | E =  | Mass of waxed core sample in water (wet weight), g                     |
|        | Cd = | $62.4$ for English units $lb/ft^3$                                     |
|        | UW = | Unit Weight in lb/ft <sup>3</sup> ; truncate to 1 decimal place, tenth |
|        |      |  |

Percent of Maximum Density;

 $\frac{UW}{VUW} \ge 100$  = Percent Density; round to 2 decimal place

Where: VUW = Voidless Unit Weight from mix design JMF letter, lb/ft<sup>3</sup>

Report: Report the specific gravity, unit weight, voidless unit weight, and percent density on Form T-108.

|                   | Can all   | 30   | ~  |       | WYOM<br>I<br>ASPH.   | UNG DI<br>MATER<br>ALT BA                  | CPART<br>IALS T<br>SE / PA                     | VIENT C<br>ESTING<br>VEMEN   | DF TRA  | WYOMING DEPARTMENT OF TRANSPORTATION<br>MATERIALS TESTING LABORATORY<br>ASPHALT BASE / PAVEMENT DENSITY REPORT   | IATIO'<br>Y<br>SPORT   |   |                            |              | Form T-108<br>(Rev. 10-18) |
|-------------------|---|--|--|-------|--|--|--|--|---|--|--|---|----------------------------|--------------|----------------------------|
| Pro<br>Pri<br>Gra | Project No:<br>Project Name:<br>Engineer:<br>Pit or Source:<br>Grading/Type:<br>Conling/Type: | Project No: <u>ERP</u> Project Number<br>Project Name: <u>As listed on Plans</u><br>Engineer: <u>Resident Engineer</u><br>Pit to Source: <u>As listed on Plans</u><br>Grantardor: <u>As listed on Plans</u><br>Contractor: <u>Contranve Mane</u> | t Number<br>1 Plans<br>1 Plans<br>1 Plans<br>1 Plans<br>1 ame                |       |  |  |  |  | ŏ   | Lot No:<br>Section(s) Represented:<br>Tons in Lot:<br>Date Placed:<br>Date Cored:<br>Date Tered:   | Lot No:<br>Represented:<br>Tous in Lot:<br>Date Placed:<br>Date Cored: | ### 10 ###<br>### 10 ###<br>####<br>####<br>MM2d5/Ynr<br>Mad7Yr | ###<br>###<br>N/IF<br>N/IF | RT           | :Lane<br>:Lane             |
|                   | ousultant:  |  | lame   |       |  |  |  |  |   | La   | b Max Vo   | Lab Max Voidless Unit Weight (VUW)                              | ight (VUW)                 | 155.0        | pcf                        |
|                   |   | Distance   |  |       | C are  |  | Weight in Air                                  |  | н   | Weight in Water  | 1.2.15   | Abserption **   | Specific<br>Gravity        | Density (pd) | % Max Density              |
| Core≄             | Station<br>Sampled  | from   | Lane   | Lüft  | Thickness  | Dry Wt.*                                   | SSD Wt.  | Wax SSD Wc   | Na Wi   | UNNAR WC.  |  |   |                            | (MU)         | S.                         |
|                   |   | Centerline   |  |       | (Inches)   | (¥)  | (B)  | (L)  | (3)   | (E)  | (B-E)  | (B-A) X 100<br>(B-E)  | See note below             | SGX @.4      | UN X 100                   |
| 1-1               | 594+38  | 9.5  | Right  | Upper | 2 1/4  | 1032.1                                     | 1033.8   |  |   | 596.0  | 437.8  | 0.39%   | 2.357                      | 147.0        | 94.84%                     |
| 1-2               | 59 <del>4-</del> 00   | 6.6  | Right  | Upper | 2  | 1235.9                                     | 1237.0   |  |   | 715.7  | 521.3  | 0.21%   | 2.371                      | 147.9        | 95.42%                     |
| 1-3               | 601+94  | 4.5  | Right  | Upper | 2  | 885.2                                      | 886.6  |  |   | 511.5  | 375.1  | 962210  | 2.360                      | 147.2        | 94.97%                     |
| 1-4               | 602+30  | <u>5</u> .0  | Right  | Upper | 2  | 818.8                                      | 2.918  |  |   | 471.6  | 348.1  | 0.26%   | 2.352                      | 146.7        | 94.65%                     |
| 1-5               | 608+13  | 7.8  | Left   | Upper | 2  | 1019.3                                     | 1020.6   |  |   | 586.7  | 433.9  | 0.30%   | 2.349                      | 146.5        | 94.52%                     |
| 1-6               | 611+39  | 8.8  | Left   | Upper | 2 1/4  | 1070.1                                     | 1071.7   |  |   | 614.0  | 457.7  | 965£.0  | 2.338                      | 145.8        | 94.06%                     |
| 1-7               | 615+15  | 10.0   | Center   | Upper | 2 1/2  | 8.0£6                                      | 932.7  |  |   | 529.2  | 403.5  | 0.47%   | 2.307                      | 143.9        | 92.84%                     |
|                   |   |  |  |       |  |  | Ave<br>Den                                     | Average<br>Density   | 94.47   | Stan<br>Dev  | 0.832  |   |                            |              |                            |
| Remarks           |   |  |  |       |  |  |  |  |   |  |  |   |                            |              |                            |
| Pn                | Prepared By:  |  |  |       |  | Date:                                      |  |  |   |  | Tested By  | Tested By (Print Name)  |                            |              |                            |
| Ð                 | Checked By:   |  |  |       |  | Date:                                      |  |  | -41 E 4                                       |  | Ce   | Certification No.   |                            |              |                            |
|                   | Specific Gravi<br>Unwaxad Core<br>(BAE)<br>(B-E)  | 2  | Calculations<br>Warked Core<br>(F - C) - (F - A)<br>(F - C) - (F - A)<br>0.9 |       | Notes:<br>* Drying is<br>drying in an<br>** If the abs<br>MTM. | not complet<br>oven (does<br>sorbtion is > | e until a coo<br>: not alter w<br>:2.0% use ti | Notes:<br>* Drying is not complete until a constant weight is obtained a<br>drying in an oven (does not after weight of core by $> 0.05\%$ )<br>** If the absorbtion is $> 2.0\%$ use the waxed procedure in Set<br>MTM. | t is obtained<br>e by > 0.05%<br>ocedure in S | Notes:<br>* Drying is not complete until a constant weight is obtained after two hours of<br>drying in an oven. (does not after weight of core by > 0.05%).<br>** If the absorbtion is > $2.0\%$ use the waxed procedure in Section 415.0 of the<br>MTM. | urs of<br>of the   |   |                            |              |                            |

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# PRECISION STATEMENTS FOR COMPARING MIX DESIGN AND AGGREGATE PROPERTY TEST RESULTS

Scope: The following precision statements define the allowable differences for comparing aggregate properties (Table 1) and mix design(s) (Table 2) between laboratories.

Use: The precision statements are used to compare contractor and WYDOT mix design(s) and aggregate results to identify discrepancies.

#### Reference

| Documents: | WYDOT 114   | WYDOT Standard Specifications                                    |  |  |  |
|------------|-------------|--|--|--|--|
|            | WYDOT 401   | WYDOT Standard Specifications                                    |  |  |  |
|            | WYDOT 803   | WYDOT Standard Specifications                                    |  |  |  |
|            | WYDOT 414.0 | Marshall Mix Design and Mix Volumetric Verification<br>Procedure |  |  |  |

# Table 1

Allowable Difference between WYDOT's and contractor's Aggregate Results:

| Aggregate Criteria                     | Allowable<br>Difference |
|--|-------------------------|
| LA Abrasion Loss, %                    | 5                       |
| Flat & Elongated, 1:5 ratio, %         | 4                       |
| Sand Equivalent, %                     | 15                      |
| Fractured Faces, %                     | 5                       |
| Fine Aggregate Angularity, %           | 3                       |
| Soundness (MgSO <sub>4</sub> ) Loss, % | 5                       |

# Table 2

Allowable Difference between WYDOT's and contractor's Mix Design Results:

|  | Allowable Difference |           |
|--|----------------------|-----------|
| Mix Criteria   | Marshall             | Superpave |
| Bulk Specific Gravity (G <sub>mb</sub> ) (Coarse & Fine) | 0.03                 | 0.03      |
| Air Voids (V <sub>a</sub> ), %                           | 1.2                  | 1.2       |
| Voids in Mineral Aggregate (VMA), %                      | 1.2                  | 1.2       |
| Voids Filled with Asphalt Binder (VFA), %                |                      | 8.0       |
| Marshall Stability, lb                                   | 900                  |           |
| Marshall Flow, 0.01 in                                   | 3                    |           |
| Tensile Strength Retained (TSR), %                       | 8                    | 8         |
| Film Thickness (F.T.), µm                                | 2                    | 2         |
| Dust to Effective Asphalt Binder Ratio (D/A)             | 0.3                  | 0.3       |
| Voidless Unit Weight (VUW), lb/ft <sup>3</sup>           | 1.5                  | 1.5       |

# PRECISION STATEMENTS FOR COMPARING CONTRACTOR QA RESULTS TO WYDOT VERIFICATION RESULTS

- Scope: The following precision statements define the allowable differences comparing gradations (Table 1) and density (Table 2) between laboratories.
- Use: The precision statements are used to compare contractor and WYDOT gradation and density results to identify discrepancies.

#### Reference

| Documents: | WYDOT 401   | WYDOT Standard Specifications        |
|------------|-------------|--------------------------------------|
|            | WYDOT 414   | WYDOT Standard Specifications        |
|            | WYDOT 415.0 | Density Testing for Compacted Mix    |
|            | WYDOT 814.0 | Sieve Analysis of Combined Aggregate |

|                                  | Allowable Gradation Difference |                                  |          |                                  |      |          |  |  |  |
|----------------------------------|--------------------------------|----------------------------------|----------|----------------------------------|------|----------|--|--|--|
|                                  | Grading (Nominal Maximum Size) |                                  |          |                                  |      |          |  |  |  |
|                                  | 1 inch                         | <sup>3</sup> ⁄ <sub>4</sub> inch | 1⁄2 inch | <sup>3</sup> / <sub>8</sub> inch | PMWC | Concrete |  |  |  |
| Sieve                            |                                | Allowable Difference             |          |                                  |      |          |  |  |  |
| Sleve                            |                                |                                  | (% Pa    | ssing)                           |      |          |  |  |  |
| 1 ¼ inch                         | 1.5                            |                                  |          |                                  |      | 1.5      |  |  |  |
| 1 inch                           | 2.0                            | 1.5                              |          |                                  |      | 2.0      |  |  |  |
| <sup>3</sup> ⁄ <sub>4</sub> inch | 3.0                            | 2.0                              | 1.5      |                                  |      | 3.0      |  |  |  |
| <sup>1</sup> / <sub>2</sub> inch | 3.4                            | 3.0                              | 2.0      | 1.5                              | 1.5  | 3.4      |  |  |  |
| <sup>3</sup> / <sub>8</sub> inch | 3.4                            | 3.4                              | 3.4      | 2.0                              | 2.0  | 3.4      |  |  |  |
| No. 4                            | 3.4                            | 3.4                              | 3.4      | 3.4                              | 3.4  | 3.4      |  |  |  |
| No. 8                            | 3.3                            | 3.3                              | 3.3      | 3.3                              | 3.3  | 3.3      |  |  |  |
| No. 16                           |                                |                                  |          |                                  |      | 3.3      |  |  |  |
| No. 30                           | 2.9                            | 2.9                              | 2.9      | 2.9                              |      |          |  |  |  |
| No. 50                           |                                |                                  |          |                                  |      | 2.9      |  |  |  |
| No. 100                          |                                |                                  |          |                                  |      | 2.9      |  |  |  |
| No. 200                          | 1.2                            | 1.2                              | 1.2      | 1.2                              | 1.2  | 1.2      |  |  |  |

|           | Table 1   |            |
|-----------|-----------|------------|
| Allowable | Gradation | Difference |
|           |           |            |

Table 2

|         | Allowable Density Difference |
|---------|------------------------------|
| Density | $1.5 \text{ lb/ft}^3$        |

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## RECOMMENDED PROCEDURE FOR NUCLEAR DENSITY GAUGE CORRELATION (BITUMINOUS PAVEMENTS)

- Scope: The degree of correlation between unit density determined with the nuclear density gauge and the unit density of the core samples is needed when utilizing a nuclear density gauge to determine in-place density measurements on bituminous paving projects.
- Use: On WYDOT paving projects, cores are required for quality acceptance and verification density testing for In-Place Density Designation I and II mix pavement.

Nuclear density testing could be used for quality control testing and In-Place Density Designation II testing of mix surfaces, stabilized base density testing, etc.

The unit density analysis should be performed on the portion of the core sample that represents that lift only. For example, when determining the correlation on the top lift of pavement, the top lift should be separated from the first lift and only that portion of the core should be used to determine the core unit density.

#### Reference

| Documents: | WYDOT 415.0 | Density Testing for Compacted Mix    |
|------------|-------------|--------------------------------------|
|            | WYDOT T-108 | Asphalt Base/Pavement Density Report |

- Apparatus: 1. Nuclear density gauge
  - 2. Coring machine
- Procedure: Obtain nuclear density readings at each location at the same time that cores are obtained. Use the average of two one-minute nuclear readings taken at each core location for the correlation. Use a minimum of seven cores and seven corresponding nuclear density readings to perform this correlation.

Report the calculated unit densities of the cores and the nuclear unit densities on Form T-108, *Asphalt Pavement Density Report*. An example of Form T-108 can be found in WYDOT 415.0.

Calculate a correlation factor for the nuclear gauge reading as follows:

1. Calculate the difference between the core density and nuclear gauge density at each test site to the nearest 0.1 pcf. Calculate the average difference and standard deviation of the differences for the entire data set to the nearest 0.1 pcf.

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- 2. If the standard deviation of the differences is equal to or less than 2.5 pcf, the correlation factor applied to the nuclear density gauge reading will be the average difference calculated above in step 1.
- 3. If the standard deviation of the differences is greater than 2.5 pcf, the test site with the greatest variation from the average difference must be eliminated from the data set and the data set properties and correlation factor recalculated following above steps 1 and 2.
- 4. If the standard deviation of the modified data set still exceeds the maximum specified in step 2, eliminate additional test sites from the data set will be recalculated using the correlation factor following steps 1 and 2. If the data set consists of less than five test sites, additional test sites must be established.
- Report: Report core unit densities, nuclear density results, and correlation results on Form T-108.

#### VOIDLESS UNIT WEIGHT VERIFICATION AND FIELD ADJUSTMENT

- Scope: This procedure describes the verification and adjustment of the production mix Voidless Unit Weight (VUW). The VUW is sometimes referred to as maximum density, theoretical maximum weight, maximum specific gravity (G<sub>mm</sub>), or Rice specific gravity.
- Use: The VUW determined from the construction mix design is developed under controlled conditions. Construction introduces many variables which may result in variation between the VUW stated in the JMF letter from the construction mix design and the VUW determined during production of the mix. Therefore, adjustment of the VUW used for density control may be warranted. This adjustment is based on the VUW and extracted asphalt content test results. Submit VUW and extracted total asphalt content test results according to *WYDOT Standard Specifications* 401.4.11, to the engineer, which will be forwarded to the Materials Program.

The WYDOT Materials Program will analyze and adjust the VUW according to the procedures described below. In addition, the contractors test results may be verified by the WYDOT Materials Program as determined by the engineer and Materials Program. Adjustments to the VUW will apply to field control in accordance with *WYDOT Standard Specifications* 401.4.11.

Reference

| Reference  |                |  |
|------------|----------------|--|
| Documents: | AASHTO T 164   | Standard Method of Test for Quantitative Extraction of Asphalt |
|            |                | Binder from Hot Mix Asphalt (HMA)                              |
|            | AASHTO T 209   | Standard Method of Test for Theoretical Maximum Specific       |
|            |                | Gravity and Density of Hot Mix Asphalt (HMA)                   |
|            | AASHTO T 308   | Standard Method of Test for Determining the Asphalt Binder     |
|            |                | Content of Hot Mix Asphalt (HMA) by the Ignition Method        |
|            | WYDOT 114      | WYDOT Standard Specifications                                  |
|            | WYDOT 401.4.11 | WYDOT Standard Specifications                                  |
|            | WYDOT 410.0    | Sampling Mix   |
|            | WYDOT 411.0    | Transporting Mix Samples                                       |
|            | WYDOT 414.0    | Marshall and Superpave Mix Design and Mix Volumetric           |
|            |                | Verification Procedure   |
|            |                |  |

Procedure: Sample in the presence of a WYDOT representative, transport if necessary, and split if necessary, the mix in accordance with WYDOT 410.0 and WYDOT 411.0. WYDOT must maintain possession of the WYDOT cores at all times. Submit split samples to the appropriate WYDOT field office. If evaluation of the test results indicates that a VUW adjustment is warranted, the engineer will submit the split samples to the WYDOT Materials Program for verification purposes.

Report the VUW and extracted total asphalt content for at least four field mix samples collected at four separate sampling locations. These samples may be volumetric verification samples. Each field mix sample will consist of three samples (typically nine cylinder cans for volumetric verification), divided as follows;

One sample comprised of three cylinder containers to be tested by the contractor,

One sample comprised of three containers submitted to WYDOT, and

One sample comprised of three cylinder containers retained by WYDOT as a referee sample.

Resolve discrepancies in accordance with *WYDOT Standard Specifications* Section 114, Laboratory, Personnel, and Correlation.

Determine the VUW for each sample according to AASHTO T 209. Replace Section 14.2.1 of AASHTO T 209 with: Calculate the Voidless Unit Weight at 77 °F by multiplying the maximum specific gravity ( $G_{mm}$ ) by 62.4 pounds per cubic foot.

Determine Total Asphalt Content (TAC) using either AASHTO T 164 (Method B) or AASHTO T 308. When using AASHTO T 164 (Method B), no correction factor is applied. When using AASHTO T 308, establish and apply the correction factor.

Calculations: Adjust the mix design equation for the field results using the following procedure:

1. Utilizing the equation developed during the mix design process, calculate the predicted Voidless Unit Weight, VUW<sub>p</sub>, for each field asphalt content. The mix design equation will be in the following form:

$$VUW_p = m x TAC + b,$$

| VUW <sub>1</sub> | p =   | predicted VUW at the evaluated asphalt content; |
|------------------|-------|---|
| TAC              | =     | evaluated total asphalt content;                |
| b                | =     | y intercept;                                    |
| m                | =     | slope of the line                               |
|                  | TAC b | U   |

2. Determine the difference between the reported VUW and  $VUW_p$  for each test result;

$$D_n = VUW_n - VUW_p$$

3. Calculate the average of the difference between the construction mix and the predicted VUW;

$$\overline{D} = \sum D_n / n$$

4. Determine  $b_{adj}$  by adding the average difference between VUW<sub>p</sub> and the field mix VUW,  $\overline{D}$ , to b and replace the original b value in the equation from step 1 so it will be in the form;

$$VUW_a = m \times TAC + b_{adj}$$

- 5. Calculate VUW<sub>a</sub> using this adjusted formula for each test result;
- 6. Determine the absolute difference between VUW<sub>a</sub> and the field mix VUW;

$$D_{an} = /VUW - VUW_a /$$

If  $D_{an}$  is greater than 1.5, then the VUW is considered an outlier. The outlier will be eliminated and the equation for VUW<sub>a</sub> will be developed with the remaining test results using procedure numbers 1 through 4 above. If two outliers are suspected, further evaluation and verification of the test results by the WYDOT Materials Program will be required.

7. Using the adjusted VUW using the final equation for VUW<sub>a</sub> from step 4 for the target asphalt content.

If  $VUW_a$  differs more than 0.50 lb/ft<sup>3</sup> from the design VUW, then the adjusted Voidless Unit Weight will be used for construction control purposes.

Additional field adjustments to the VUW will be considered after at least four additional consecutive test results are submitted to the engineer and the WYDOT Materials Program and if the absolute difference of adjustment exceeds  $0.50 \text{ lb/ft}^3$ .

Example Calculations:

A. Record the equation developed during the mix design,

| Mix Design Information |                |  |  |  |  |
|------------------------|----------------|--|--|--|--|
| TAC, %                 | VUW, $lb/ft^3$ |  |  |  |  |
| 4.50                   | 155.2          |  |  |  |  |
| 5.00                   | 153.0          |  |  |  |  |
| 5.50                   | 151.4          |  |  |  |  |
| 6.00                   | 149.6          |  |  |  |  |
| b =                    | 171.6          |  |  |  |  |

 $VUW_P = -3.68 \text{ x TAC} + 171.6$ 

| Target:    | 4.90%  | asphalt | @      | 153.6 lb/ft <sup>3</sup> (VUW | 7) |
|------------|--------|---------|--------|-------------------------------|----|
| I ui gott. | 1.2070 | usphan  | $\sim$ | 155.010/10 (10.00             | /  |

B. Record the construction mix data. Calculate VUW<sub>p</sub>,  $D_n$ , and  $\overline{D}$ .

| Constru | ction Data |       |      |
|---------|------------|-------|------|
| TAC     | VUW        | VUWp  | D    |
| 5.23    | 151.1      | 152.4 | -1.3 |
| 5.07    | 151.6      | 152.9 | -1.3 |
| 4.80    | 151.8      | 153.9 | -2.1 |
| 4.90    | 152.8      | 153.6 | -0.8 |
| 5.20    | 153.5      | 152.5 | 1.0  |
|         |            | D     | -0.9 |

C. Determine  $b_{adj}$  by adding  $\overline{D}$  to b and substituting  $b_{adj}$  for b into the mix design equation in order to calculate VUW<sub>a</sub>.

$$b_{adj} = 171.6 - 0.9 = 170.7$$
  
VUW<sub>a</sub> = - 3.68 x TAC + 170.7

D. Calculate  $VUW_a$  for each field determined asphalt content. Outliers are detected when a  $D_a$  exceeds 1.5. Since the difference for the last test result does exceed 1.5, this test result is an outlier and eliminated.

| Construction Data |       |                         |       |               |
|-------------------|-------|-------------------------|-------|---------------|
| TAC VUW           |       | <b>VUW</b> <sub>a</sub> | $D_a$ |               |
| 5.23              | 151.1 | 151.5                   | 0.4   |               |
| 5.07              | 151.6 | 152.0                   | 0.4   |               |
| 4.80              | 151.8 | 153.0                   | 1.2   |               |
| 4.90              | 152.8 | 152.7                   | 0.1   |               |
| 5.20              | 153.5 | 151.6                   | 1.9   | >1.5, Outlier |

E. Determine the VUW adjustment equation with the outlier removed.

| Constru | ction Data       |                    |       |
|---------|------------------|--------------------|-------|
| TAC     | VUW              | VUWp               | $D_n$ |
| 5.23    | 151.1            | 152.4              | -1.3  |
| 5.07    | 151.6            | 152.9              | -1.3  |
| 4.80    | 151.8            | 153.9              | -2.1  |
| 4.90    | 152.8            | 153.6              | -0.8  |
|         |                  | $\overline{D}_{n}$ | -1.4  |
|         | b <sub>adj</sub> | 170.2              |       |

 $VUW_a = -3.68 \text{ x TAC} + 170.2$ 

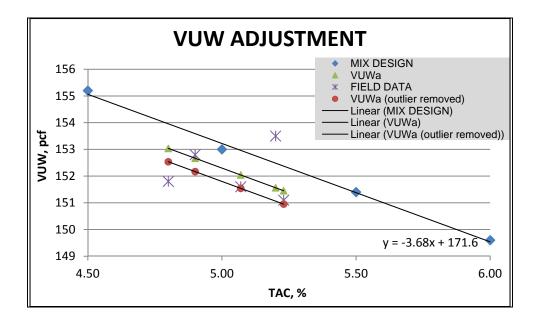
F. Calculate the adjusted voidless unit weight for the design asphalt content.

$$VUW_a = -3.68 \times 4.9 + 170.2 = 152.2 \text{ lb/ft}^3$$

G. Determine the difference between the mix design VUW and the adjusted VUW.

Difference = 
$$VUW - VUW_a = 153.6 - 152.2 = 1.4 \text{ pcf} > 0.5 \text{ pcf}$$

Since the difference exceeds  $0.50 \text{ lb/ft}^3$ , the adjusted VUW of 152.2 pcf will be used for construction control at the target asphalt content of 4.90%.



### ASPHALT / LIME CONTENT REPORT (INVOICE AND TANK VOLUME)

- Scope: This form calculates the quantity of Performance Graded Asphalt Binder (PGAB) and Hydrated Lime incorporated into Hot Plant Mix (HPM) utilized on the project. This procedure describes the calculations involved in determining asphalt binder and lime content by percentage and as a tonnage from the levels in the storage tank(s), determined by "tank stabs" for Asphalt Binder, and the weight (mass) for Hydrated Lime. This procedure also describes instructions for calculations used on WYDOT Form E-56. Hydrated Lime is based on the percentage of asphalt binder and lime in the HPM.
- Use: This procedure is used to report the daily Asphalt Binder Content and Lime Content used in the production of mix, such as Hot Plant Mix (HPM) pavement and Plant Mix Wearing Course (PMWC). The amount of asphalt binder and lime used is determined on a daily basis, based on the amount of asphalt binder and lime delivered and the levels in the storage tank(s) for asphalt binder (PGAB). Refer to *WYDOT Standard Specifications* subsection 2.3 of 401.4.7.5, paragraph 2.3, for PGAB and *WYDOT Standard Specifications* 413.3 paragraph 4 for Hydrated Lime measurements.

| Reference  |        |                 |  |
|------------|--------|-----------------|--|
| Documents: | WYDO   | OT 401          | WYDOT Standard Specifications  |
|            | WYDO   | OT 413          | WYDOT Standard Specifications  |
|            | WYDO   | OT 841.0        | Asphalt Volume Correction Table  |
|            | WYDO   | DT E-56         | Asphalt and Lime Report  |
| Apparatus: | 1.     | Calibrated me   | asuring stick to measure (stab) the depth of asphalt binder in   |
| 11         |        | the storage tan |  |
|            | 2.     | WYDOT For       | m E-56, daily Asphalt and Lime Report of Asphalt Binder<br>Lime Used (see example in this section). Form is available                                      |
|            | 3.     |                 | ery invoices, Certificates of Compliance (COC), and loading  |
|            | 4.     | Storage tank v  | volume tables (or dimensions of storage tanks).  |
| Procedure: | The fo | llowing inform  | ation is needed to perform these calculations:   |
|            | 1.     | Obtain          | It received since previous report<br>ed from refinery invoices, truck manifest, weigh ticket,<br>Certificate of Compliance (COC) received at time of<br>Ty |

| 2   |  |
|-----|--|
| 2.  | Tons of lime received since previous report                    |
|     | Obtained from invoices, truck manifest, weigh ticket, and/or   |
|     | Certificate of Compliance (COC) received at time of delivery   |
| 3.  | Tons of asphalt in tanks, obtained from previous report        |
| 4.  | Temperature of each tank at time of tank stab                  |
|     | Recorded from tank at time of tank stab                        |
| 5.  | Specific Gravity at 60 °F                                      |
|     | Obtained from invoices, truck manifest, weigh ticket, and/or   |
|     | Certificate of Compliance (COC) received at time of delivery   |
| 6.  | Depth of asphalt in each tank; this is the tank stab depth     |
| 7.  | Storage tank volume tables                                     |
|     | Maintained by contractor for each specific tank                |
| 8.  | Asphalt Conversion Table in WYDOT 841.0                        |
| 9.  | Standard density of the asphalt, pounds per gallon at 60 °F    |
|     | Obtained from refinery invoices, truck manifest, weigh ticket, |
|     | and/or Certificate of Compliance (COC) received at time of     |
|     | delivery   |
| 10. | Total tons of plant mix produced                               |
|     | Obtained from WYDOT Form E-78                                  |
| 11. | Voided tons of plant mix                                       |
|     | Obtained from WYDOT Form E-78                                  |

### Asphalt

Quantities: The following describes the calculations performed on WYDOT Form E-56 (see the example in this section). WYDOT Form E-56 is a dual use form. First described are instructions for WYDOT Form E-56, Asphalt Report section, followed by the Lime Report section.

# All calculations in the Asphalt Report and Lime Report sections are rounded to the nearest hundredth (0.01). Use these rounded values in all subsequent calculations.

Project Setup: The E-56 is located in CMS under the Tree Structure labeled *Oil and Lime* in the left portion of the CMS window. Add an E-56 in CMS by right-clicking *Oil and Lime* and select *Add Binder*. From the *Binder Type* pull down menu, select the applicable *Binder Type* and select *Save*. Return to the *Oil and Lime* tree and right-click *Add E-56*. Select the *Report Date* for the corresponding date the material was placed. From the *Asphalt Binder* pull down menu, select the applicable binder bid item. From the *Select Lime* pull down menu, select the applicable Hydrated Lime bid item.

Report:

# **Oil Report**

This section will correspond to PG Binder located on the left hand side of the screen under OIL.

- 1. Right-click in the Invoice No. Box and select Add.
- 2. Enter the corresponding Invoice data (Invoice No. & Tons)
- 3. Populate the Balance Left On Last Report
- 4. Populate the *S.G of P.G.A.B* (Enter the Specific Gravity of the P.G.A.B. at 60 °F obtained from the Asphalt Invoice. Enter as many decimal places as are provided by the supplier.)
- 5. Populate the *Inches In Tank* (Use a calibrated measuring stick to measure (stab) the depth of asphalt binder in the storage tank. Measure the height of the asphalt in each tank using a tank stab reading and record in inches to the nearest half inch.)
- 6. Populate the *Temperature* (Enter the temperature of the asphalt in °F at the time of the Tank Stab.)
- 7. Populate *Gallons In Tank* (Enter the volume of asphalt, in gallons, in each storage tank using the storage tank volume tables provided by the contractor.
- 8. Populate *LBS of Oil / Gallon* (Input the weight or standard density of the asphalt binder in lbs/gallon at 60 °F as recorded on the Oil Invoice. Enter to as many decimal places as are provided by the supplier.)
- 9. Populate *Design Oil* % (This value is obtained from the approved mix design)

# Lime Report

This section will correspond to the Hydrated Lime located on the right hand side of the screen under **LIME**.

- 1. Right-click in the Invoice No. Box and select Add.
- 2. Enter the corresponding Invoice data (Invoice No. & Tons)
- 3. Populate the *Balance Left On Last Report*
- 4. Populate the *Ending Lime Reading* in the *Auxiliary* storage in lbs (Auxiliary storage is only to be used if lime is delivered onto the project and is stored in something other than the two storage silos that are available for use on Form E-56. Most mobile operations will not require auxiliary storage. The auxiliary storage is most applicable for locations that have stationary plants.)
- 5. Populate the *Ending Lime Reading in Silo 1 in lbs* (Input the ending LBS of lime for each storage used.)
- 6. Populate the *Ending Lime Reading in Silo 2 in lbs* (Input the ending LBS of lime for each storage used.)
- 7. Populate the % *RAP* (RAP used at the plant (if applicable))
- 8. Populate *Tons of Dry Aggregate Previous* (This value will be taken from the previous E-56 Report, or be 0 on the 1<sup>st</sup> report.)

# Material Produced This Date

- 1. Right-click in the Material Produced This Date Box and select Add.
- 2. From the *Select Bid Item* pull down menu, select the applicable *Bid Item* (*Hot Plant Mix, Hot Plant Mix Leveling, Hot Plant Mix Approaches, etc...*)
- 3. Populate the *Produced* column with the tons of material produced (Input the total tons of material Produced for each type of HPM)
- 4. Populate the *Tons Voided* with the tons of material voided (Input the total tons of material Voided for each type of HPM.)

Note - Be sure to evaluate Subsection 401.5.1 of the Standard Specifications to ensure the approved mix design asphalt binder is within the Materials and Rates tolerance set.

# Remarks

1. Populate *Remarks* (Enter relevant comments or observations such as voided load tickets, material remaining in tanks at beginning of project, samples taken, and any unusual events.)

# **Form Completion**

- 1. Select the *Approved* Check Box
- 2. Select Post to Ledger Button
- 3. Select the *E-56* Button

### WYOMING DEPARTMENT OF TRANSPORTATION

Asphalt and Lime Report

Project # 1804261

Item: 19 - 401.03329 - ASPHALT BINDER (PG 76-28)

Item #: 401.03329

Date: 7/19/2018

Oil Report

#### OIL RECEIVED SINCE LAST REPORT

|               | Invoice No. | Tons       |
|---------------|-------------|------------|
|               | 7-367575    | 38.49      |
| Total Tons Re |             | ort: 38.49 |
|               |             |            |

| Balance Left On Last Report:          | 98.25  |
|---------------------------------------|--------|
| Total Tons On Hand For Use This Date: | 136.74 |

#### REMAINING OIL

S.G OF P.G.A.B. 1032

|                   | TANK 1    | TANK 2   |
|-------------------|-----------|----------|
| Inches in Tank    | 70.00     | 77.00    |
| Temperature       | 318       | 315      |
| Gallons In Tank   | 12924.00  | 10771.00 |
| Temp Corr Factor  | 0.9256    | 0.9265   |
| Gallons @ 60F     | 11,962.45 | 9,979.33 |
| LBS Of Oil/Gallon | 8.6120    | 8.6120   |
| Tons Left In Tank | 51.51     | 42.97    |
|                   |           |          |
|                   |           |          |

#### PAY TONS FOR OIL

| 136.74 |
|--------|
| 94,48  |
| 42.26  |
|        |

#### Item: 23 - 413 01000 - HYDRATED LIME Item #. 413 01000 Report #: 2

#### Lime Report LIME RECEIVED SINCE LAST REPORT

|                 | Invoice         | No.          | Tons    |
|-----------------|-----------------|--------------|---------|
| Total Tons Re   | ceived Since L  | ast Report.  | 0       |
| Ba              | ance Left On L  | ast Report:  | 23.40   |
| Total Tons Or   | Hand For Use    | e This Date: | 23.40   |
| REMAINING LIME  |                 |              | 1.1.1   |
| Ending Lime     | Reading         | LBS          | TONS    |
|                 | Auxiliary       | 33000.00     | 16.50   |
| % RAP           | Silo 1          | 0.00         | 0.00    |
| 15.00 %         | Silo 2          | 0.00         | 0.00    |
|                 | Tons            | Left In Tank | 16.50   |
| PAY TONS FOR LI | ME              |              | P       |
| Tor             | ns of Lime Use  | d This Date  | 6.90    |
| Tons of Ma      | aterial Produce | d This Date  | 1109.97 |
| 1               | ons of Oil Use  | d This Date  | 42.26   |
| Ta              |                 | d This Data  | 00.0    |

| TUIS OF OIL USED THIS Date          | 42.20    |
|-------------------------------------|----------|
| Tons of Lime Used This Date         | 6.90     |
| Tons of RAP Used This Date          | 166.50   |
| Tons of Dry Aggregate This Date     | 894.31   |
| Tons of Dry Aggregate Previous      | 462.46   |
| Total Tons of Dry Aggregate to Date | 1,356.77 |

#### MATERIAL PRODUCED THIS DATE

| Bid Item                                 |         |          | Produced | 1    | Tons Voided | Pay Tons | Pay Factor      | Adj. Amt |
|--|---------|----------|----------|------|-------------|----------|-----------------|----------|
| 17 - 401.03310 - HOT PLANT MIX (RECYCLE) |         | 1,109.97 |          | 3.00 | 1,106.97    | 1.00     | \$0.00          |          |
| Total Tons                               | 1109.97 | 3.00     | 1106.97  |      |             | Aggregat | e and RAP Ratio | 0.81     |

| Percent Oil Added This Date | 3.81 % |
|-----------------------------|--------|

Aggregate and RAP Ratio 0.81 Void Dry Aggregate This Date (Tons) 2.42

# WYOMING DEPARTMENT OF TRANSPORTATION

Asphalt and Lime Report

| Project #, I804261<br>Item: 19 - 401 03329 - ASPHALT BINDER (PG 76-28) |             | Item: 23 - 413.01000 - HYDRATED LIME |        |
|--|-------------|--------------------------------------|--------|
| Item #: 401.03329  |             | Item #: 413.01000                    |        |
| Date: 7/19/2018  | Report #. 2 |                                      |        |
| Design Oil %   | 3.86 %      | Percent Lime Added This Date         | 0.77 % |
| Voided Oil This Date   | 0,11        | Void Lime This Date (Tons)           | 0.02   |
| Total Oil Pay Tons This Date   | 42.15       | Total Lime Pay Tons This Date        | 6.88   |
| Remarks  |             |                                      |        |

Approved 07/20/2018 Approved By MARK JOHNSON

E-56

#### **CORRELATION OF CORE DENSITY RESULTS**

- Scope: This statistical procedure compares the mix (hot plant mix, recycled hot plant mix, warm plant mix) densities determined by WYDOT with those determined by the contractor. A two-tailed paired t-test is run on the core densities determined by the two laboratories. This procedure determines whether one can be 99 percent confident that the two laboratories are achieving different test results. This procedure will not detect minor differences between the two laboratories.
- Use: This procedure determines whether densities determined by WYDOT and the contractor may be used interchangeably. If the data generated by WYDOT and the contractor are found to be significantly different, then the dispute resolution procedure will be followed.

The two-tailed paired t-test determines whether average the core densities are significantly different. The directional bias test indicates if one laboratory is getting consistently higher or lower results than the other.

If there is change in testing personnel or equipment, repeat the correlation process using production test results.

Reference

| Documents: | WYDOT 114     | WYDOT Standard Specifications     |
|------------|---------------|-----------------------------------|
|            | WYDOT 401     | WYDOT Standard Specifications     |
|            | WYDOT 415.0   | Density Testing for Compacted Mix |
|            | WYDOT T-165CD | Correlation of Core Densities     |

Procedure: Collect seven sets of two cores, for a total of fourteen cores according to WYDOT 415.0. Per WYDOT 415.0, assign each pair a label so that pairs sampled together may be compared during the statistical analysis. Seven cores will be tested by WYDOT and the other seven will be tested by the contractor.

Determine the density of each core using WYDOT 415.0. Report the core density values to the nearest  $0.1 \text{ lb/ft}^3$ .

Eliminate outliers. Outliers are those pairs of core densities that are more than two standard deviations away from the mean of the differences.

Perform a two-tailed paired t-test on the density data as described in this section. Use the level of significance,  $\alpha$ , of 0.01.

Evaluate for directional bias. "Directional bias" is considered to exist when all, or all but one of the tests are higher for one laboratory than the other and the average difference exceeds  $0.5 \text{ lb/ft}^3$ . "Directional bias" does not exist when at least two of the tests are less than, or equal to the corresponding paired test, or when the average difference is less than  $0.5 \text{ lb/ft}^3$  when all of the tests are higher for one laboratory than the other.

If any directional bias occurs, or if the t-test indicates that the two laboratories are achieving significantly different results, see Further Evaluation at the end of this section.

Calculations: 1. Calculate the difference between the seven WYDOT densities and the seven contractor densities using the following equation:

$$X_i - Y_i = Z_i$$

| Where: | i =     | individual sample                              |
|--------|---------|--|
|        | $X_i =$ | WYDOT core density for sample p                |
|        | $Y_i =$ | contractor core density for sample pair i      |
|        | $Z_i =$ | difference between paired samples for sample i |

2. Determine the mean (average) of the differences using the following equation:

$$\overline{Z} = \left(\frac{1}{n}\right) \sum_{i=n}^{n} Z_{i}$$

Where:  $\overline{Z}$  = mean (average) sample core density n = number of samples, seven in this case  $\Sigma$  = sum of unit densities

3. Calculate the sample standard deviation<sup>1</sup> of the differences in core densities. This is done using the sample standard deviation function on a calculator or spreadsheet according to the following equation:

$$s = \sqrt{\left(\frac{1}{n-1}\right) \sum_{i=1}^{n} (Z_i - \overline{Z})^2}$$

Where: s = sample standard deviation

<sup>&</sup>lt;sup>1</sup> On most calculators and spreadsheets there are two standard deviations, a population standard deviation and a sample standard deviation: Use the sample standard deviation. To use a calculator, first determine and record the differences,  $Z_i$ . Then calculate the standard deviation of these differences.

4. Eliminate up to one outlying data point. An outlier is defined as any density difference, Z<sub>i</sub>, more than two standard deviations from the mean (average) of the differences.

If  $|Z_i - \overline{Z}| > 2s$  then the i<sup>th</sup> pair of densities is an outlier and is eliminated.

If an outlier is eliminated, repeat numbers 2 and 3, without the discarded outlying density difference, then go to the paired t-test of this section. Do not repeat number 4; only one outlier may be eliminated.

Paired t-test: 1. Select the appropriate value to use for s in calculating the t-test statistic:

If the sample standard deviation calculated in number 3 above is between 0.50 and  $2.00 \text{ lb/ft}^3$ , use the calculated standard deviation.

If the calculated standard deviation is less than 0.50 lb/ft<sup>3</sup>, use  $s = 0.50 \text{ lb/ft}^3$ .

If the calculated standard deviation is greater than 2.00 lb/ft<sup>3</sup>, use s =  $2.00 \text{ lb/ft}^3$ .

2. Calculate the t-test statistic using the following equation:

$$t = \frac{|\overline{Z}|}{\sqrt{\frac{s^2}{n}}}$$

Where: t = t-test statistic

 $|\overline{Z}|$  = absolute value of the mean differences in density for paired samples

- s = standard deviation selected in number 1 of this section (t-tests)
- 3. If t is less than the critical t value<sup>2</sup>,  $t_{crit} = 3.707$ , then the t-test does not indicate a significant difference between the WYDOT, data,  $X_i$ , and the

<sup>&</sup>lt;sup>2</sup> If a different number of samples are correlated, a different  $t_{crit}$  must be selected. A two-tailed t-test statistic must be selected for the appropriate degrees of freedom. For five pairs,  $t_{crit} = 4.604$ ; for six pairs,  $t_{crit} = 4.032$ ; for seven pairs,  $t_{crit} = 3.707$ ; for eight pairs,  $t_{crit} = 3.499$ ; for nine pairs,  $t_{crit} = 3.355$ ; for eleven pairs,  $t_{crit} = 3.169$ ; and for twelve pairs,  $t_{crit} = 3.106$ . The WYDOT Materials Program or a standard statistics textbook may be consulted for assistance.

contractor's data,  $Y_i$ . If an outlier has been eliminated and the paired t-test is performed on six cores, the critical t value changes to  $t_{crit} = 4.032$ .

4. Evaluate for directional bias.

Example: The data on Table 1 of this section is used to perform the example calculations.

- 1. Report the calculations using CMS on the WYDOT Form T-165CD.
- 2. Record the seven bulk specific gravities for both, WYDOT,  $X_i$ , and the contractor,  $Y_i$ .
- 2. Calculate the averages,  $Z_i$ .
- 3. Calculate the standard deviation.
- 4. The seventh data pair is outside the range of -2.45 to 2.63 lb/ft<sup>3</sup> so it is discarded as an outlier.

Table 1: Example Data: Core Densities, lb/ft<sup>3</sup>

Note that only one outlier may be discarded.

| WYDOT, X <sub>i</sub> | Contractor, Y <sub>i</sub>        | Difference, Z <sub>i</sub> |
|-----------------------|-----------------------------------|----------------------------|
| 141.4                 | 140.9                             | 0.5                        |
| 142.3                 | 141.7                             | 0.6                        |
| 140.7                 | 140.8                             | -0.1                       |
| 141.6                 | 141.4                             | 0.2                        |
| 142.1                 | 141.6                             | 0.5                        |
| 141.0                 | 140.4                             | 0.6                        |
| 142.0                 | 144.9                             | <u>-2.9</u>                |
|                       | Mean (average) $(\overline{Z}) =$ | 0.09                       |
| Star                  | ndard Deviation $(s) =$           | 1.27                       |

Since an outlier has been discarded; an average difference of  $0.38 \text{ lb/ft}^3$  and a standard deviation of 0.279 (see Table 2), is calculated.

|                       | Outlier Discarde                  | <u>d</u>                   |  |  |
|-----------------------|-----------------------------------|----------------------------|--|--|
| WYDOT, X <sub>i</sub> | Contractor, $Y_i$                 | Difference, Z <sub>i</sub> |  |  |
| 141.4                 | 140.9                             | 0.5                        |  |  |
| 142.3                 | 141.7                             | 0.6                        |  |  |
| 140.7                 | 140.8                             | -0.1                       |  |  |
| 141.6                 | 141.4                             | 0.2                        |  |  |
| 142.1                 | 141.6                             | 0.5                        |  |  |
| 141.0                 | 140.4                             | 0.6                        |  |  |
|                       | Mean (average) $(\overline{Z}) =$ | 0.38                       |  |  |
| Star                  | ndard Deviation $(s) =$           | 0.279                      |  |  |

Table 2: Example Data: Core Densities, lb/ft<sup>3</sup>

5. Calculate the value of s to determine the t-test statistic.

Since the standard deviation of 0.279  $lb/ft^3$  is less than the minimum standard deviation of 0.50  $lb/ft^3$ , use  $s = 0.50 lb/ft^3$ .

6. Calculate the t-test statistic (see number 2 of Paired t-test).

$$t = \frac{|\overline{Z}|}{\sqrt{\frac{s^2}{n}}} = \frac{|0.38|}{\sqrt{\frac{0.50^2}{6}}} = 1.862$$

Where: t = the t-test statistic.

- 7. The t-test statistic in the example is 1.862. Since one outlier has been eliminated, select the correct critical t value for six pairs. The critical t value is 4.032 (see Note 2). Since the test statistic, 1.862, is less than the critical value, 4.032, conclude that the WYDOT data is not significantly different from the contractor's data. There is a 99 percent confident level that the two data sets represent the same population statistically.
- 8. There is no directional bias since the average difference of the sample pairs is less than  $0.5 \text{ lb/ft}^3$ .

WYDOT 423.0 (Rev. 10-18) Further Evaluation:

- 1. Resolve the discrepancy in accordance with Subsection 114.3.3, *"Correlation"*.
- 2. For Informational Purposes Only:

WYDOT and Contractors swap cores and observe QC testing.

Report: Report the results on Form T-165CD (see examples in this section).

WYDOT 423.0 (Rev. 10-18)



## Wyoming Department of Transportation



#### August 22, 2018 Correlation of Core Densities

| Tester A: Mark Johnson              | Organization A: WYDOT       |  |
|-------------------------------------|-----------------------------|--|
| Tester B: Frankie Adams             | Organization B: Croell, Inc |  |
| Resident Engineer: Steve Cook, P.E. | Contractor: Croell, Inc.    |  |

Testing Date: 7/18/2018

|   |         | Differer            | Outlier?   | ifferences pcf | -      | ensities, po           | 1             | Sample<br>Pair ID |  |
|---|---------|---------------------|------------|----------------|--------|------------------------|---------------|-------------------|--|
|   | emoved) | (Outlier rei        | outine i   | increments put | B      | 1                      | A             | and the second    |  |
|   | 1       |                     | NO         | 1.80           | 51.20  | ) 1                    | 153.0         | 1                 |  |
|   |         |                     | NO         | -1.80          | 53.40  | ) 1                    | 151.6         | 2                 |  |
|   |         |                     | NO         | -2.00          | 50.30  | ) 1                    | 148.3         | 3                 |  |
|   |         |                     | NO         | -1.50          | 52.90  | ) 1                    | 151.4         | 4                 |  |
|   |         |                     | NO         | 0.70           | 50.90  | )   1                  | 151.6         | 5                 |  |
|   |         |                     | NO         | -1.10          | 50.70  | ) 1                    | 149.6         | 6                 |  |
|   |         | 2                   | NO         | -0.50          | 55.50  | ) 1                    | 155.0         | 7                 |  |
| 1 | NA      | Diff:               | Avg        | pcf            | -0.629 | ference:               | Average Dif   |                   |  |
|   | NA      | f Diff:             | SD o       | pcf            | 1.409  | erences:               | tion of Diffe | rd Devia          |  |
|   | NA      | . SD:               | Max        | pcf            | 2.00   | viation:               | Standard D    | ximum             |  |
|   | NA      | . SD:               | Min        | pcf            | 0.5    | viation:               | Standard D    | inimum            |  |
|   | NA      | t <sub>crit</sub> : |            | 1000           | 3.707  | _ t <sub>crit</sub> :_ | 2.190         | *SD:              |  |
|   | NA      | t:                  |            | _              | 1.180  | _ t:_                  | -3.447        | *SD:              |  |
|   | NA      | / Fail:             | Pass       | 100            | Pass   | ss / Fail:             | Pa            |                   |  |
|   | NA      | Bias:               | irectional |                | NO     | al Bias:               | Direction     |                   |  |

Comments:

WYDOT 423.0 (Rev. 10-18)

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WYDOT 423.0 (Rev. 10-17)

#### WYDOT 423.0

T-165CD (3-2000)



# Wyoming Department of Transportation

### September 28, 2017 Correlation of Core Densities

Project No(s): SIB-NHPPI-0901091 & NHPPI-BR-I901118 & ARSCT-I901A01 & ARSCT-N601A02 & STP-E-N601039

Tester A: WYDOT Technician

Organization A: WYDOT

Tester B: Contractor Technician

Organization B: DOWL

Contractor: Reiman Corp & High Country Const., Inc. JV

Resident Engineer: Jerry Buckley, P.E.

Testing Date: 5/16/2017

|              | Sample       | Densiti              | es, pcf                                 | Differences, pcf | Outlier?  | Differe             |        |    |
|--------------|--------------|----------------------|---|------------------|-----------|---------------------|--------|----|
|              | Pair ID      | A                    | В                                       | Concretioned for | Contract. | (Outlier re         | muved) |    |
|              | 36           | 142.50               | 143.60                                  | -1.10            | NO        |                     |        |    |
|              | 37           | 141.20               | 142.70                                  | -1.50            | NO        |                     |        |    |
|              | 38           | 145.20               | 145.80                                  | -0.60            | NO        |                     |        |    |
|              | 39           | 139.10               | 140.20                                  | -1.10            | NO        |                     |        |    |
|              | 40           | 139.60               | 142.00                                  | -2.40            | NO        |                     |        |    |
|              | 41           | 142.10               | 145.20                                  | -3.10            | NO        |                     |        |    |
|              | 42           | 146.70               | 149.50                                  | -2.80            | NO        |                     | 1.1    |    |
|              |              | erage Differen       | - 1 T T T T T T T T T T T T T T T T T T | 3 - 1            |           | g Diff:             | NA     | po |
| Standa       | ard Deviatio | on of Differenc      | es: 0.96                                | 33pcf            | SD (      | of Diff:            | NA     | pc |
| M            | aximum Sta   | andard Deviati       | on: 2.0                                 | 0pcf             | Ma        | x, SD:              | NA     | pc |
| M            | linimum Sta  | andard Deviati       | on: 0.5                                 | 5pcf             | Mi        | in. SD:             | NA     | pc |
| Avg Dif. + 2 | 2*SD: (      | 0.125 t <sub>c</sub> | arit <sup>:</sup> 3.70                  | 07               |           | t <sub>crit</sub> : | NA     | _  |

Pass / Fail:

**Directional Bias:** 

Min. SD: <u>NA</u>pcf t<sub>crit</sub>: <u>NA</u> t: <u>NA</u> Pass / Fail: <u>NA</u> Directional Bias: NA

Comments:

Fail

YES

WYDOT 423.0 (Rev. 10-17)

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#### CONTRACTOR MICROSURFACING MIX DESIGN PROCEDURE

Scope: This procedure describes the method for independent microsurfacing mix designs and establishes the information which is to be reported with a submitted mix design. This procedure applies to all projects which require the Contractor to submit microsurfacing mix designs. A microsurfacing mix design will recommend the "combination" of additives, aggregate, emulsion, mineral filler, and water to produce a mix that will perform under specific traffic (present and future) and environmental conditions (temperature, humidity).

Ensure laboratories performing mix designs meet the requirements of *WYDOT Standard Specifications* Section 114.2 for all applicable AASHTO test methods.

Use: This procedure is to be used for preparation of a mix design by the contractor and for submission on WYDOT Form E-46M (see blank form in this section) to the WYDOT Materials Program for final approval.

#### Reference

| nerenee    |              |  |
|------------|--------------|--|
| Documents: | AASHTO M 85  | Portland Cement  |
|            | AASHTO M 208 | Standard Specification for Cationic Emulsified Asphalt     |
|            | AASHTO M 303 | Lime for Asphalt Mixtures                                  |
|            | AASHTO M 320 | Performance-Graded Asphalt Binder                          |
|            | AASHTO M 332 | Performance-Graded Asphalt Binder Using Multiple Stress    |
|            |              | Creep Recovery (MSCR) Test                                 |
|            | AASHTO R 66  | Standard Practice for Sampling Asphalt Materials           |
|            | AASHTO T 2   | Sampling of Aggregates                                     |
|            | AASHTO T 11  | Materials Finer than 75 µm (No. 200) Sieve in Mineral      |
|            |              | Aggregate  |
|            | AASHTO T 19  | Bulk Density ("Unit Weight") and Voids in Aggregate        |
|            | AASHTO T 27  | Sieve Analysis of Fine and Coarse Aggregates               |
|            | AASHTO T 49  | Penetration of Bituminous Materials                        |
|            | AASHTO T 53  | Softening Point of Bitumen                                 |
|            | AASHTO T 59  | Testing Emulsified Asphalts                                |
|            | AASHTO T 96  | Resistance to Degradation of Small-Size Coarse Aggregate   |
|            |              | by Abrasion and Impact in the Los Angeles Machine          |
|            | AASHTO T 104 | Soundness of Aggregate by Use of Sodium Sulfate or         |
|            |              | Magnesium Sulfate  |
|            | AASHTO T 112 | Clay Lumps and Friable Particles in Aggregate              |
|            | AASHTO T 176 | Plastic Fines in Graded Aggregates and Soils by Use of the |
|            |              | Sand Equivalent Test                                       |
|            | AASHTO T 313 | Determining the Flexural Creep Stiffness of Asphalt Binder |
|            |              | Using the Bending Beam Rheometer (BBR)                     |
|            |              |  |

| AASHTO T 315  | Determining the Rheological Properties of Asphalt Binder  |
|---------------|---|
|               | Using a Dynamic Shear Rheometer (DSR)                     |
| AASHTO T 316  | Viscosity Determination of Asphalt Binder Using           |
|               | Rotational Viscometer                                     |
| AASHTO T 350  | Multiple Stress Creep Recovery (MSCR) Test of Asphalt     |
|               | Binder Using a Dynamic Shear Rheometer (DSR)              |
| ASTM C 29     | Standard Test Method for Bulk Density ("Unit Weight")     |
|               | and Voids in Aggregate                                    |
| ASTM D 6372   | Standard Practice for Design, Testing and Construction of |
|               | Micro-Surfacing   |
| ISSA A143     | Recommended Performance Guideline for Micro Surfacing     |
| ISSA TB147    | Test Methods for Measurement of Stability and Resistance  |
|               | to Compaction, Vertical and Lateral Displacement of       |
|               | Multi-layered Fine Aggregate Cold Mixes - Method A        |
| WYDOT 114.2   | WYDOT Standard Specifications                             |
| WYDOT 410.2   | WYDOT Standard Specifications                             |
| WYDOT 410.4.5 | WYDOT Standard Specifications                             |
| WYDOT 801.1.1 | WYDOT Standard Specifications                             |
| WYDOT 803.6.2 | WYDOT Standard Specifications                             |
| WYDOT 803.7   | WYDOT Standard Specifications                             |
| WYDOT 804.1   | WYDOT Standard Specifications                             |
| WYDOT 804.3   | WYDOT Standard Specifications                             |
| WYDOT 814.1.1 | WYDOT Standard Specifications                             |
| WYDOT 820.1   | WYDOT Standard Specifications                             |
| WYDOT 832.0   | Deleterious Substances In Portland Cement Concrete        |
| WYDOT E-46M   | Microsurfacing Mix Design                                 |
|               |   |

- Procedure: Optimize the following characteristics in the microsurfacing mix design:
  - Mixability Ensure the aggregate, control additives, emulsified asphalt, mineral filler, and water mix together forming a homogeneous, free-flowing, uniformly coated surfacing material applied in a continuous fashion to roadway surface using the microsurfacing equipment.
  - Workability Ensure the applied mixture sets to a rain-safe condition quickly without segregation, raveling, displacement, or flushing. Ensure the mixture cures in a controlled manner within a reasonably defined time period providing sufficient coating on aggregate and allowing return of traffic.

Performance – Ensure the mixture resists traffic-induced stresses, maintains satisfactory friction resistance, does not ravel, de-bond, bleed, exhibit moisture damage, or lose cohesiveness over the life of the treatment.

Perform the mix design according to the standard industry practice. Recommended method is described in International Slurry Surfacing Association (ISSA) Technical Bulletins (TB), *"Recommended Performance Guideline For Micro Surfacing"* A143 (Section 5.2), and ASTM D 6372, International Standard Practice for Design, Testing, and Construction of Micro-Surfacing.

For materials selection, provide quality components in the mixture as follows:

- Aggregate Conform to requirements of Subsection 803.7, Aggregate for Microsurfacing, and if applicable, Subsection 803.6.2, Polish Resistant Aggregate. Ensure compatibility of aggregate with emulsified asphalt and provide all criteria used to establish, and test data to verify, compatibility of aggregate and emulsified asphalt. Ensure job mix formula (JMF) complies with requirements of Subsection 410.4.5.
- Asphalt Conform to requirements for CQS-1HP emulsified asphalt per Subsections 410.2, Materials, and 804.3, Emulsified Asphalt, Table 804.3-1.

Emulsified

- Mineral Filler Conform to requirements of Subsection 801.1.1 for Portland Cement, and Subsection 820.1 for hydrated lime.
- Water Ensure use of potable water free of harmful salts and contaminants conforming to requirements of Subsection 814.1.1.

Determine minimum emulsion content, determine minimum residual asphalt content by total weight of dry aggregate, verify that mix and set times are appropriate for the climatic conditions expected during the project, and report quantitative effects of moisture content on the unit weight of the aggregate (bulking effect) according to AASHTO T 19 (ASTM C 29).

Ensure base asphalt binder for emulsified asphalt complies with requirements specified in Subsection 804.1, Performance Graded Asphalt Binder, and has a  $J_{nr3.2}$  of 4.0 kPa<sup>-1</sup> or less per Table 1 in AASHTO M 332. To do so, determine the pavement climatic high temperature (per current LTPPBind software, >90% reliability, and no 'grade-bumping') and perform Multiple Stress Creep Recovery testing per AASHTO T 350 on distillation residue only, not RTFO residue.

For the completed mix design, test every property at the minimum emulsion content to ensure all properties in Table 410.4.5-2, Testing Requirements, meet specifications. Include in the mix design the aggregate proportions, the recommended minimum polymer-modified emulsified asphalt content, recommended mineral filler content, water rate, and other additives to control mix set times and cohesion properties.

For Test Procedure ISSA TB147 (ASTM D 6372), after compacting and removing the specimen from the loaded wheel track machine, immediately remeasure the specimen both laterally and vertically in the wheel path and record the results. Calculate the lateral displacement as the percent increase of the original width. Calculate the vertical displacement as the percent decrease of the original net thickness. Ensure the vertical displacement is no greater than 15%.

General: Report the mix design information on WYDOT Form E-46M (see blank form in this section) and include the following:

Aggregate Information, both coarse and fine;

Dry Weight and SSD Weight Aggregate Gradation and JMF with JMF units Specific Gravity (SSD) Absorption Magnesium Sulfate Loss per AASHTO T 104 Source Location

For Coarse Aggregate, also include;

Percentage of Wear per AASHTO T 96

For Fine Aggregate, also include;

Fineness Modulus Colorimetric (See WYDOT 832.0)

**Emulsified Asphalt Information;** 

Minimum residual asphalt content by total weight of dry aggregate Residual asphalt PG grade (e.g., PG58-28) Residual asphalt  $J_{nr3.2}$  at pavement climatic high temperature Minimum emulsion content Emulsion grade (e.g., CQS-1HP) Emulsion supplier Minimum polymer content by percent solids of residual asphalt weight content Polymer type (i.e., SBS, etc)

Additives Information;

Percent content Type Supplier

Mineral Filler Information;

Percent by total weight of dry aggregate Type (i.e., Portland Cement, hydrated lime) Supplier

Water Information;

Moisture content, % Source

Mixture Properties;

Wet Track Abrasion, One Hour Loss, maximum Wet Track Abrasion, 6 Day Soak Loss, maximum Excess Asphalt by LWT Sand Adhesion, maximum Mix Time @ 77 °F, minimum Wet Stripping, minimum Wet Cohesion @ 30 minutes (set), minimum Wet Cohesion @ 60 minutes (traffic), minimum or Near Spin Classification Compatibility, minimum grade points Lateral Displacement, maximum Vertical Displacement, maximum Specific Gravity after 1,000 cycles of 125 lb, maximum

#### WYOMING DEPARTMENT OF TRANSPORTATION MICROSURFACING MIX DESIGN (Including JMF)

|                    | t Name<br>ngineer | ERP No   | ame<br>er's Name  | =                        | Contractor                     | XX/XX/XXXX<br>Company Name<br>Company Name          |
|--------------------|-------------------|----------|---|--------------------------|--------------------------------|---|
| SIE VE :           | SIZE              |          | AVG.GRADATION 60 % OF<br>TOTAL ITEM<br>CRUSHED TO DATE  | JOB MIX<br>FORMULA (JMF) | TOLERANCE<br>(GRADING<br>BAND) | WIDE BAND   |
| 3/8 in ch          | (9.5 m            | m)       | 100   | 100                      | 100                            | 100   |
| No. 4              | (4.75 n           | nm)      | 77  | 77                       | 72-82                          | 70 to 90  |
| No. 8              | (2.36 n           | nm)      | 49  | 49                       | 45-55                          | 45 to 70  |
| No. 16             | (1.18 n           | nm)      | 35  | 35                       | 30-40                          | 28 to 50  |
| No. 30             | (0.60 n           | nm)      | 26  | 26                       | 21-31                          | 19 to 34  |
| No. 50             | (0.30 n           | nm)      | 20  | 20                       | 16-24                          | 12 to 25  |
| No. 100            | (150 µ            | m)       | 13  | 13                       | 10-16                          | 7 to 18   |
| No. 200            | (75 µm            | 1)       | 7.6   | 7.6                      | 5.6-9.6                        | 5 to 15   |
| The virgin materia | ul was co<br>%    |          | at percentages (%) as follows:<br>REGATE<br>SOURCE  | FRACTURED<br>FACES, %/ % | P OL ISH<br>Resistant, Y/N     | SOUNDNE SS (Mg SO↓),<br>%Less                       |
| 1                  | 28                | Max      | Pit Name  | 100/95                   | У                              | 25 max  |
| 2                  | 14                | Wax      | Pit Name  | 95/90                    | У                              | 25 max  |
| Э                  | 58                | Max      | Pit Name  | 100/95                   | У                              | 25 max  |
| 0.00 0.0           |                   |          | 11.01 N22 K24   |                          |                                |   |
| Conter             | ŕ                 |          | Supplier or Source  | Grade / Type             | J <sub>nr32</sub>              | Comments  |
| Emulsion           | 1                 | ,min.    |   | CQS-1HP                  | 000200                         |   |
| Residual Asphalt   | 2 - 1989.)<br>1   | 7 ,min.  |   | PG58-28                  | ≤ 4                            | PVMT climate hitemp. 58° c.                         |
| Polymer            |                   | Э,min.   |   | SBS                      |                                |   |
| P ortl andC ement  | 110               | ± 1      |   |                          | (*****)                        |   |
| Hydrated Lime      | 1.5               | ± 1      |   |                          |                                | 0   |
| Additive           | 100200101         | max      |   |                          | 100000                         |   |
| Water              | 9                 | ± 3      |   |                          | 01200%                         |   |
| TestProcedure      |                   |          | Description   | Value                    |                                | Specification                                       |
| SSA TB100          | Wet Tr            | ack Abra | ision, One Hr. Loss   | 3                        | g/ft <sup>2</sup>              | 50 g/ft <sup>2</sup> max.                           |
|                    |                   |          | ision, 6 Day Soak Loss  | 5                        | g/ft <sup>2</sup>              | 75 g/ft <sup>2</sup> max.                           |
| SA TB109           |                   |          | by LWT Sand Adhesion  | 10                       | g/ft <sup>2</sup>              | 50 g/ft <sup>2</sup> max.                           |
| SSA TB113          |                   | me @ 77  | na et 🖌 de la casa de la casa de la casa de casa de la | 185                      | sec.                           | 120 sec. Min.                                       |
| SATB114            |                   | ripping  |   | 90 +                     | %                              | 90% min.  |
| SSA TB139          |                   |          | Ø 30 min (set)  | 15                       | kg-in                          | 31 kg-in min.                                       |
|                    |                   |          | 2, 60 min (traffic)   | 21                       | kg-in                          | 51 kg-in min. or Near Spin                          |
| SSA TB144          |                   |          | ompatibility  | BAA (A=4,B=3             | Children and an and            | 그렇게 잘 많다. 그렇게 같은 것은 것이 같아요. 말을 가지 않는 것이 같아요. 것을 많다. |
|                    |                   |          |   |                          |                                | adhesion), abrasion loss < 3                        |
| SSA TB147          | Lateral           | Displace | ement   | 2                        | %                              | 5% max.   |
|                    |                   | l Displa |   | 10                       | %                              | 15% max.  |
|                    |                   |          | Cycles of 125 lbs   | 1.95                     | - T                            | 2.10 max.   |

| Proposed Paving Date: |             |    |
|-----------------------|-------------|----|
| <u>b</u>              | Signatures  |    |
| Supplier:             | Paving Sub: |    |
| Email                 | Email:      | 73 |
| Phone #:              | Phone #     |    |
| Date:                 | Date:       |    |
|                       | Resident    |    |
| Prime Contractor:     | Engineer    |    |
| Email:                | Email:      |    |
| Phone #:              | Phone #     |    |
| Date:                 | Date:       |    |

#### WYDOT CONCRETE MIX DESIGN PROCEDURE

Scope: This procedure documents the requirements for obtaining a concrete mix design or referencing an approved mix design from the WYDOT Materials Program, and the amounts of concrete aggregate, cementitious material, and admixtures that are to be submitted. It also addresses the procedure for developing and obtaining approval for a silica fume concrete mix design.

This procedure applies to all concrete placed separate from Quality Control/Quality Assurance specifications.

Use: This procedure will be used to determine the steps to follow and the amounts of concrete constituents (including aggregate, cement, fly ash, silica fume, chemical admixtures, etc) that must be collected and submitted to the WYDOT Materials Program for the purpose of running a mix design or conducting test batches.

Reference

| WYDOT 472.0 | Contractor Concrete Mix Design Procedure |
|-------------|--|
| WYDOT 816.0 | Sieve Analysis of Concrete Aggregate     |
| WYDOT E-45  | Concrete Mix Design                      |
| WYDOT T-100 | Report of Tests on Concrete Mix Designs  |
| WYDOT T-120 | Sample Transmittal                       |
|             | WYDOT 816.0<br>WYDOT E-45<br>WYDOT T-100 |

Procedure: Check the plans to determine the classes of concrete and types of cement called for. A mix design will be required for each different class of concrete, including modified mixes, for each type or source of cement used on the project, or for any change in admixtures. For each mix design, a WYDOT Form E-45 will be completed by the contractor or supplier, sent through the WYDOT engineer, and finally forwarded to the WYDOT Materials Program, a minimum of 35 days before concrete placement. Concrete placement may begin on receipt of the T-100 from the Materials Program.

Run a gradation test on the coarse and fine aggregate using the procedure outlined in WYDOT 816.0 *Sieve Analysis of Concrete Aggregate* before the material is sent to the WYDOT Materials Program. A mix design will not be performed on out of specification material.

Submit all mix designs through the Resident Engineer's office for proper processing prior to being sent to the Materials Program. A mix design will not be performed on out of specification material.

Along with the Form E-45, and the necessary Form T-120 for each material submittal, submit the following quantities of materials to the WYDOT Materials Program for the appropriate mix designs:

Submit ALL aggregate samples in standard canvas bags, 30 lb - 50 lb in each bag. For liquid admixtures submit 1 quart of each type.

Structural Concrete Aggregate:

600 lb of coarse aggregate

400 lb of fine aggregate

For each additional mix design on the same project from the same source, send 270 lb of coarse aggregate and 200 lb of fine aggregate that will be needed for each mix design. Aggregate samples will be sent to the WYDOT Materials Program a minimum of 35 days prior to construction intended use.

#### P.C.C.P Aggregate:

775 lb of coarse aggregate

600 lb of fine aggregate

For each mix design on Portland Cement Concrete Pavement (PCCP) mix design.

Representative samples of coarse and fine aggregate should be sent to the WYDOT Materials Program as soon as possible and a minimum of 35 days before the aggregate will be used in construction.

> The samples sent in for mix designs are not check samples and cannot be used as such. Check samples are taken only during production.

#### Fly Ash:

When fly ash is to be used in the concrete mix design, a fly ash sample should be taken for the project. Send 50 lb of fly ash and ship it in plastic bucket(s) or container(s).

Record on Form T-120 the class of fly ash used, the manufacturer's name, and the invoice number if possible. It will not be necessary to record the contractor's name or the name of the ready mix company.

#### Portland Cement:

A Portland Cement sample should be taken for each source and type of cement used on the project. The sample must be free of any soil or rocks. Send 140 lb of cement and ship it in plastic bucket(s) or container(s). A Portland Cement sample should be taken for each source and type of cement used on the project.

Record on Form T-120 the type of cement used, the manufacturer's name, and the invoice number if possible. It will not be necessary to record the contractor's name or the name of the ready mix company.

Silica Fume:

A silica fume concrete mix design must be developed by the contractor with the aid of an admixture manufacturer prior to requesting mix design approval from the WYDOT Materials Program. Batching proportions and batching sequence must be determined by this process. Results of this mix development will be submitted to the WYDOT Materials Program when requesting mix design approval. A Laboratory test mix will be conducted by the WYDOT Materials Program utilizing these instructions. If the proposed mix design does not provide a satisfactory mix, as determined by WYDOT Materials Program, the contractor must resubmit a revised mix design. The contractor will provide the following items to the WYDOT engineer at least 30 days prior to placement:

- 1. A completed Form E-45 indicating all materials to be used, including the manufacturer and source for all materials.
- 2. A letter indicating proportions of all materials, including water. The aggregate proportions will indicate whether they are saturated, surface dry condition or dry condition. Total or net water will also be indicated as appropriate based on aggregate condition.
- 3. An equipment letter indicating the mixing equipment to be used.
- 4. A batch sequence letter indicating the sequence of material batching and mixing times.
- 5. Submit sufficient samples of all mix constituents so that a test mix may be batched at the WYDOT Materials Program.

Sufficient samples will be a minimum of:

100 lb of cement
400 lb of coarse aggregate
300 lb of fine aggregate
25 lb of silica fume
1 lb of fibers
1 quart each of all liquid or dry admixtures

(which includes normal and high-range water reducers and air-entraining admixture).

No more than two mix designs for each placement location will be batched by the WYDOT Materials Program at no cost to the contractor. The contractor will be charged a fee for each additional mix design confirmation.

The contractor must conduct a trial batch prior to placement to verify in-field conditions, utilizing stockpiled aggregate as proposed for the project and simulating proposed haul distance. Trial batch material may not be used in the resurfacing work.

Referencing Mix Designs:

If a proposed mix design is composed of identical components to a previous mix design, the previous mix may be referenced if less than two years old. In such cases, aggregate analysis only will be required. Send 100 lb of coarse aggregate and 100 lb of fine aggregate along with Form E-45 showing all mix design components to the WYDOT Materials Program for testing.

For silica fume concrete, referencing to avoid the laboratory test mix will only be allowed within one year of use. The on-site trial batch will always be required.

Mix Design Approval:

The WYDOT Materials Program will determine acceptability of all mix designs and reference designs upon determination of mixture properties and strength development trends. Upon approval, a copy of Form T-100PE or Form T-100SE (see example forms in WYDOT 472.0), with the mix design proportions used, mix consistency results, and strength results, will be forwarded to the WYDOT engineer. Concrete placement may begin upon receipt of Form T-100PE, or Form T-100SE.

#### WYOMING DEPARTMENT OF TRANSPORTATION CONCRETE MIX DESIGN

E-45 (Rev. 09-16)

| DEPARTMENT          |                  |                |                  |                           |                                     |               |            |  |  |
|---------------------|------------------|----------------|------------------|---------------------------|-------------------------------------|---------------|------------|--|--|
| Project Number:     | ERP Project I    | Number         |                  | Date Submitted:           | XX/XX/XX                            | x             |            |  |  |
| Project Name:       | Project Nam      | e or Locatior  | i                | Supplier:                 | n Supplier's Name<br>n Company Name |               |            |  |  |
| Resident Engineer:  | Resident Eng     | ineer's Nam    | e                | Contractor:               |                                     |               |            |  |  |
| Engineer's Town:    | Engineer's T     | own            |                  | Batch Plant Location:     | Town                                |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
|                     | mix design for   | 04 - 241-020   |                  |                           |                                     |               | - concrete |  |  |
|                     | to be used for   |                |                  |                           | 1                                   |               | is         |  |  |
|                     | hereby requeste  | ed. The follow | ing materials ar | e proposed for use in the | above mix.                          |               |            |  |  |
| Cement:             | Type:            | I-II           |                  | Supplier/Manufacturer:    | Holeim (Trie                        | dent Plant)   |            |  |  |
| Fly Ash:            | Class:           | Р              |                  | Source:                   | Craig                               |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
| Admixtures:         | aining Supplier/ | Manufacturor   | Maeter Build     | one                       | Trade Name:                         | Micro - Air   |            |  |  |
|                     | ducing Supplier/ |                |                  | 8                         | -                                   | Pozzolith 322 |            |  |  |
| Water 16            | aacing sappners  | Manufacturer.  | Muster Duna      |                           | - Traue Maine.                      | TOZZONIH SEE  |            |  |  |
| Other Additives (sp | ecify):          |                |                  |                           |                                     |               |            |  |  |
| 000                 | - 545            | Manufacturer:  |                  |                           | Trade Name:                         |               |            |  |  |
|                     | Supplier/        | Manufacturer:  |                  |                           | -<br>Trade Name:                    | 5             |            |  |  |
|                     | Supplier/        | Manufacturer:  |                  |                           | -<br>Trade Name:                    |               |            |  |  |
|                     | Supplier/        | Manufacturer:  |                  |                           | Trade Name:                         | 1             |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
| Aggregates:         |                  |                |                  |                           |                                     |               |            |  |  |
| Coarse:             | Specification:   |                |                  |                           | Source (Pit):                       | Pit Name      |            |  |  |
|                     | Location:        | Location of    | f Pit            |                           | _                                   |               |            |  |  |
| Fine:               | Specification:   |                |                  |                           | Source (Pit):                       | Pit Name      |            |  |  |
|                     | Location:        | Location o     | f Pit            |                           | _                                   |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
|                     | First antic      | ipated date of | concrete use:    |                           |                                     |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
| Remarks:            |                  |                |                  |                           |                                     |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |
|                     |                  |                | Si               | gnatur es:                |                                     |               |            |  |  |
| Supplier:           |                  |                |                  | Concrete Sub:             | 5                                   |               |            |  |  |
| Email:              |                  |                |                  | Em ail:                   |                                     |               |            |  |  |
| Phone #:            |                  |                |                  | Phone #:                  |                                     |               |            |  |  |
| Date:               |                  |                |                  | Date:                     |                                     |               |            |  |  |
|                     | 40.              |                |                  |                           | с.<br>                              |               |            |  |  |
| Prime Contractor:   |                  |                |                  | Resident Engineer:        |                                     |               |            |  |  |
| Email:              |                  |                |                  | Em ail:                   |                                     |               |            |  |  |
| Phone #:            |                  |                |                  | Phone #:                  |                                     |               |            |  |  |
| Date:               |                  |                |                  | Date:                     |                                     |               |            |  |  |
|                     |                  |                |                  |                           |                                     |               |            |  |  |

#### WYOMING TRANSPORTATION DEPARTMENT MATERIALS BRANCH REPORT OF TESTS ON CONCRETE MIX DESIGNS

T-100 (Rev. 05-04)

#### cc: Quinn

|                   | Laboratory No.:<br>Date Sampled:<br>Engineer:<br>Source (CA):<br>Source (FA):<br>Field No. (CA):<br>Field No. (FA):<br>Class Concrete:   | 2016-043<br>2/23/16<br>SHENEFE<br>GRANITE<br>LUMMIS<br>CA<br>FA<br>CLASS "B | CAYON<br>PIT  |            | - Kerper            | M                 | Date Receiv<br>Date Tested<br>Location:<br>Location (C<br>Location (F<br>Project No.<br>Date Mix R<br>Saved As:<br>REGATE | l:<br>CA):<br>CA):<br>:<br>un: | 2/25/16<br>2/26/16<br>CHEYENI<br>HARRIM.<br>CHEYENI<br>STP-PM-E<br>3/9/16<br>STP-PM-E | AN, WY.<br>NE, WY.<br>3161007<br>3161007 |                          | AGGREC | s. Quini |
|-------------------|--|---|---------------|------------|---------------------|-------------------|---|--------------------------------|---|--|--------------------------|--------|----------|
| TEST              | -  |   | 1             | REGATE     |                     | The second second |   |                                |   |  |                          |        |          |
| METHOD            |  | WT RET  | SPECS         | %PASSING   | WTRET               | SPECS             | %PASSING  | WT RET                         | SPECS   | %PASSING<br>100                          | WT RET                   | SPECS  | %PASSING |
| AASHTO            | 1 1/2" (37.5 mm)   |   | 100<br>95-100 | 100        | -                   | -                 |   |                                |   | 100                                      |                          |        |          |
|                   | 1" (25.0 mm)<br>3/4" (19.0 mm)   |   | 95-100        | 94         | -                   |                   | -   | _                              | 1   | 100                                      |                          | -      |          |
|                   | 3/4" (19.0 mm)<br>1/2" (12.5 mm)   |   | 25-60         | 48         |                     | -                 | -   |                                | ×   | 100                                      | -                        | -      |          |
|                   | 3/8" (9.5 mm)  | -   | 20-60         | 26         |                     |                   |   | _                              | 100   | 100                                      |                          | -      |          |
|                   | 3. F   |   | 0.10          |            |                     | -                 |   | _                              |   | 99                                       |                          | -      |          |
| <b>T-2</b> 7      | #4 (4.75 mm)   |   | 0-10          | 8          | _                   | ×                 |   |                                | 95-100  |  |                          | -      | -        |
|                   | #8 (2.36 mm)   |   | 0-5           | 5          |                     | -                 | 1   |                                | 45-80   | 89                                       |                          | -      |          |
|                   | #16 (1.18 mm)  |   | -             |            |                     | -                 |   |                                | 45-80   | 66                                       |                          | -      |          |
|                   | #30 (0.600 mm)   |   | -             | 3          |                     | -                 |   |                                | 10.00   | 40                                       | -                        | -      |          |
|                   | #50 (0.300 mm)   |   |               | 3          |                     |                   | -   |                                | 10-30   | 17                                       |                          | -      |          |
|                   | #100 (0.150 mm)  |   | 1.0.2         | 2          |                     |                   |   |                                | 2-10  | 5  |                          |        |          |
| _                 | #200 (0.075 mm)  | -   | 0-2           | 1.6        |                     | -                 | -   |                                | 0-4   | 1.7                                      |                          | -      |          |
| T-27              | FINENESS MODULUS:  |   |               |            |                     | -                 |   | _                              | -   | 2.84                                     |                          |        | -        |
| 1                 | SPECIFIC GRAVITY:  | 2.748   |               | -          | -                   | -                 |   | 2.633                          | -   | 2.04                                     |                          | -      |          |
| T-85,T-84<br>T-21 | COLORIMETRIC:  | 2.748   |               | -          |                     | -                 |   | CLEAR                          | 1   |  | -                        |        | -        |
|                   |  | 074   | -             |            |                     |                   |   |                                |   | 1  |                          |        |          |
| T-85,T-84         | ABSORPTION:  | 0.746   | (%)           |            | -                   | (%)               | 1   | 0.604                          | (%)   |  | -                        | (%)    |          |
| T-96              | ABRASION:<br>SODIUM SULPHATE:  | "B" 24.9<br>0.179   | (%)           |            |                     | (%)               |   | 0.847                          | (%)   |  |                          | (%)    |          |
| T-104             | A DESCRIPTION OF THE PARTY OF T | 0.179   | (%)           | alass      | "B"                 | (%)               |   | 0.847                          | (%)   |  |                          | (%)    | 1-       |
|                   | CONCRETE DESIGN:   |   |               |            |                     | I-II              |   |                                |   |  |                          |        |          |
|                   | CONCRETE DESIGN CEM  |   |               | MOUNTAIN   |                     | 268               | 1004  |                                |   |  |                          |        |          |
|                   | CEMENT: MOUNTAIN   |   |               | 451<br>113 | LBS/CY              |                   | kg/m3   |                                |   |  |                          |        |          |
|                   | FLY ASH: JEWETTE "   | ŀ   | -             |            | LBS/CY              | 67                | kg/m3   |                                |   |  |                          |        |          |
|                   | FINE AGGREGATE:  |   | DRY           | 1178       | LBS/CY              | 699               | kg/m3   | h.                             |   |  |                          |        |          |
|                   | COARSE AGGREGATE:  |   | DRY           | 1921       | LBS/CY              | 1140              | kg/m3   |                                |   |  |                          |        |          |
|                   | TOTAL WATER:   |   |               | 32.3       | GAL/CY              | 160.              | L/m3  |                                |   |  |                          |        |          |
| 5.0.A.            | NET WATER:   |   | -             | 248        | LBS/CY              | 147               | kg/m3   |                                |   |  |                          |        |          |
| T-119             | SLUMP:   | Same da Paralana  |               | 2.50       | INCHES              | 64                | mm  | -                              |   |  |                          | -      |          |
| T-152             | BRAND & % AIR :  | VR10 MBVR   |               | 4.7        | PERCENT             | 4.7               | PERCENT   | N                              | 7   |  | 7                        |        | TT       |
|                   | WATER/CEMENT RATIO:  |   |               |            |                     | 0.440             |   |                                |   |  |                          | /      |          |
| A                 | W/CEMENT & FLY ASH R.  |   | _             | 0.440      | a a manufactor anos | 1.000.00.000      |   |                                |   |  |                          |        |          |
| T-121             | UNIT WT FRESH CONCRE   |   |               | 144.7      | LBS/CUFT            | 2320              | kg/m3   |                                | X K   | and Split Cone to                        |                          | Shear  | Columpar |
|                   | ADMIX: POLYHEED  | 997   |               | 13 OZ.     | 100# CEM            | 848mls            |   | A                              | Cone  | B i                                      |                          | D      | E        |
|                   | ADMIX:   |   |               |            | 100# CEM            | -                 | 100 kg CEM  | -                              |   |  |                          |        |          |
|                   | ADMIX:   |   |               |            | 100# CEM            | -                 | 100 kg CEM  |                                |   |  | TO F                     |        |          |
|                   | ADMIX:   |   |               |            | LBS/CY              | -                 | kg/m3   | · · · · ·                      | TY  | PE FRACTI                                |                          | 5      |          |
| T-22              | CYLINDERS:   |   | 0.022         |            | 252                 |                   | 200   |                                | 1   | FRACTURE                                 | Contraction and a second | -      |          |
|                   | 5 Days   | Cyl   | 3660          | 3480       | P.S.I.              | 24.0              | MPa   |                                |   | D  | D                        | DS     |          |
|                   | 7 Days   | Cyl   | 3750          | 3750       | P.S.I.              | 25.9              | MPa   |                                |   | D  | D                        | DS     |          |
|                   | 14 Days  | Cyl   | 4440          | 4500       | P.S.I.              | 31.0              | MPa   |                                |   | D  | D                        | CF     |          |
|                   | 28 Days  | Cyl   | 4960          | 5260       | P.S.I.              | 36.3              | MPa   | -                              | -   | D  | D                        | DS     |          |
|                   | 28 Days  | Cyl   |               | 5250       | P.S.I.              | 36.2              | MPa   |                                |   |  | D                        | DS     |          |
|                   | 28 Days  | Cyl   |               | 5360       | P.S.I.              | 37.0              | MPa   |                                |   |  | D                        | DS     | 1        |

Remarks

THIS MATERIAL MEETS SPECIFICATIONS

DESIGN PHONED OR FAXED: GREG MILBURN, P.E.

STATE MATERIALS ENGINEER

TESTED BY: REVIEWED BY: TQ, CF, DS

C. ROMO, P.E.

MATERIALS ENGINEER

#### **CONTRACTOR CONCRETE MIX DESIGN PROCEDURE**

Scope: This procedure describes required mix design procedures for independent concrete mix designs and establishes the information which is to be reported with a submitted mix design. This procedure applies to Quality Control / Quality Assurance (QC / QA) projects which require the Contractor to submit concrete mix designs.

Ensure laboratories performing mix designs meet the requirements of WYDOT Standard Specifications.

Use: This procedure is to be used for preparation of a mix design by the contractor and for submission of a contractor's mix design. Submit information on a WYDOT Form E-45 (see example form in WYDOT 471.0 section) to the WYDOT Materials Program for final approval.

Reference

| Documents: | ASTM C39/C39M   | Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens |
|------------|-----------------|---|
|            | ASTM C131/C131M | Standard Test Method for Resistance to Degradation of                           |
|            |                 | Small-Size Coarse Aggregate by Abrasion and Impact in                           |
|            |                 | the Los Angeles Machine   |
|            | ASTM C88        | Standard Test Method for Soundness of Aggregate by                              |
|            |                 | Use of Sodium Sulfate or Magnesium Sulfate                                      |
|            | WYDOT           | Current WYDOT Standard Specifications *   |
|            | WYDOT 471.0     | WYDOT Concrete Mix Design Procedure   |
|            | WYDOT 475.0     | Correlation of Compressive Strength to Flexural Strength                        |
|            | WYDOT 476.0     | Allowable Range of Mix Design Strength Results                                  |
|            | WYDOT 832.0     | Deleterious Substances in Portland Cement Concrete                              |
|            | WYDOT E-45      | Concrete Mix Design   |
|            | WYDOT T-100SE   | Structural Concrete Pavement Mix Design   |
|            | WYDOT T-100PE   | Portland Cement Concrete Pavement Mix Design                                    |
|            |                 |   |

♦ Refer to "For All Concrete Sections" notation in Table of Contents – 400 Pavements.

Procedure: The concrete mix design will be conducted according to industry common practice. The mix design process will include a trial batch. The trial batch may be done in either a laboratory mixer or a field production mixer.

WYDOT 472.0 (Rev. 10-18) Structural Concrete:

The mix design will meet the requirements of *WYDOT Standard Specifications* and any additional requirements shown in the contract. The mix design information will be reported on WYDOT Form T-100SE. This procedure is to be used for preparation of a mix design by the contractor and for submission of a contractor's mix design. Submit information on a WYDOT Form E-45 (see example form in WYDOT 471.0 section) to the WYDOT Materials Program for final approval.

The mix design results will include a minimum of three 28 day compressive strength results. The "laboratory mix design strength" will be defined as the mean of the 28 day compressive strength results.

Portland Cement Concrete Pavement:

The mix design will meet the requirements of *WYDOT Standard Specifications* and any additional requirements shown in the contract. The mix design information will be reported on WYDOT Form T-100PE (see example form in this section).

The mix design results will include a minimum of three 28 day compressive strength results and three 28 day flexural strength. The design flexural strength will be defined as the average of the 28 day flexural strength results, unless modifications are indicated in the contract. The range of the mix design strength values will meet the limits as specified in WYDOT 476.0.

A compressive strength to flexural strength correlation constant will be calculated according to WYDOT 475.0 and reported on WYDOT Form T-100PE. This constant will be used for calculating flexural strength based on field collected compressive strength cylinders.

General: Suppliers should contact their admixture product sales representative for specific mix design recommendations. Current WYDOT specifications allow a maximum of 0.45 water-to-cementitious materials (w/cm) ratio. In order to achieve workable mixes, normal range water reducers alone may not perform adequately. Water reducers are listed in WYDOT 111.0 as normal range (NRWR), mid-range (MRWR), and high-range (HRWR).

With the exception of accelerators, on-site admixtures are not required as part of the mix design trial batch. However, the mix design information will include the information listed following under *Admixtures* on the appropriate Form T-100PE or Form T-100SE.

When stabilizers are to be used in the mix design, the stabilizer will be incorporated into the trial batch. The stabilizer will be added as indicated in the batching sequence. The transport time will be simulated prior to reactivating the stabilizer. The mix design information will include the information listed as follows under *Stabilizer* on the appropriate Form T-100PE or Form T-100SE.

Include the following:

Along with Form E-45 submit quantities of materials in accordance with WYDOT 471.0 for a verification mix design.

Completed Form T-100PE or Form T-100SE.

A batching sequence will be submitted with the Form T-100PE or Form T-100SE.

Class of Concrete and Specified Design Strength

Fine Aggregate Information;

Dry Weight and SSD Weight Aggregate Gradation Fineness Modulus Specific Gravity (SSD) Absorption Sodium Sulphate Loss per ASTM C88 Colorimetric (See WYDOT 832.0) Source Location

Coarse Aggregate Information;

Dry Weight and SSD Weight Aggregate Gradation Specific Gravity (SSD) Absorption Sodium Sulphate Loss per ASTM C88 Percentage of Wear per ASTM C131/C131M Source Location

#### WYDOT 472.0 (Rev. 10-18)

Additional Information;

Weight, Type, and Brand of Cement

Weight, Class, and Source of Fly Ash

Weight, Class, and Source of Other Pozzolans

All Admixtures and Dosages (including any special handling or mixing requirements for admixture introduction)

Weight of Net or Mixing Water (total water minus absorbed water) Water/Cement Ratio

Water/Cement+Pozzolan ratio

Unit Weight, Slump and Air Content

Early Strength Results (1, 2, 7 day, etc.), for high early strength mixes

Fracture Type of Cylinders per ASTM C39/C39M (See Form T-100SE)

A minimum of four 28-day Compressive Strength Results for structural concrete.

A minimum of three 28-day Compressive Strength Results and a minimum of three 28-day Flexural Strength Results for Portland Cement Concrete Pavement.

On-Site Admixtures;

Type of admixtures which are anticipated on site Dosage rate (including maximum dosage rate) Mixing requirements

Stabilizers;

Type of stabilizer Dosage rate, not to exceed 4 oz per 100 lb cement Mixing requirements during transport Anticipated slump and air loss (if any) during transport Method of reactivation at the site Initial set time

Units:

Weights: lb Volumes: gal/yd<sup>3</sup> respectively Admixture: fluid oz/100 lb of cement or lb/yd<sup>3</sup> Strength: psi



#### WYOMING DEPARTMENT OF TRANSPORTATION PORTLAND CEMENT CONCRETE PAVEMENT MIX DESIGN

Form T-100PE (Rev. 09-16)

Lab No.: ## Lab Mix No.: ##

Class: PCCP

Date Run: 9/17/2016

| Project Number:     | ###               | Project Location:  | On Plans       |
|---------------------|-------------------|--------------------|----------------|
| Engineer:           | Resident Engineer | Engineer Location: | Town           |
| CA Source Name:     | Pit Name          | CA Location:       | County         |
| FA Source Name:     | Pit Name          | FA Location:       | County         |
| General Contractor: | Company Name      | Concrete Supplier: | Ready Mix Name |

| Test<br>Method | ¢i,    | eve Size            |  |   |          |         | 1.11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1 | MEDIUM<br>AGGREGATE |                       |         | FINE<br>AGGREGATE |          |      |         |
|----------------|--------|---------------------|--|---|----------|---------|--|---------------------|-----------------------|---------|-------------------|----------|------|---------|
| AASHTO         | 31     | eve Size            | Pei                                    | rcent P                                 | assing   |         | Perc                                     | cent                | Passing               |         | Perce             | ent Pass | ing  |         |
| AASHIO         |        |                     | Spec                                   | s                                       | Mix      |         | **Spec                                   | s                   | Mix                   |         | Specs             |          | Mix  | (       |
|                |        | 1½"                 | 100                                    |   | 100      |         |  |                     |                       |         |                   |          |      | [       |
|                |        | 1"                  | 95-10                                  | 0                                       | 100      |         |  |                     |                       |         |                   |          |      |         |
|                |        | 3/4"                |  |   | 98       |         |  |                     | 0                     |         |                   |          |      |         |
|                |        | 1/2"                | 25-6                                   | 0                                       | 50       |         |  |                     | 0                     |         |                   |          |      |         |
| T-27           |        | 3/8''               |  |   | 30       |         |  |                     | 0                     |         | 100               |          | 100  | )       |
|                |        | #4                  | 0-10                                   | )                                       | 4        |         |  |                     |                       |         | 95-100            |          | 97   |         |
|                |        | #8                  | 0-5                                    |   | 2        |         |  |                     | <                     |         |                   |          | 87   | 5       |
|                |        | #16                 |  |   | 2        |         |  |                     |                       |         | 45-80             |          | 71   |         |
|                |        | #30                 |  |   | 2        |         |  |                     |                       |         |                   |          | 43   |         |
|                |        | #50                 |  |   | 2        |         |  |                     |                       |         | 10-30             |          | 19   | k -     |
|                |        | #100                |  |   | 2        |         |  |                     |                       |         | 2-10              |          | 5    |         |
|                |        | #200                | 0-2                                    |   | 1.8      |         |  |                     |                       |         | 0-4               |          | 2.9  | ·       |
| T-27           | Finene | ss Modulus (        |  |   |          |         | 1  |                     |                       |         |                   | 2.7      | ·    |         |
| T-21           |        | Colorir             |  |   |          |         |  |                     |                       | Transmi |                   | Stand    | ard  |         |
| T-96           |        | orasion Resis       | STATICS INSPECTION                     | 27.                                     | .0       | %       |  |                     |                       | %       |                   |          |      | _       |
| T-85,T-84      | Spe    | cific Gravity (     |  | 2.65                                    | 50       |         |  |                     |                       |         |                   |          |      |         |
| T-85,T-84      |        |                     | rption:                                | 0.8                                     | 0        | %       |  |                     |                       | %       |                   | 2.6      | 1    | %       |
| T-104          | Sc     | odium Sulfate       | Loss:                                  | 1.0                                     | 0        | %       |  |                     |                       | %       |                   | 4.0      | 0    | %       |
|                | Т      | otal Water Vo       | olume:                                 | 38.                                     | 2 gal/cy | 1       | 8  | C                   | Cement                |         | Fly Ash           | Other    | Pozz | olan    |
|                | * Mi   | xing Water W        | /eight:                                |   | 6 lb/cy  |         | Weight:                                  |                     | 580 lb/cy             |         |                   |          |      | lb/cy   |
|                | W      | ater/Cement         | Ratio:                                 | 0.4                                     |          | 1 т     | vpe/Class:                               |                     | I/II                  |         | Class F           |          |      | · ·     |
|                |        | /Cem+Pozz.          |  | 0.4                                     |          | Brar    | nd/Source:                               | Γ                   | acotah                | Н       | eadwaters         |          |      |         |
| T-119          |        | Slump, ir           | hches:                                 | 3 1/                                    |          |         | angersbergenssen, menne                  |                     | arse Aggr             |         | led. Aggr.        | Fine     | Ago  | ar.     |
| T-121          |        | Unit Weigh          |  | 142                                     |          | 1 🗅     | ry Weight:                               |                     | 1688 <sub>lb/cy</sub> |         | lb/cy             |          |      | B lb/cy |
| T-152          |        | Air Conte           | 1943-13                                | 6.0                                     | C        |         | D Weight:                                |                     | 1700 lb/cy            |         | lb/cy             |          |      | ) Ib/cy |
| T-22           | Co     | mpressive St        | 1000000000 000 00000000000000000000000 | 1                                       | Fle      | 31      | Strength                                 |                     |                       |         | Admixture         | )C       |      |         |
| T-22           | Days   |                     | Fracture T                             | vne                                     | Dave     |         | psi                                      |                     | Туре                  |         | Brand             |          | Dosa | ae      |
| 1 01           | 3      | 3810                | D                                      | <b>J</b> P <b>U</b>                     | 3        |         | 630                                      |                     | Daravair              |         | Grace             |          |      | j oz/cy |
|                | 7      | 4210                | Ē                                      |   | 7        |         | 695                                      |                     | WRD                   | Ą       | Grace             |          |      | oz/cy   |
|                | 7      | 4240                | E                                      |   | 7        |         | 710                                      |                     | Recove                |         | Grace             | 1        |      | 3 oz/cy |
|                | 28     | 5820                | D                                      |   | 28       |         | 725                                      |                     |                       |         |                   |          |      |         |
|                | 28     | 5500                | E                                      |   | 28       |         | 710                                      |                     | Ur                    | nits: ( | unless other      | wise not | ed)  | 1       |
|                | 28     | 5500                | E                                      |   | 28       |         | 835                                      |                     |                       |         | sage:lb/cy        | Volume   | /    | /cv     |
|                |        | orrelation Cor      |  |   |          |         | 000                                      |                     |                       |         | cement            | Weight   |      |         |
|                |        | lay flex str divide | a series a series e a series de        | quare                                   | * Mix    | ina V   | Vater is To                              | tal V               |                       |         | osorbed Wat       |          |      |         |
|                |        | e aver 28 day co    |  | 0.0000000000000000000000000000000000000 |          |         |  |                     |                       |         | oarse and m       |          |      |         |
|                |        | e Types             |  |   |          | cs'' re | efers to the                             |                     |                       |         | and medium        |          | ons. |         |
| N 7            |        |                     |  |   | 0.42     | w/cr    | ratio for ha                             | nd p                | aving                 |         |                   |          |      |         |
|                |        |                     |  |   | 0.38     | w/cr    | ratio for mo                             | chin                | e paving              |         |                   |          |      |         |
|                |        |                     | SHEAR C                                |   |          | Pre     | epared By:                               | Pen                 | arer's nam            | 10      |                   | ate: 9/1 | 7/20 | 16      |
|                |        |                     |  |   |          |         |  |                     |                       |         |                   |          |      |         |

#### WYDOT 472.0 (Rev. 10-18)

#### WYOMING DEPARTMENT OF TRANSPORTATION STRUCTURAL CONCRETE MIX DESIGN

Form T-100SE (Rev. 09-16)

| desap-intent        |                   |                    |              |              |        |
|---------------------|-------------------|--------------------|--------------|--------------|--------|
| Project Number:     | ####              | Project Location:  | On plans     | Lab No.:     | ####   |
| Engineer:           | Resident Engineer | Engineer Location: | Town         | Lab Mix No.: | ###    |
| CA Source Name:     | Pit Name          | CA Location:       | County/Town  | Class:       | A,B,S, |
| FA Source Name:     | Pit Name          | FA Location:       | County/Town  | Date Run:    | ~      |
| General Contractor: | Company Name      | Concrete Supplier: | Company Name |              |        |
|                     |                   |                    |              |              |        |

| Test<br>Method | Si            | eve Size              |  | AGGRE     | DARSE MEDIUM<br>BREGATE AGGREGA |       |                           | GATE              |  | FINE<br>AGGREGATE |   |               |                 |         |
|----------------|---------------|-----------------------|--|-----------|---------------------------------|-------|---------------------------|-------------------|--|-------------------|---|---------------|-----------------|---------|
| AASHTO         |               | 0120                  | F  | Percent P | assing                          |       | 10 J153 C                 | 2. 18/18/21/A (B) | Passing  |                   | Perce                                   | ent P         | assing          |         |
|                |               |                       | Sp   | ecs       | Mix                             |       | **Spec                    | S                 | Mix  | 3                 | Specs                                   |               | Mix             | :       |
|                |               | 11⁄2"                 |  | 00        | 100                             |       |                           |                   |  |                   |   |               |                 |         |
|                |               | 1"                    | 95-  | 100       | 99                              |       |                           |                   |  |                   |   |               |                 |         |
|                |               | 3/4"                  |  |           |                                 |       |                           |                   |  |                   |   |               |                 |         |
|                |               | 1/2"                  | 25   | -60       | 43                              |       |                           |                   |  |                   |   |               |                 |         |
| T-27           |               | 3/8"                  |  |           |                                 |       |                           |                   |  |                   | 100                                     |               | 100             |         |
|                |               | #4                    |  | 10        | 3                               |       |                           |                   |  |                   | 95-100                                  |               | 100             | )       |
|                |               | #8                    | 0  | -5        | 2                               |       |                           |                   |  |                   | 100000000000000000000000000000000000000 |               | 0.00            |         |
|                |               | #16<br>#30            |  |           |                                 |       |                           |                   |  |                   | 45-80                                   |               | 64              |         |
|                |               | #30<br>#50            |  |           |                                 |       |                           |                   |  |                   | 10.00                                   |               | 15              |         |
|                |               | #100                  |  |           |                                 |       |                           |                   |  |                   | 10-30                                   |               | 15              |         |
|                |               | #200                  |  | -2        | 0.2                             |       | 1                         |                   |  |                   | 2-10<br>0-4                             |               | <u>3</u><br>1.7 | 8       |
| T-27           | Finone        | #200<br>ess Modulus ( |  | -2        | 0.2                             |       |                           |                   |  |                   | 0-4                                     |               | 2.97            |         |
| T-27           | rinene        | Colorii               |  |           |                                 |       |                           |                   |  |                   |   |               | 2.97<br>Clear   | - 1     |
| T-21<br>T-96   |               | brasion Resis         |  | 23        |                                 | ]%    |                           | <b></b>           |  | %                 |   | (             | Jear            | _       |
| T-85,T-84      | St. 1997 44   | ecific Gravity        |  |           | 05.05                           | /°    |                           |                   |  | /0                |   |               |                 | - I     |
| T-85, T-84     | She           |                       | rption:  | 2.80      |                                 | %     |                           |                   |  | %                 |   |               |                 | %       |
| T-104          | 6             |                       |  | 0.5       |                                 | %     | 3                         |                   |  | %                 |   |               |                 | %       |
| 1-104          | - 30          | odium Sulfate         | LOSS.  | 0.4       | -0                              | 70    |                           |                   |  | 70                |   |               |                 | 70      |
|                | Т             | otal Water Vo         | olume:   | 2         | 6 gal/cy                        | 1     |                           | Ce                | ement  |                   | Fly Ash                                 | Oth           | er Pozz         | olan    |
|                |               | ixing Water V         | and the second state of the second states  |           | 7 lb/cy                         |       | Weight:                   |                   | 532 lb/cy  |                   | lb/cy                                   |               |                 | lb/cy   |
|                | 2017 A.C. 102 | vater/Cement          | -  | 0.3       |                                 | 1 τ   | vpe/Class:                |                   | I-II   |                   |   | -             |                 |         |
|                |               | r/Cem+Pozz.           | and a second sec | 0.0       |                                 |       | nd/Source:                | -                 | lolcim   |                   |   |               |                 |         |
| T-119          |               | Slump, i              |  | 2.0       | 0                               |       |                           |                   | rse Aggr   | N                 | led. Aggr.                              | F             | ine Agg         | Ir.     |
| T-121          |               | Unit Weigh            | esected to the second  | 148       | 200 D                           | 1 -   | ory Weight:               |                   | 907 lb/cy  |                   | lb/cy                                   |               |                 | b/cy    |
| 12 23461423    |               |                       | 500002   | 6.        |                                 |       | SD Weight:                |                   | 917 lb/cy  |                   |   | -             |                 | B/cy    |
| T-152          |               | Air Conte             | 2  | 0.        |                                 | 00    | so weight.                |                   | 917 lb/cy  |                   | lb/cy                                   |               | 1255            | p Ib/cy |
| T-22           |               | ompressive St         | trength  |           | Units                           |       | unless                    |                   |  |                   | Admixture                               | es            |                 |         |
|                | Days          | psi                   | Fracture   | Туре      |                                 |       | se noted                  |                   | Туре   | 9                 | Brand                                   |               | Dosa            | ge      |
|                | 7             | 4200                  |  | 3         | Weig                            |       |                           |                   | WRA  | ۱                 | Grace                                   |               | 38              | oz/cy   |
|                | 7             | 4340                  |  | 3         |                                 |       | gal/cy                    |                   |  |                   | WRDA 64                                 | 4             |                 | oz/cy   |
|                | Ave           | 4270                  |  |           |                                 |       | e Dosage:                 |                   |  |                   |   |               |                 | oz/cy   |
|                | 14            | 4340                  |  | ٩         |                                 |       | oz per                    |                   | Air  | 1                 | Grace                                   |               | 7               | oz/cy   |
|                | 14            | 4270                  |  | 3         | 100                             | lb ce | ement                     | ΙL                |  |                   | Daravair                                | 9             |                 | oz/cy   |
|                | Ave           | 4370                  |  |           |                                 |       |                           |                   |  |                   | 1000                                    |               |                 | oz/cy   |
|                | 28            | 4990                  |  | 3         |                                 |       |                           |                   |  |                   |   |               |                 | oz/cy   |
|                | 28            | 4920                  |  | 3         |                                 |       |                           |                   |  |                   | osorbed Wate                            |               |                 |         |
|                | 28            | 4830                  |  | ٩         |                                 |       | 00                        | •                 | <ol> <li>March 1998 Annual State Street St<br/>Street Street Stre</li></ol> |                   | oarse and m                             |               |                 |         |
|                | 28            | 4870                  |  | 3         | "Spe                            | cs" r | efers to the              | com               | oined co   | arse              | and medium                              | grac          | lations.        |         |
|                | Ave           | 4900                  |  |           |                                 |       |                           |                   |  |                   |   |               |                 |         |
|                | Fractur       | re Types              |  |           | COM                             | MEN   | ITS:                      | <u>Mix i</u>      | s accept   | abled             | as submitted                            |               |                 |         |
|                | , raotai      |                       |  | · · · · · | -                               |       |                           |                   |  |                   |   |               |                 |         |
|                |               |                       | 3-EAR<br>D   | E         |                                 |       | epared By:<br>Contractor: |                   |  |                   |   | ate:          |                 |         |
|                |               |                       | -  |           |                                 | 2     | Sonnacion.                |                   |  |                   | D                                       | a.e. <b>-</b> |                 |         |

#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

Scope: This test method covers the procedure for determining the concretes compressive strength by applying a compressive axial load to molded cylinders or cores.

This procedure applies to projects which include WYDOT Standard Specifications.

Use: This procedure is used to determine if the compressive strengths of the concrete are in compliance with the specified strength or to determine the concretes strength at a specific time.

Reference

| Documents: | ASTM C39      | Standard Test Method for Compressive Strength of |
|------------|---------------|--|
|            |               | Cylindrical Concrete Specimens                   |
|            | WYDOT         | Current WYDOT Standard Specifications *          |
|            | WYDOT T-109   | Concrete Placing Report                          |
|            | WYDOT T-100PE | Portland Cement Concrete Pavement Mix Design     |
|            | WYDOT T-100SE | Structural Concrete Mix Design                   |
|            |               |  |

♦ Refer to "For All Concrete Sections" notation in Table of Contents - 400 Pavements.

Procedure: Same as ASTM C39 with the following requirements.

Cylinder molds will be 4 inch x 8 inch.

Report information on WYDOT Form T-100PE and/or T-100SE when reporting mix design information.

Report information on WYDOT Form T-109 when reporting placing and break information.

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#### FLEXURAL STRENGTH OF PORTLAND CEMENT CONCRETE BEAMS

Scope: This test method covers the procedure for determining the concretes flexural strength by the use of a simple beam with third point loading.

This procedure applies to projects for Portland Cement Concrete Pavement in WYDOT Standard Specifications.

Use: This procedure is used to determine the flexural strength of the concrete for Quality Control and Quality Acceptance (QC / QA) or to determine the concrete strength at a specific time.

Reference

| Documents: | ASTM C78      | Standard Test Method for Flexural Strength of Concrete |
|------------|---------------|--|
|            |               | (Using Simple Beam with Third-Point Loading)           |
|            | WYDOT         | Current WYDOT Standard Specifications *                |
|            | WYDOT 486.0   | Making and Curing Concrete Beams                       |
|            | WYDOT T-100PE | Portland Cement Concrete Pavement Mix Design           |
|            | WYDOT T-109   | Concrete Placing Report                                |

- ✤ Refer to "For All Concrete Sections" notation in Table of Contents 400 Pavements.
- Procedure: Same as ASTM C78 with the following requirements:

Span length, "L", of the testing apparatus will be 18 inch.

The beam mold dimensions will be as specified in WYDOT 486.0.

- Report: Report information on WYDOT Form T-100PE when reporting mix design information or on WYDOT Form T-109 when reporting placing and break information.
- Commentary: When calculating the modulus of rupture, "R", (flexural strength) per the equation in the *Calculation* of ASTM C78, the equation can be simplified to the following form when the dimensions specified above are used.

R = P / 12 when "R" is in psi and "P" is in lb

WYDOT 474.0 (Rev. 10-18)

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#### CORRELATION OF COMPRESSIVE STRENGTH TO FLEXURAL STRENGTH

Scope: This test method covers the procedure for determining and applying the correlation constant used for calculating flexural strength of Portland Cement Concrete Pavement (PCCP) based on compressive strength results.

This procedure applies to projects which include WYDOT Standard Specifications.

Use: This procedure is used for the determination of the compressive strength to flexural strength correlation constant from the mix design information. The constant is then used to convert compressive strength field data to flexural strength.

Reference

| Documents: | WYDOT         | Current WYDOT Standard Specifications *        |
|------------|---------------|--|
|            | WYDOT 476.0   | Allowable Range of Mix Design Strength Results |
|            | WYDOT T-100PE | Portland Cement Concrete Pavement Mix Design   |

- ♦ Refer to "For All Concrete Sections" notation in Table of Contents 400 Pavements.
- Procedure: The following equation will be utilized:

 $FS = C_C x (CS)^{1/2}$ 

Solving for  $C_C$  yields:  $C_C = FS / (CS)^{1/2}$ 

The values for flexural strength, "FS", and compressive strength, "CS", will be determined from the mix design results. Both the flexural strength values and the compressive strength values will come from the same batch. The flexural strength value will be the average of a minimum of three 28 day beam tests and the compressive strength value will be the average of a minimum of three 28 day cylinder tests.

Report: Report information on WYDOT Form T-100PE, Portland Cement Concrete Pavement Mix Design.

The range of the mix design strength values will meet the limits as specified in WYDOT 476.0. The correlation constant, " $C_C$ ", will be recorded to (0.01).

All strength values from the mix design will be reported.

If a new mix design is required, a new correlation constant will be calculated.

After review and approval from the WYDOT Materials Program, the correlation constant will be used to calculate the flexural strength from the 28-day Quality Control and Quality Acceptance (QC / QA) cylinders tests if the cylinder option is selected.

The number of samples required to evaluate a sublot will be in accordance with the *WYDOT Standard Specifications*. If the flexural strength is to be determined from the cylinder compressive strengths, the number of required samples will be based on the required number of cylinders.

#### ALLOWABLE RANGE OF MIX DESIGN STRENGTH RESULTS

Scope: This method covers procedures for determining the allowed range of mix design strength results.

This procedure applies to projects which include WYDOT Standard Specifications.

This section applies only to Quality Control and Quality Acceptance (QC/QA) projects for which Contractor mix designs are used, according to WYDOT 472.0.

Use: This procedure provides the allowed limits for the range of strength results from the mix design trial batch.

#### Reference

| Documents: | ASTM C39             | Standard Test Method for Compressive Strength of Cylindrical Concrete Specimens                              |
|------------|----------------------|--|
|            | ASTM C78             | Standard Test Method for Flexural Strength of Concrete (Using Simple Beam with Third-Point Loading)          |
|            | ASTM C670            | Standard Practice for Preparing Precision and Bias<br>Statements for Test Methods for Construction Materials |
|            | WYDOT<br>WYDOT 472.0 | Current WYDOT Standard Specifications<br>Contractor Concrete Mix Design Procedure                            |

- ♦ Refer to "For All Concrete Sections" notation in Table of Contents 400 Pavements.
- Procedure: The difference between the maximum and the minimum 28 day compressive strength results from the mix design trial batch samples will be less than or equal to the values shown below:

#### Table 1

| Average Mix Design 28 day<br>Compressive Strength, psi | Maximum Allowed Difference<br>Of Compressive Strength Results<br>4 x 8 Cylinders |
|--|--|
| 3000 to 3499   | 350 psi  |
| 3500 to 3999   | 400 psi  |
| 4000 to 4499   | 450 psi  |
| 4500 to 4999   | 500 psi  |
| 5000 to 5499   | 560 psi  |
| 5500 to 5999   | 610 psi  |
| 6000 to 6499   | 660 psi  |
| 6500 or greater  | 690 psi  |
|  |  |

A minimum of three 28 day compressive strength tests are required for the mix design. If more than three tests are used to determine the average compressive strength value, the above range limits will still apply.

The difference between the maximum and the minimum 28 day flexural strength results from the mix design trial batch samples will be less than or equal to the values shown below:

#### Table 2

| Average Mix Design 28 day<br>Flexural Strength, psi | Maximum Allowed Difference<br>Of Flexural Strength Results |
|---|--|
| 650 to 699  | 125 psi  |
| 700 to 749  | 135 psi  |
| 750 to 799  | 145 psi  |
| 800 to 849  | 155 psi  |
| 850 to 899  | 165 psi  |
| 900 or greater                                      | 175 psi  |

A minimum of three 28 day flexural strength tests are required for the mix design. If more than three tests are used to determine the average flexural strength value, the above range limits will still apply.

#### FIELD SAMPLING FRESH CONCRETE

- Scope: This method describes the procedure for acquiring representative samples of fresh concrete as delivered to the project site. This procedure is adopted from ASTM C172.
- Use: This procedure is used to collect samples of fresh concrete at the project site for the purpose of obtaining test samples for determining specification compliance of the concrete.

To assure accuracy in testing of fresh concrete, every precaution should be taken to obtain a sample of concrete which is truly representative of the entire batch and then to protect that sample from the damaging effects of evaporation and contamination.

Apparatus: As per ASTM C172.

Reference

| Documents: | ASTM C172   | Standard Method of Test for Sampling Freshly Mixed |
|------------|-------------|--|
|            |             | Concrete   |
|            | WYDOT       | Current WYDOT Standard Specifications �            |
|            | WYDOT T-109 | Concrete Placing Report                            |
|            | WYDOT T-128 | Construction Test Requirements                     |

✤ Refer to "For All Concrete Sections" notation in Table of Contents – 400 Pavements.

Procedure: As per ASTM C172.

Commentary: Measure slump, air content, unit weight, temperature, and strength specimens from one composite sample. Each test is to be performed by a single tester.

Note: Unit weight should be measured while conducting air content procedure.

Report the sampling and testing information on WYDOT Form T-109.Refer to additional requirements for projects in *WYDOT Standard Specifications* and/or Form T-128.

WYDOTs representative will determine which loads will be sampled for quality acceptance (QA).

Report: Report information on WYDOT Form T-109, *Concrete Placing Report*.

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#### METHOD OF DETERMINING TEMPERATURE OF FRESHLY MIXED CONCRETE

| Scope:     | This test method describes procedures for determining the temperature of freshly mixed concrete. This procedure is adopted from ASTM C1064. |   |  |
|------------|---|---|--|
| Use:       | This procedure is used for determining the temperature of freshly mixed concrete.   |   |  |
| Apparatus: | As per ASTM C1064.  |   |  |
| Reference  |   |   |  |
| Documents: | ASTM C1064  | Standard Test Method for Temperature of Freshly Mixed<br>Hydraulic-Cement Concrete) |  |
|            | WYDOT   | Current WYDOT Standard Specifications *   |  |
|            | WYDOT 477.0   | Field Sampling Fresh Concrete   |  |
|            | WYDOT T-109   | Concrete Placing Report   |  |
|            | <ul> <li>Refer to "For All Control</li> </ul>   | efer to "For All Concrete Sections" notation in Table of Contents – 400 Pavements.  |  |
| Procedure: | As per ASTM C1064.  |   |  |
| Report:    | Report information on WYDOT Form T-109, Concrete Placing Report.  |   |  |

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### **UNIT WEIGHT (DENSITY) OF CONCRETE**

Scope: This test method covers the procedure for determining the unit weight of freshly mixed concrete. This procedure is adopted from ASTM C138.
 Use: This method is used to calculate the unit weight and yield of the freshly mixed concrete at the project site for the purpose of determining specification compliance of the concrete

Apparatus: As per ASTM C138.

Reference

| Reference  |             |  |
|------------|-------------|--|
| Documents: | ASTM C29    | Standard Test Method for Bulk Density ("Unit Weight") and  |
|            |             | Voids in Aggregate   |
|            | ASTM C138   | Standard Test Method for Density (Unit Weight), Yield, and |
|            |             | Air Content (Gravimetric) of Concrete                      |
|            | ASTM C172   | Standard Practice for Sampling Freshly Mixed Concrete      |
|            | ASTM C231   | Standard Test Method for Air Content of Freshly Mixed      |
|            |             | Concrete by the Pressure Method                            |
|            | WYDOT       | Current WYDOT Standard Specifications *                    |
|            | WYDOT 100.0 | Definitions - WaterTable                                   |
|            | WYDOT 477.0 | Field Sampling Fresh Concrete                              |
|            | WYDOT 481.0 | Air Content of Freshly Mixed Concrete                      |
|            |             |  |

♦ Refer to "For All Concrete Sections" notation in Table of Concretes – 400 Pavements.

Calibration: As per ASTM C231 and ASTM C29.

$$V = \frac{W_{\text{Total} -} W_{\text{Tare}}}{D}$$

Where:

| V           | = | Volume of container, ft <sup>3</sup> .               |
|-------------|---|--|
| $W_{Total}$ | = | Weight of water, container and strike-off plate, lb; |
| $W_{Tare}$  | = | Tare of empty container and strike-off plate, lb;    |
| D           | = | Unit Weight of water (See WYDOT 100.0);              |

Procedure: As per ASTM C138.

$$D = \frac{W_{\text{Total}} - W_{\text{Tare}}}{V}$$

Where:

Te: D = Unit Weight (Density) of Concrete,  $lb/ft^3$ W<sub>Total</sub> = Weight of concrete and container, lb; W<sub>Tare</sub> = Tare of empty container, lb; V = Volume of container,  $ft^3$ . Report: Report information on WYDOT Form T-109, *Concrete Placing Report*.

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### **SLUMP TEST**

- Scope: This test method describes the procedure for determining the concretes slump in both the laboratory and the field. This procedure is adopted from ASTM C143.
- Use: This procedure is used to determine the consistency of the fresh concrete at the project site for the purpose of determining specification compliance for structural concrete and is considered an applicable method for concrete having coarse aggregate up to 1½ inch in size.

The maximum slump specifications for the class of concrete are found in *WYDOT Standard Specifications*.

Apparatus: As per ASTM C143.

### Reference

| Iterenere              |  |   |
|------------------------|--|---|
| Documents:             | ASTM C143                                | Standard Test Method for Slump of Hydraulic-Cement Concrete   |
|                        | WYDOT                                    | Current WYDOT Standard Specifications �   |
|                        | WYDOT 477.0                              | Field Sampling Fresh Concrete   |
|                        | WYDOT T-109                              | Concrete Placing Report   |
|                        | <ul> <li>Refer to "For All Co</li> </ul> | ncrete Sections" notation in Table of Contents – 400 Pavements.   |
| Sampling:              | Sample in accordance                     | e with WYDOT Standard Specifications and WYDOT 477.0.   |
| Procedure:             | As per ASTM C143.                        |   |
| Report:                | Report the slump in specimen during the  | terms of inches to the nearest $\frac{1}{4}$ inch of subsidence of the test on Form T-109.                          |
| Precision<br>and Bias: |  | <i>tandard Specifications</i> for acceptable tolerances between two laboratories, rather than Table 1 in ASTM C143. |

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### AIR CONTENT OF FRESHLY MIXED CONCRETE

Scope: This test method describes the procedure for determining the air content of freshly mixed concrete in both the laboratory and the field. This procedure is adopted from ASTM C231.

The procedure in ASTM C231 describes the use of two types of air meters, only Type B air meters are allowed on WYDOT projects. The principle of the Type B meter consists of equalizing a known volume of air at a known pressure in a sealed air chamber with an unknown volume of air in the concrete sample. The dial on the pressure gauge is being calibrated in terms of percent air for the observed pressure at which equalization takes place.

Use: This method is used to determine the air content of the freshly mixed concrete in the laboratory or at the project site for the purpose of determining specification compliance.

The percent of entrained air content, range specification for the class of concrete, and air content values are found in *WYDOT Standard Specifications*.

- Apparatus: As per ASTM C231.
  - \* Calibration cylinder (5% air puck) is an acceptable alternative to the calibrating vessel.

### Reference

| Documents: | ASTM C138   | Standard Test Method for Density (Unit Weight), Yield, and<br>Air Content (Gravimetric) of Concrete |
|------------|-------------|---|
|            | ASTM C231   | Standard Test Method for Air Content of Freshly Mixed   |
|            |             | Concrete by the Pressure Method   |
|            | WYDOT       | Current WYDOT Standard Specifications �   |
|            | WYDOT 477.0 | Field Sampling Fresh Concrete   |
|            | WYDOT 479.0 | Unit Weight (Density) of Concrete   |
|            | WYDOT T-109 | Concrete Placing Report   |
|            | WYDOT T-480 | Equipment Calibration, Verification, Maintenance and  |
|            |             | Checking Form   |
|            | WYDOT T-481 | Report of Calibration Verification  |

♦ Refer to "For All Concrete Sections" notation in Table of Contents – 400 Pavements.

Calibration: As per ASTM C231.

Sampling: Obtain a representative sample of freshly mixed concrete in accordance with WYDOT 477.0.

WYDOT 481.0 (Rev. 10-18)

This procedure must be started within five minutes of obtaining the composite sample and completed within fifteen minutes of obtaining the composite sample. There is a ten minute window for running the air content test.

Procedure: As per ASTM C138.

Report: Report calibration information on WYDOT T-480.0, *Equipment Calibration, Verification, Maintenance, and Checking Form* and WYDOT T-481.0, *Report of Calibration Verification.* Report air content results on WYDOT Form T-109, *Concrete Placing Report* 

### REPLACEMENT PARTS LIST FOR PRESS-UR-METER

### Part No.

- 1. Pressure chamber
- 2. Pressure chamber cap
- 3. Pressure chamber elbow
- 4. Pressure chamber gasket
- 5. Pressure chamber air release stem
- 6. Pressure chamber air release cap
- 7. Complete gauge
- 8. Pump assembly complete
- 9. Pump piston leather
- 10. Pump air-check gasket
- 11. Needle valve stem
- 12. Needle valve nut
- 13. Need valve lever
- 14. Need valve lever
- 15. Needle valve "O" ring
- 16. Needle valve spring
- 17. Needle valve spring retainer
- 18. Needle valve seat assembly
- 19. Cover

- 20. Cover "O" ring
- 21. Cover Pet cock
- 22. Clamp
- 23. Clamp nut
- 24. Clamp trunion
- 25. Clamp spring
- 26. Clamp toggle
- 27. Toggle set screw
- 28. Toggle lock nut
- 29. Base
- 30. Base handle
- 31. Calibrating vessel (not illustrated)
- 32. Calibrating tube (outer) (not illustrated)
- 33. Calibrating tube (inner) (not illustrated)
- 34. Strike off bar (not illustrated)
- 35. Tamping Rod (not illustrated)
- 36. Syringe (not illustrated)
- 37. Gauge glass (not illustrated)
- 38. Carrying case (not illustrated)

#### WYOMING DEPARTMENT OF TRANSPORTATION T-481 MATERIALS TESTING LABORATORY (Rev. 09-16) Calibration Procedure MTM 481.0 REPORT OF CALIBRATION VERIFICATION Refer to General Equipment Inventory/ Calibration File for calibration frequency information.

### **UNIT WEIGHT**

| AIR METER NO                    |               | DATE              | CALIBR     | ATED:       | MM/DD/YR   |
|---------------------------------|---------------|-------------------|------------|-------------|------------|
| TARE = <b>8.31</b>              |               |                   | INIT       | IALS:       | JT         |
| VOL. = <b>0.2462</b>            |               | LAST CALIBRATION: |            |             | MM /DD /YR |
|                                 |               | NEXT              | CALIBRA    | ATION:      | MM/ DD /YR |
| A = Empty Buck                  | cet.          | A =               | 8.31       | Ъ           |            |
| B = Glass Plate                 |               | В =               | 2.80       | lb          |            |
| C = Wt. of Wate                 | r             | C =               | 15.34      | lb          |            |
| W = Total Wt.                   |               | W =               | 26.45      | lb          |            |
| T = Temp. of W                  | ater          | T =               | 70         | °F          |            |
| For temperature/density of wate | r refer to WY | DOT 100.0         | – Definiti | ons Water I | Table .    |
| D = Density of V                | Vater         | D =               | 62.301     | _lb/ft³     |            |
| FORMULA = C / D =               | VOL. (CU. F   | Т.)               | 0.2462     | lb/ft³      |            |
| 1.1                             | PRESSUR       | E METER           | CALIB      | RATION      |            |
|                                 | C Puck        |                   | /essel     |             |            |
| INITIAL READING=                | 3.0%          |                   |            |             |            |

CALIBRATION POINTS= (record to nearest 0.1%)

Gauge Reading @ 5% Gauge Reading @ 10% 4.0%

### **Equipment Calibration, Verification, Maintenance and Checking Form** (Rev. 09-16)



| Equipment Type: | Pressure Meter |
|-----------------|----------------|
| Model No:       | Туре В         |
| Serial No:      | ###            |
| Brand:          | Brand name     |
| Specification:  | Every 3 months |

| Maintenance Description |  |
|-------------------------|--|
|                         |  |
|                         |  |
|                         |  |
|                         |  |

AASHTO Rec's or Mandantory cal/ver/ck/maint Frequency: ASTM-C138/ C29/ C231

| Last             | Next             | Date             | Calibration  | *     |                     |
|------------------|------------------|------------------|--------------|-------|---------------------|
| cal/ver/maint/ck | cal/ver/maint/ck | cal/ver/maint/ck | TARE/ VOLUME | Initl | Comments or Results |
| 09/01/16         | 12/01/16         | 12/02/16         | 7.85 / .2473 |       |                     |
| 12/01/16         | 03/01/17         |                  | 7.85 / .2474 |       |                     |
|                  |                  |                  | 7.85 / .2475 |       |                     |
|                  |                  |                  | 7.85 / .2476 |       |                     |
|                  |                  |                  |              |       |                     |
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\* See worksheets for original initial of person conducting equipment checks.

T-480 Example.xlsx

WYDOT 481.0 (Rev. 10-18)

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### **CONCRETE PLACING REPORT**

- Scope: This procedure describes the method used in recording and reporting the physical properties of the fresh concrete at the project site, water-cement ratios, placement conditions and cylinder and/or beam identification numbers.
- Use: The *Concrete Placing Report*, WYDOT Form T-109, is used to record the properties of the fresh concrete along with placement location and placement conditions. The WYDOT Form T-109 provides a permanent record and copies of the placing report accompany the concrete cylinders and/or beams when they are transported for testing.
- Sampling: Representative samples of the fresh concrete will be taken as outlined in WYDOT 477.0.
- Procedure: Use one of the versions of the WYDOT Form T-109 (see example in this section) as a record and report form, indicating as much information as possible about the concrete being delivered to the project. The sampling location will be in accordance with WYDOT 477.0.

Record the laboratory mix design data, which will be based on a  $1 \text{ yd}^3$  mix, the weather conditions, and all test results including temperature (WYDOT 478.0), density (WYDOT 479.0), slump (WYDOT 480.0), and air content (WYDOT 481.0), and, whether or not cylinders and/or beams are taken.

When cylinders are taken, a minimum of three cylinders will always be used for determining the ultimate 28 day strength. Any early breaks will require additional cylinders.

Record the number of days until cylinders are to be broken in the column Requested Testing Age (Days) and the location of each set of cylinders taken so that if necessary they can pinpoint the area of the placement at a later date.

Record the water/cement ratio being used by subtracting the absorbed water from the total water in a unit volume of concrete and dividing this result by the weight of the cement in the unit volume of concrete.

| Example: | Per yd <sup>3</sup> of concrete | Total water*: |                  |        |
|----------|---------------------------------|---------------|------------------|--------|
|          |                                 | Absorption:   | <u>- 30.0 lb</u> |        |
|          |                                 | Net water:    | 250.4 lb         |        |
|          | Water/cement Ratio              | Net Water     | 250.4 lb         | = 0.44 |
|          | for unit volume                 | Total Cement  | 575 lb           | - 0.44 |

\* Total water includes all water added into the mix which includes all the water in the aggregate, the water added at the batch plant and the water added at the site.

| Basic Project Information     |                 |  |  |  |
|-------------------------------|-----------------|--|--|--|
| Project Number:               | B123456         |  |  |  |
| Project Name:                 | Bridge Rehab    |  |  |  |
| Resident Engineer:            | A Baker         |  |  |  |
| Engineer's Town:              | Anytown         |  |  |  |
| Concrete Class:               | A               |  |  |  |
| Max w/c-F.A. ratio:           | 0.45            |  |  |  |
| Fine Aggregate Source:        | Best Pit        |  |  |  |
| Coarse Aggregate Source:      | Arm Pit         |  |  |  |
| Cement Type:                  | -               |  |  |  |
| Cement Supplier/Manufacturer: | Holcim          |  |  |  |
| Fly Ash Class:                | F               |  |  |  |
| Fly Ash Source:               | Bridger         |  |  |  |
| Fly Ash to Cement Ratio:      | 1.0:1.0         |  |  |  |
| Silica Fume Source:           |                 |  |  |  |
| Fiber Source:                 |                 |  |  |  |
| Concrete Supplier:            | ABC Concrete    |  |  |  |
| Water Source:                 | City of Anytown |  |  |  |
| Is Water Potable?             | Yes             |  |  |  |

|               | the Lab                  | the mix design from | All information can be found on |
|---------------|--------------------------|---------------------|---------------------------------|
| 7             |                          | 2018-001            | Lab Mix Design #:               |
| ues under 1%  | Enter values             | 0.827%              | Fine Aggregate Absorption:      |
| 0.5% as 0.005 |                          | 1.152%              | Coarse Aggregate Absorption:    |
|               | dry weight               | 1171                | Fine Aggregate (Ib/CY):         |
|               | dry weight               | 1727                | Coarse Aggregate (Ib/CY):       |
|               |                          | 526                 | Cement (lb/CY):                 |
|               |                          | 132                 | Fly Ash (lb/CY):                |
|               | _                        | No                  | Lithium Used:                   |
|               | %                        |                     | Air Content Correction Factor:  |
|               |                          | (if needed)         | Silica Fume Info                |
|               | _                        |                     | -                               |
|               |                          | on mix design)      | Additives (as listed            |
|               |                          | Quantity *          | <u>Name</u>                     |
|               |                          |                     | AMEY 310                        |
| :             | oz/100 cwt               |                     | AMEX 210                        |
|               | oz/100 cwt<br>oz/100 cwt | 5                   | WRDA 64                         |
| :             | ·                        | 5                   |                                 |
|               | oz/100 cwt               | 5                   |                                 |

#### Notes (Please Read):

> Mixes with medium aggregate are not supported in this form.

> All info on this page can be entered before placement starts.

> Leave the field blank if you aren't using that source or product.

> When information is added in the "Basic Project Information" section other fields of this entire file will be populated. An error on this tab will leave fields unavailable or add unnecessary fields on other tabs.

> "Concrete Class", "Fly Ash to Cement Ratio", "Is water potable?", and "Lithium Used" have drop down menus, select from the options shown.

 "Max w/c-F.A. ratio" is auto-populated based on Class selected. For SFMC the cement plus fly ash portion includes the silica solids.
 > Assume 1:1 fly ash replacement ratio unless told otherwise.
 In-Spec Test Limits \*

|            | Min  | Max    | * These limits are auto populated    |
|------------|------|--------|--------------------------------------|
| Slump (in) | 0.0  | 6.0    | based on the class of concrete. If   |
| Air        | 4.5% | 7.5%   | necessary, other values can be input |
| Temp       | 50°F | 90 ° F | here for special mixes.              |

|                 | Project           | No                 | B1234      | 456         |               | Supplier  | AB           | C Cond       | rete                | _              | C   | lass of C         | oncrete      |                       | Α             | -              |               |       |
|-----------------|-------------------|--------------------|------------|-------------|---------------|-----------|--------------|--------------|---------------------|----------------|---|-------------------|--------------|-----------------------|---------------|----------------|---------------|-------|
|                 | CY                |                    | 1/4        | 1/2         | 2             | 1         | 2            |              | 3                   | 4              |   | 5                 | 6            |                       | 7             | 8              |               | 10    |
| ds 🔶            | Cement            |                    | 132        | 263         |               | 526       | 105          | 2            | 1578                | 210            | 4   | 2630              | 315          | 6                     | 3682          | 420            | 8             | 5260  |
| Solids<br>(lbs) | Fly Ash           |                    | ///££///   | /// 66      |               | 132//     | 264          | //////       | 396                 | 52             | 11/11/2                                       | 660               | 79           |                       | 924           | 105            | <u>6     </u> | 1320  |
| <i>s</i> –      |                   |                    |            |             |               |           |              |              |                     |                | <i></i>                                       |                   | 3//////      |                       |               |                |               |       |
|                 | 0.0%              |                    | 293        | 586         | 5             | 1,171     | 2,34         | 2            | 3,513               | 4,68           | 4   | 5,855             | 7,02         | 26                    | 8,197         | 9,36           | 8             | 11,71 |
|                 | ////0.5%          | 111                | //294///   | ///589      |               | //1,177 / | 1/2,35       |              | 3,531//             | /4,70          |   | 5,884//           | 7.06         |                       | 8,238 //      | 9,41           |               | 11,76 |
|                 | 1.0%              |                    | 296        | 592         |               | 1,183     | 2,36         |              | 3,548               | 4,73           |   | 5,914             | 7,09         |                       | 8,279         | 9,46           |               | 11,82 |
|                 | ///1.5%           | 11.1               | /297///    | ///599      |               | /1,189    | 1/2,37       |              | 3,566 //            | //4,75         |   | 5,943/            | 1/7,13       |                       | 8,320         | 9,50           |               | 11,88 |
| (s              | 2.0%              |                    | 299        | 598         |               | 1,194     | 2,38         |              | 3,583               | 4,77           |   | 5,972             | 7,16         | 1                     | 8,361         | 9,55           |               | 11,94 |
| (Ibs)           | /// 2.5%          | 11.1               | /300 //    | ///601      | 1111          | //1,200// | //2,40       |              | 3,601//             | /4,80          |   | 6,001//           | 7,20         |                       | 8,402         | 9,60           |               | 12,00 |
| ш               | 3.0%              |                    | 302        | 604         | -             | 1,206     | 2,41         |              | 3,618               | 4,82           |   | 6,031             | 7,23         |                       | 8,443         | 9,64           |               | 12,06 |
|                 | ////3.5%/         | 11.7               | /303///    | 607         |               | /1212//   | 1/2,42       |              | 3,636//             | //4,84         |   | 6,060 //          | 17.27        |                       | 8,484         | 9,69           |               | 12,12 |
| G               | 4.0%              |                    | 305        | 609         |               | 1,218     | 2,43         |              | 3,654               | 4,87           |   | 6,089             | 7,30         |                       | 8,525         | 9,74           |               | 12,17 |
| Ŭ               | ////4.5%/         |                    | //306///   | ///612      |               | /,1,224// | 1/2,44       |              | 3,671               | /4,89          |   | 6,118//           | 1/7,34       |                       | 8,566 //      | 9,79           |               | 12,23 |
| Ϋ́.             | 5.0%              |                    | 308        | 615         |               | 1,230     | 2,45         |              | 3,689               | 4,91           |   | 6,148             | 7,37         |                       | 8,607         | 9,83           |               | 12,29 |
| Ğ               | 1///5.5%          | 11.7               | //309///   | 618         |               | //1,235// | 2,47         |              | 3,706%              | // 4,94        |   | 6,177             | 7/7/41       |                       | 8,648         | 9,88           |               | 12,35 |
| AGGREGATE       | 6.0%              | 1                  | 311        | 621         |               | 1,241     | 2,48         |              | 3,724               | 4,96           |   | 6,206             | 7,44         |                       | 8,689         | 9,93           |               | 12,41 |
| ш               | ////6.5%          | 11/1               | //312///   | 624         | 1111          | //1,247// | 7/2,49       |              | 3,741%              | //4,98         |   | 6,236             | 1/7/48       |                       | 8,730         | 9,97           |               | 12,47 |
| FINE            | 7.0%              |                    | 314        | 627         | -             | 1,253     | 2,50         | Î            | 3,759               | 5,01           |   | 6,265             | 7,51         |                       | 8,771         | 10,02          |               | 12,53 |
|                 | 1// 7.5%          | 11.1               | 315//      | ///630      |               | /1,259//  | //2,51       |              | 3,776//             | //5,03         | × × × × × ×                                   | 6,294             | // 7,55      |                       | 8,812         | /10,0          |               | 12,58 |
|                 | 8.0%              | Ť                  | 316        | 633         | -             | 1,265     | 2,52         |              | 3,794               | 5,05           |   | 6,323             | 7,58         |                       | 8,853         | 10,11          |               | 12,64 |
|                 | ////8.5%          | 11.1               | 318//      | /// 636     | 111           | //1,271// | //2,54       |              | 3,812 //            | //5,08         | 2 2 1 X 2 1                                   | 6,353//           | 7,62         |                       | 8,894         | //10,10        |               | 12,70 |
|                 | 9.0%              |                    | 319        | 639         |               | 1,276     | 2,55         | 3            | 3,829               | 5,10           |   | 6,382             | 7,65         |                       | 8,935         | 10,2           | -             | 12,76 |
|                 | 0.0%              |                    | 432        | 864         |               | 1,727     | 3,45         | 4            | 5,181               | 6,90           | 8   | 8,635             | 10,3         | 52                    | 12,089        | 13,8:          | 16            | 17,27 |
|                 | /// 1.0%          | 111                | /436///    | ///873      | 111           | /1,744 // | //3,48       | <u>97,7</u>  | 5,233 //            | //6,97         |   | 8,721//           | / 10,4       | 667 72                | 12,210/       | 13,9           |               | 17,44 |
| ğ               | 1.5%              |                    | 438        | 877         | '             | 1,753     | 3,50         | 6            | 5,259               | 7,01           | 2   | 8,765             | 10,5         | 17 :                  | 12,270        | 14,0           | 23 :          | 17,52 |
| AGGREGATE (lbs) | ///2.0%           | 11.1               | /441//     | ///881      | 1//           | /1,762//  | //3,52       | 3%/          | 5,285 //            | 17,04          | 6/.//.  | 8,808             | //10,5       | 69% (Z.               | 12,331        | 14,0           | 9274 VI       | 17,61 |
|                 | 2.5%              |                    | 443        | 886         | ; [           | 1,770     | 3,54         | 0            | 5,311               | 7,08           | 1   | 8,851             | 10,6         | 21 :                  | 12,391        | 14,16          | 51            | 17,70 |
|                 | ///3.0%           | 11.1               | 445///     | /// 890     |               | /_1,779// | //3,55       | 87/4         | 5,336 //            | 7,11           | 5////   | 8,894             | //10,6       | 73% //                | 12,452%       | / 14,2         | 30% 22        | 17,78 |
| B               | 3.5%              |                    | 447        | 894         |               | 1,787     | 3,57         | 5            | 5,362               | 7,15           | 0   | 8,937             | 10,7         | 25 1                  | 12,512        | 14,30          | 00 :          | 17,87 |
| R               | ///4.0%           | 11.4               | /449///    | ///899      | 11.1          | 1,796//   | //3,59       | 2// //       | 5;388 //            | //7,18         | <b>4</b> //////////////////////////////////// | 8,980 //          | /10,7        | 767. 7/1              | 12,573        | /14,36         | 59% //:       | 17,96 |
| ů.              | 4.5%              |                    | 451        | 903         |               | 1,805     | 3,60         | 9            | 5,414               | 7,21           | 9   | 9,024             | 10,82        | 28 1                  | 12,633        | 14,43          | 38 :          | 18,04 |
| Ă               | ///5.0%/          | ////               | /454 //,   | ///,907     |               | /,1,813// | //3,62       | 7/1.//       | 5,440//             | //7,25         | 3/////  | 9,067//           | 10,8         | 80% 7/1               | 12,693        | /14,50         | 37/2//        | 18,13 |
| щ               | 5.5%              |                    | 456        | 912         |               | 1,822     | 3,64         | 4            | 5,466               | 7,28           | 8   | 9,110             | 10,9         | 32 1                  | 12,754        | 14,57          | 76 :          | 18,22 |
| ß               | ////6.0%/         | []].[]             | 458 //     | ///916      |               | //1,831// | //3,66       |              | 5,492               | //7,32         |   | 9,153 //          | / 10,98      | 84% 7/1               | 12,814        | /14,64         | 15/2//        | 18,30 |
| Ā               | 6.5%              |                    | 460        | 920         |               | 1,839     | 3,67         |              | 5,518               | 7,35           |   | 9,196             | 11,0         |                       | L2,875        | 14,71          |               | 18,39 |
| COARSE          | ////7.0%/         | 11.11              | 462 //     | ///924      |               | //1,848// | // 3,69      |              | 5,544               | 17,39          |   | 9,239//           | // 11,0      |                       | LZ,935%       | 14,78          |               | 18,47 |
| 0               | 7.5%              |                    | 464        | 929         |               | 1,857     | 3,71         |              | 5,570               | 7,42           |   | 9,283             | 11,13        |                       | 12,996        | 14,89          |               | 18,56 |
|                 | ////8.0%          | ([],[]             | /.467///.  | ///933      | 112 9         | 1,865     | //,3,73      |              | 5,595 //<br>NE MOIS | 7,46<br>TURE C |   | 9,326 //.<br>IT % | //11,19      | 12/21                 | 13,056        | 14,92          | 21% [2]       | 18,65 |
|                 | COARSE %          | 0.0%               | 0.5%       | 1.0%        | 1.59          | % 2.0%    | 2.5%         | 3.0%         |                     | 4.0%           | 4.5%  | 5.0%              | 5.5%         | 6.0%                  | 6.5%          | 7.0%           | 8.0%          | 9.0   |
| ~               | 0.0%              | 39                 | 38         | 38          | 37            |           | 36           | 35           | 34                  | 34             | 33  | 32                | 31           | 31                    | 30            | 29             | 28            | 2     |
| CY]             | //1.0%///         | //31/              | ///16//    | //36//,     | <i>1/,</i> ás | ///34//   | //34//       | //35/        | //32//,             | //31//         | //31//  | //30//            | //29//       | //29//                | //28//        | 1/21//         | //26/         | 1/2   |
|                 | 1.5%              | 36                 | 35         | 35          | 34            |           | 33           | 32           | 31                  | 30             | 30  | 29                | 28           | 28                    | 27            | 26             | 25            | 23    |
| per             | //2.0%///         | //35/              | ///34//    | //34//      | //33          |           | /31//        | //31/        | //30//,             | //29//         | //29//  | //28//            | //121//      | 1/20/1                | //26//        | //25//         | //24//        | //2   |
| S               | 2.5%              | 34                 | 33         | 33          | 32            |           | 30           | 30           | 29                  | 28             | 28  | 27                | 26           | 26                    | 25            | 24             | 23            | 2:    |
| WATER (Gallons  | //3.0%///         | //39/              | //32//     | 1/32//      | /31           |           | //29//       | //29/        | //28//              | /21//          | //27//  | //26//            | 1/15/1       | //24//                | //24//        | //23//         | //22//        | //20  |
| Ĭ               | 3.5%              | 32                 | 31         | 30          | 30            |           | 28           | 28           | 27                  | 26             | 26  | 25                | <b>Z4</b>    | 23                    | 23            | 22             | 21            | 19    |
| 0               | //4,0%///         | //śi//             | ///30//    | //29//      | //29          |           | //27///      | //21//       | //26//              | //25//         | //25//  | //24//            | //23//       | //22//                | 1/22/1.       | //////         | //20//        | //1   |
| 5               | 4.5%              | 30<br>(//:56/)     | 29         | 28          | 28<br>//iii   |           | 26           | 26           | 25                  | 24             | 23  | 23                | 22<br>////// | 21                    | 21            | 20             | 19            | 17    |
| Hin I           | //5.0%///         | //29//             | 28//       | //27///     | //27          | _         | //25///      | //25//       | 24//                | //23//         | //22//  | //22//            | //21//,      | //20//                | //20//,       | //19//         | //18/         | ///10 |
| F               | 5.5%<br>//6.0%/// | 28<br>//ź7//       | 27         | 26          | 26<br>//25    |           | 24<br>//23// | 24<br>//22// | 23                  | 22<br>//21//   | 21  | 21                | 20<br>//19// | 19                    | 19            | 18             | 16            | 19    |
| >               | 6.5%              | 26                 | 25         | 24          | 24            | _         | 22           | 21           | 21                  | 20             | 19  | 19                | 18           | / <u>/18</u> //<br>17 | //18///<br>17 | 17//           | 1/15//        | 13    |
| >               | 0.37<br>//7.0%//  | 20                 | 23         | 24          | <br>//23      |           | /21//        | //20//       | 21                  | 20             | 19  | 19                | 18           | 1/                    | 1/            | 16             | 14<br>//13//  | 1:    |
|                 | 7.5%              | <u>//25/</u><br>24 | 23         | 22          | 21            |           | 20           | 19           | 19                  | 18             | 17  | 17                | 16           | 15                    | 14            | 14             | 12            | 1:    |
|                 | //8.0%//          | //23/              |            | <br>//21/// | 21<br>/20     | _         | 20           | //18/        | 19                  | 10             | //16//  | 16/               | 10           | //14//                | //13//        | 14<br>[/]13[]] | 12            |       |
|                 |                   | 1                  |            |             |               |           |              |              |                     |                |   |                   |              |                       |               |                |               | 1000  |
|                 | Admixtur          |                    | Lithium (a |             |               | AMEX 210  |              | WRDA         |                     |                |   |                   |              |                       |               |                |               |       |
|                 | oz/CY:            |                    | n/a        | 1           |               | 0         |              | 26           | 5                   |                |   |                   |              |                       |               |                |               |       |

### CONCRETE BATCH SHEET

Note: If lithium is used in the mix, it's included in water calculations.



# WYOMING DEPARTMENT OF TRANSPORTATION Daily Concrete Placing Report

| Repo   |  | <u>1                                    </u>  | Ī   | Mix Design  | Informatio              | n                       |  |   |  |  |  |  |
|--|--|---|---|---|-------------------------|-------------------------|--|---|--|--|--|--|
| Date Pla   | ced: 8/31  | /2018   |   | Concrete 0  | lass:                   | Α                       | Cement (lb/  | /CY): 526   |  |  |  |  |
| Project  | : No: B12  | 3456  |   |   |                         |                         | Fly Ash (lb  | /CY) 132  |  |  |  |  |
| Resident Engin   | ieer: A B  | aker  | Fine  | Agg Absorp  | tion: 0.8               | 3%                      | Fine Aggregate (lb/CY): 1171   |   |  |  |  |  |
| Engineer's To  | own: Any   | town  | Coarse  | Agg Absorp  | tion: 1.1               | 5%                      | Coarse Aggregate (lb/  | (CY): 1727  |  |  |  |  |
| Supp   | olier: ABC C   | oncrete   | :rete   |   |                         |                         |  |   |  |  |  |  |
|  |  | Po  | our Sum   | mary  |                         |                         |  | 2.06  |  |  |  |  |
| Total Batched Toda   | av = 60.0  | Total Placed Previo   | us = 0  | cation, Description & Weather Info:                               |                         |                         |  |   |  |  |  |  |
| Total Was  | <u> </u>   | Total Placed to Da  |   | 5.0   |                         | butments 1 & 2 wing wal |  |   |  |  |  |  |
| Total Placed Toda  |  |   |   |   | Calm                    |                         |  |   |  |  |  |  |
|  |  | Ľ   | oads Te   | sted  | -1479-0-                | -                       |  |   |  |  |  |  |
| General Load   | Information  |   | Batch Info  |   | • • • • • • • • • • • • |                         | Test Re  | sults   |  |  |  |  |
| Ticket #   | 1  | Water (batch, gal)  | 290   | Batch In  | Admixture               | s (oz)                  | Test Number  | QC-SC-A-1   |  |  |  |  |
|  | Abutment 1, west   | Water (added, gal)  | 15  | Tolerance?  | AMEX 210                | 30                      | Slump (in)   | 4.25  |  |  |  |  |
| Load Placed Location:  | wing wall  | Fine Aggregate (lb)   | 12050   | Yes   | WRDA 64                 | 26                      | Air (%)  | 3.50%   |  |  |  |  |
| Fine Agg Moisture:   | 3.0%   | Coarse Agg (lb)   | 17610   | Yes   |                         |                         | Density (pcf)  | 143.5   |  |  |  |  |
| Coarse Agg Moisture:   | 2.0%   | Cement (lb)   | 5260  |   |                         |                         | Temperature (F)  | 75  |  |  |  |  |
| Time Batched:  | 1:00 PM  | Fly Ash(lb)   | 1320  | Yes   |                         |                         | W/(C+FA) Ratio   | 0.45  |  |  |  |  |
| Time Placed:   | 1:30 PM  |   |   | r   |                         |                         | # Cylinders Cast   | 5   |  |  |  |  |
| Load Size (CY):  | 10.0   |   |   |   |                         |                         | Tester Name/Cert #   | F. Darcy #123   |  |  |  |  |
|  | of spec. Test taken half   | way through load, last fiv  | e yards rej   | ected, next l   | oad will be             | tested                  | · · ·  |   |  |  |  |  |
| General Load   | Information  | Load  | Batch Info  | ormation  |                         |                         | Test Re  | sults   |  |  |  |  |
| Ticket #   | 2  | Water (batch, gal)  | 290   | Batch In  | Admixture               | s (az)                  | Test Number  | QC-SC-A-2   |  |  |  |  |
| Load Placed Location:  | Abutment 1, west   | Water (added, gal)  | 15  | Tolerance?  | AMEX 210                | 45                      | Slump (in)   | 4.50  |  |  |  |  |
|  | ving wall  | Fine Aggregate (Ib)   | 12050   | Yes   | WRDA 64                 | 26                      | Air (%)  | 4.70%   |  |  |  |  |
| V  |  | Coarse Agg (lb)   | 17610   | Yes   |                         |                         | Density (pcf)  | 144.1   |  |  |  |  |
| Fine Agg Moisture:   | 3.0%   | COBISE ARK (ID)   |   |   |                         |                         | Temperature (F)  | 78  |  |  |  |  |
| Fine Agg Moisture:   | 3.0%<br>2.0%   | Coarse Agg (ib)<br>Cement (ib)  | 5260  | Voc   |                         |                         | Temperature (F)  | 78  |  |  |  |  |
| Fine Agg Moisture:   |  | ÷ i   | 5260<br>1320  | Yes   |                         |                         | W/(C+FA) Ratio   | 0.45  |  |  |  |  |
| V<br>Fine Agg Moisture:<br>Coarse Agg Moisture:  | 2.0%   | Cement (lb)   |   | Yes   |                         |                         |  | <i>0.45</i><br>5  |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):   | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0   | Cement (lb)<br>Fly Ash(lb)  | 1320  |   |                         |                         | W/(C+FA) Ratio   | 0.45  |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):   | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0   | Cement (lb)   | 1320  |   | ment, air in            | spec.                   | W/(C+FA) Ratio<br># Cylinders Cast   | <i>0.45</i><br>5  |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):<br>Remarks: Dosed on site<br>General Load   | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air  | Cement (Ib)<br>Fly Ash(Ib)<br>entrainer, reved 75 time<br>Load  | 1320<br>s before sta  | arting place  | ment, air in            | spec.                   | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Re  | 0.45<br>5<br>F. Darcy #123<br>sults   |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):<br>Remarks: Dosed on site<br>General Load<br>Ticket #   | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6  | Cement (lb)<br>Fly Ash(lb)<br>entrainer, reved 75 time<br>Load<br>Water (hatch, gal)  | 1320<br>s before sta<br>l Batch Info<br>300                                 | arting places<br>prmation<br>Batch In                             | Admixture               | s (oz)                  | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #   | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3  |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):<br>Remarks: Dosed on site<br>General Load<br>Ticket #   | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6  | Cement (Ib)<br>Fly Ash(Ib)<br>entrainer, reved 75 time<br>Load<br>Water (batch, gal)<br>Water (added, gal)  | 1320<br>s before sta<br>l Batch Info<br>300<br>10                           | arting place<br>prmation<br>Batch In<br>Tolerance?                |                         | s (oz)<br>45            | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Re<br>Test Number<br>Slump (in)   | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3<br>5.00                                    |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):<br>Remarks: Dosed on site<br>General Load<br>Ticket #   | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6  | Cement (Ib)<br>Fly Ash(Ib)<br>entrainer, reved 75 time<br>Load<br>Water (batch, gal)<br>Water (added, gal)<br>Fine Aggregate (Ib)                                   | 1320<br>s before sta<br>Batch Info<br>300<br>10<br>12050                    | arting places<br>prmation<br>Batch In                             | Admixture               | s (oz)                  | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Re<br>Test Number   | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3  |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):<br>Remarks: Dosed on site<br>General Load<br>Ticket #   | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6<br>Abutment 2, east wing<br>wall<br>3.0%                               | Cement (Ib)<br>Fly Ash(Ib)<br>entrainer, reved 75 time<br>Load<br>Water (batch, gal)<br>Water (added, gal)  | 1320<br>s before sta<br>l Batch Info<br>300<br>10                           | arting place<br>prmation<br>Batch In<br>Tolerance?                | Admixture               | s (oz)<br>45            | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Re<br>Test Number<br>Slump (in)   | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3<br>5.00                                    |  |  |  |  |
| Fine Agg Moisture: Coarse Agg Moisture: Time Batched: Time Placed: Load Size (CY): Cemarks: Dosed on site General Load Ticket # Load Placed Location: Fine Agg Moisture: Coarse Agg Moisture:                            | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6<br>Abutment 2, east wing<br>wall<br>3.0%<br>2.0%                       | Cement (Ib)<br>Fly Ash(Ib)<br>entrainer, reved 75 time<br>Load<br>Water (batch, gal)<br>Water (added, gal)<br>Fine Aggregate (Ib)                                   | 1320<br>s before sta<br>l Batch Info<br>300<br>10<br>12050<br>17610<br>5260 | arting places<br>armation<br>Batch In<br>Tolerance?<br>Yes<br>Yes | Admixture               | s (oz)<br>45            | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Number<br>Slump (in)<br>Air (%)   | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3<br>5.00<br>4.80%                           |  |  |  |  |
| Fine Agg Moisture:<br>Coarse Agg Moisture:<br>Time Batched:<br>Time Placed:<br>Load Size (CY):<br>Remarks: Dosed on site<br>General Load<br>Ticket #<br>Load Placed Location:<br>Fine Agg Moisture:                      | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6<br>Abutment 2, east wing<br>wall<br>3.0%                               | Cement (lb)<br>Fly Ash(lb)<br>entrainer, reved 75 time<br>Load<br>Water (batch, gal)<br>Water (added, gal)<br>Fine Aggregate (lb)<br>Coarse Agg (lb)                | 1320<br>s before sta<br>l Batch Info<br>300<br>10<br>12050<br>17610         | arting places<br>armation<br>Batch In<br>Tolerance?<br>Yes        | Admixture               | s (oz)<br>45            | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Number<br>Slump (in)<br>Air (%)<br>Density (pcf)                                      | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3<br>5.00<br>4.80%<br>144                    |  |  |  |  |
| Fine Agg Moisture: Coarse Agg Moisture: Time Batched: Time Placed: Load Size (CY): Remarks: Dosed on site General Load Ticket # Load Placed Location: Fine Agg Moisture: Coarse Agg Moisture: Time Batched: Time Placed: | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6<br>Abutment 2, east wing<br>wall<br>3.0%<br>2.0%<br>3:00 PM<br>3:25 PM | Cement (lb)<br>Fly Ash(lb)<br>entrainer, reved 75 time<br>Load<br>Water (batch, gal)<br>Water (added, gal)<br>Fine Aggregate (lb)<br>Coarse Agg (lb)<br>Cement (lb) | 1320<br>s before sta<br>l Batch Info<br>300<br>10<br>12050<br>17610<br>5260 | arting places<br>armation<br>Batch In<br>Tolerance?<br>Yes<br>Yes | Admixture               | s (oz)<br>45            | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Re<br>Test Number<br>Slump (in)<br>Air (%)<br>Density (pcf)<br>Temperature (F)        | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3<br>5.00<br>4.80%<br>144<br>80<br>0.46<br>5 |  |  |  |  |
| V Fine Agg Moisture: Coarse Agg Moisture: Time Batched: Time Placed: Load Size (CY): Remarks: Dosed on site General Load Ticket # Load Placed Location: Fine Agg Moisture: Coarse Agg Moisture: Time Batched:            | 2.0%<br>1:20 PM<br>1:55 PM<br>10.0<br>e with 15 ounces of air<br>Information<br>6<br>Abutment 2, east wing<br>vall<br>3.0%<br>2.0%<br>3:00 PM            | Cement (lb)<br>Fly Ash(lb)<br>entrainer, reved 75 time<br>Load<br>Water (batch, gal)<br>Water (added, gal)<br>Fine Aggregate (lb)<br>Coarse Agg (lb)<br>Cement (lb) | 1320<br>s before sta<br>l Batch Info<br>300<br>10<br>12050<br>17610<br>5260 | arting places<br>armation<br>Batch In<br>Tolerance?<br>Yes<br>Yes | Admixture               | s (oz)<br>45            | W/(C+FA) Ratio<br># Cylinders Cast<br>Tester Name/Cert #<br>Test Number<br>Slump (in)<br>Air (%)<br>Density (pcf)<br>Temperature (F)<br>W/(C+FA) Ratio | 0.45<br>5<br>F. Darcy #123<br>sults<br>QC-SC-A-3<br>5.00<br>4.80%<br>144<br>80<br>0.46      |  |  |  |  |

**T-110** 

Concrete Cylinder Transmittal

|                           | )                     |             |             |                     |          |                             |  |                      |                   |                              |  |  |  |
|---------------------------|-----------------------|-------------|-------------|---------------------|----------|-----------------------------|--|----------------------|-------------------|------------------------------|--|--|--|
|                           | Project No.           |             | B12345      |                     |          |                             | F  | iel                  | d Report No       | 1                            |  |  |  |
|                           | nt Engineer           |             | A Bake      |                     |          |                             | Date Placed 8/31/2018  |                      |                   |                              |  |  |  |
|                           | te Supplier           |             | ABC Conc    |                     |          |                             |  | Concrete Class A     |                   |                              |  |  |  |
| Test                      | ing Agency            |             | None        |                     |          | Lab Mix Design No. 2018-001 |  |                      |                   |                              |  |  |  |
| Teste                     | er/Cert no.           |             | F. Darcy #  | 123                 |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       |             |             |                     |          |                             | The state is the state of the s |                      |                   |                              |  |  |  |
|                           |                       |             |             |                     | /lix Des | -                           | This Load  |                      | Stockpile         | Absorption                   |  |  |  |
| ltem                      |                       | Source      | . (         | (Y/N) 1 CY Batch    |          |                             | 10 CY  |                      | Moisture          |                              |  |  |  |
| Crs Agg (Pit Nan          | ·                     | Arm Pit     | -           | <u>N</u> <u>526</u> |          |                             | 17610  | -                    | 2.0%              | 0.01152                      |  |  |  |
| Fine Agg (Pit Nan         | ·                     | Best Pit    | <u> </u>    | <u>N</u>   -        | 1727     | _                           | 12050  | -                    | 3.0%              | 0.00827                      |  |  |  |
| Cement/Typ                |                       | Holcim I-II |             | -                   | 526      | _                           | 5260   | -                    |                   | Matan Add d On               |  |  |  |
| Fly Ash/Cla<br>Silica Fun |                       |             |             | -                   | 132      |                             | 1320   | -                    |                   | Water Added On               |  |  |  |
|                           | Water City of Anytown |             |             | .   -               |          |                             | - 200  | -                    |                   | Site                         |  |  |  |
| vvat                      | er City               | of Anytow   | n   -       | <u>N</u>            |          | Í                           | 290  | -                    |                   | 15                           |  |  |  |
|                           |                       |             |             | I                   |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       | A           | dmixtures   |                     |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       |             | - 1         | Plant, I            |          |                             | ite, Load:   |                      | Water/Cer         | ment Ratio 0.56              |  |  |  |
|                           | Product N             |             |             | Tota                | Oz       | T                           | otal Oz  |                      | Water/Cer         | menticious 0.45              |  |  |  |
|                           | AMEX 2                |             |             | 30                  | )        | 0                           |  |                      |                   |                              |  |  |  |
|                           | WRDA 64               |             |             |                     |          |                             | 0  |                      |                   | CRETE PLACED                 |  |  |  |
|                           |                       |             |             |                     |          |                             |  |                      | To La             |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  |                      | This Repo         |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  |                      | Tot               | al <u>55</u> yd <sup>3</sup> |  |  |  |
| Ger                       | eral Pour L           | ocation,    |             |                     |          |                             |  | _                    |                   |                              |  |  |  |
|                           |                       |             | tructure X  | YZ. Abuti           | ments 1  | L & 2 w                     | ing walls, L   | .ov                  | //High 46/75, C   | alm                          |  |  |  |
|                           |                       |             |             | ,                   |          |                             | <u> </u>   |                      |                   |                              |  |  |  |
|                           | Placed                | Location A  | butment 1   | l, west w           |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       | A           | ir test out | of spec.            | Test ta  | ken ha                      | lfway throu  | ıgh                  | load, last five y | /ards rejected, next         |  |  |  |
|                           | 1                     | Remarks Ic  | oad will be | tested.             |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  |                      |                   |                              |  |  |  |
| Cylinder                  |                       | ne          | Slump       | Air                 |          | nit Wt                      | Temp   | Requested Testing Ag |                   | Remarks                      |  |  |  |
| Number                    | Batched               | Placed      | (in)        | (%)                 | (11      | os/yd)                      | (F)  |                      | (Days)            | Nemarks                      |  |  |  |
| 1                         | 1:00                  | 1:30        | 4.25        | 3.5%                |          | .43.5                       | 75   |                      | 3                 |                              |  |  |  |
| 2                         | 1:00                  | 1:30        | 4.25        | 3.5%                |          | 43.5                        | 75   |                      | 5                 |                              |  |  |  |
| 3                         | 1:00                  | 1:30        | 4.25        | 3.5%                |          | .43.5                       | 75   |                      | 28                |                              |  |  |  |
| 4                         | 1:00                  | 1:30        | 4.25        | 3.5%                |          | 43.5                        | 75   |                      | 28                |                              |  |  |  |
| 5                         | 1:00                  | 1:30        | 4.25        | 3.5%                | 6 1      | 43.5                        | 75   |                      | 28                |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  | <b>_</b>             |                   |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       |             | ļ           |                     |          |                             |  | L                    |                   |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  | <u> </u>             |                   |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       |             |             |                     |          |                             |  |                      |                   |                              |  |  |  |
|                           |                       |             | 1           | 1                   | 1        |                             |  |                      |                   |                              |  |  |  |

Concrete Cylinder Transmittal

| A Baker       Date Placed       8/31/2018         Concrete Supplier       ABC Concrete       Date Placed       8/31/2018         Concrete Supplier       ABC Concrete       Class       A         Testing Agency       None       Lab Mix Design No.       2018-001         Tester/Cert no.       F. Darcy #123       Date Placed       8/31/2018         Item       Source       Lab Mix Design No.       2018-001         Tester/Cert no.       F. Darcy #123         Heated       Mix Design This Load       Stockpile       Absorption         Concrete Class       A         Mater Mix Design This Load       Stockpile       Absorption         Tester/Cert Name       Heated       Mix Design No.       2.0%       0.00827         Fire Agg (Pit Name)       Arm Pit       N       2.0%       Water Added On         Site Total Oz       Total Oz       Total Oz <th co<="" th=""><th>GERALFTMENT</th><th>)</th><th></th><th></th><th></th><th></th><th></th><th colspan="6">Field Report No. 1</th></th>  | <th>GERALFTMENT</th> <th>)</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th colspan="6">Field Report No. 1</th> | GERALFTMENT  | )           |             |              |          |                    |                           | Field Report No. 1 |                 |                   |  |  |  |
|---|---|--------------|-------------|-------------|--------------|----------|--------------------|---------------------------|--------------------|-----------------|-------------------|--|--|--|
| Concrete Supplier       ABC Concrete       Concrete Class       A         Testing Agency       None       Lab Mix Design No.       2018-001         Tester/Cert no.       F. Darcy #123       Lab Mix Design No.       2018-001         Item       Source       Heated       Mix Design:       This Load       Moisture       Absorption         Crs Agg (Pit Name)       Best Pit       N       526       5260       3.0%       0.01152         Cement/Type       Holcim       I-II       N       526       5260       3.0%       0.00827         Cement/Type       Holcim       I-II       Silica Fume       Water Added On       Site       Made       Site         Water       City of Anytown       N       2290       Instance       Water/Cement Ratio       0.56         WRDA 64       26       15       ConCRETE PLACED       Made       On Site       ConCRETE PLACED       Made         General Pour Location,       Description & Abutment 1, west wing wall       Dosed on site with 15 ounces of air entrainer, reved 75 times before starting Remarks placement, air in spec.       Placed Location Abutment 1, west wing wall         Description & Batched       Placed       A:r       A:r       Made       Remarks <td></td> <td>•</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td colspan="6"></td>  |   | •            |             |             |              |          |                    |                           |                    |                 |                   |  |  |  |
| Item Source         Lab Mix Design No. 2018-001           Item Source         Main Design No. 2018-001           Item Source         Main Design: This Load 10 CY         Mone Moisture         Absorption           Creating (Pt Name)         Arm Pit N         Sign No. 2018-001           Fine Agg (Pt Name)         Arm Pit N         N         Stockpile Moisture         Absorption           Cement/Type Holcim I-II         N         Stockpile Stockpile Moisture         Absorption           Stockpile Moisture         Abdmixtures           Product Name         Plant, Load: On Site, Load: Total Oz         Total Oz         Total Oz         Water/Cement Ratio         0.56           MURD 64         290         Water/Cement Ratio         0.56           Mater Xurees           Admixtures         Plant, Load: Total Oz         Total Oz           MRDA 64         2         CONCRETE PLACED           Colspan="2">Colspan="2" <th colspa<="" td=""><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td colspan="6"></td></th>  | <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td colspan="6"></td>                              |              | -           |             |              |          |                    |                           |                    |                 |                   |  |  |  |
| Tester/Cert no.       F. Darcy #123         Item       Source       Iteated       Mix Design:       This Load       Stockpile       Absorption         Crs Agg (Pit Name)       Arm Pit       N       526       17610       2.0%       0.01152         Grs Agg (Pit Name)       Best Pit       N       526       5260       3.0%       0.00827         Cement/Type       Holcim       I-II       Size       1320       3.0%       0.00827         Fly Ash/Class       Bridger       F       132       1320       3.0%       0.00827         Silica Fume       Gridger       F       132       1320       3.0%       0.00827         Water       City of Anytown       N       290       Image (Structure Added On Site)       Site         Water       Mix Dasid       On Site, Load:       Total Oz       Image (Structure Added On Site)       Site         WRDA 64       26       Image (Structure Added On Site)         General Pour Location,       45       15       CONCRETE PLACED       Image (Structure Added On Site)       Image (Structure Added On Site)         Description & Weather Info  |   |              |             |             |              |          |                    |                           |                    |                 |                   |  |  |  |
| Item         Source         Heated<br>(Y/N)         Mix Design:<br>1 CY Batch         This Load<br>10 CY         Moisture<br>Moisture         Absorption           Crs Agg (Pit Name)         Arm Pit         N         526         17610         2.0%         0.01152           Cement/Type         Holcim         I-II         N         526         5260         3.0%         0.00827           Cement/Type         Holcim         I-II         N         526         5260         3.0%         0.00827           Silica Fume         III         N         526         5260         3.0%         0.00827           Water         City of Anytown         N         IIII         290         IIIII         Silica Fune           Water         City of Anytown         N         IIIIII         IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII   |   |              |             |             |              | <u> </u> |                    | Lab Mix Design No2018-001 |                    |                 |                   |  |  |  |
| Item         Source         (Y/N)         1 CY Batch         10 CY         Moisture         Absorption           Crs Agg (Pit Name)         Arm Pit         N         526         17610         2.0%         0.01152         0.00827           Cement/Type         Holcim         I-II         N         526         5260         3.0%         0.00827           Fly Ash/Class         Bridger         F         132         1320         0.00827         0.00827           Silica Fume         Mater         City of Anytown         N         290         15         0.00827           Water         City of Anytown         N         290         15         0.00827         0.00827           Water Added On         Site         132         1320         1320         15         0.0%         0.155           Water Added On         Site         Commode         Total Oz         Total Oz         15         0.45         0.45           AMEX 210         45         15         15         0         70         16         0.45         0.43           Description & Weather Info         Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm         0.064 on site with 15 ounces of air entrainer, reved 75 times before starting Remarks <t< td=""><td>Teste</td><td>er/Cert no.</td><td></td><td>F. Darcy #</td><td><i>‡</i>123</td><td></td><td></td><td colspan="6"></td></t<>  | Teste   | er/Cert no.  |             | F. Darcy #  | <i>‡</i> 123 |          |                    |                           |                    |                 |                   |  |  |  |
| Item         Source         (Y/N)         1 CY Batch         10 CY         Moisture         Absorption           Crs Agg (Pit Name)         Arm Pit         N         526         17610         2.0%         0.01152         0.00827           Cement/Type         Holcim         I-II         N         526         5260         3.0%         0.00827           Fly Ash/Class         Bridger         F         132         1320         0.00827         0.00827           Silica Fume         Mater         City of Anytown         N         290         15         0.00827           Water         City of Anytown         N         290         15         0.00827         0.00827           Water Added On         Site         132         1320         1320         15         0.0%         0.155           Water Added On         Site         Commode         Total Oz         Total Oz         15         0.45         0.45           AMEX 210         45         15         15         0         70         16         0.45         0.43           Description & Weather Info         Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm         0.064 on site with 15 ounces of air entrainer, reved 75 times before starting Remarks <t< td=""><td></td><td></td><td></td><td></td><td></td><td>Min Dec</td><td>ion. I</td><td><b>T</b>L <b>1</b></td><td>_</td><td>Ctaskuila</td><td></td></t<>   |   |              |             |             |              | Min Dec  | ion. I             | <b>T</b> L <b>1</b>       | _                  | Ctaskuila       |                   |  |  |  |
| Crs Agg (Pit Name)         Arm Pit         N         526         17610         2.0%         0.01152           Fine Agg (Pit Name)         Best Pit         N         526         5260         3.0%         0.00827           Cement/Type         Holcim         I-II         526         5260         3.0%         0.00827           Silica Fume         Bridger         F         132         1320         1320         1320           Water         City of Anytown         N         Total Oz         Total Oz         Total Oz         Total Oz           AMEX 210         45         15         15         15         0.00827         Water/Cement Ratio         0.56           WRDA 64         26         15         15         0         yd³         Total Oz         0         yd³           General Pour Location,         26         -         -         -         -         -         0         yd³           Description & Weather Info         Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm         -         -         -         -         -         -         -         -         -         <   | ltem  |              | Source      |             |              |          | -                  |                           |                    |                 | Absorption        |  |  |  |
| Fine Agg (Pit Name)         Best Pit         N         1727         12050         3.0%         0.00827           Cement/Type         Holcim         I-II         Sile         Sile         Sile         Water Added On         Sile           Silica Fume   |   |              |             |             |              |          |                    |                           | -+                 |                 | 0.01152           |  |  |  |
| Cement/Type       Holcim       I-II         Fly Ash/Class       Bridger       F         Silica Fume   |   |              |             | —   ·       |              |          |                    |                           | ·                  |                 |                   |  |  |  |
| Fly Ash/Class       Bridger       F         Silica Fume   |   |              |             | <u></u>   · | <u> </u>     |          |                    |                           | ·                  |                 | - 0.00027         |  |  |  |
| Silica Fume   |   |              |             |             |              |          |                    |                           | ·                  |                 | Water Added On    |  |  |  |
| Water       City of Anytown       N       290       15         Admixtures         Admixtures         Product Name       Plant, Load:       On Site, Load:       Water/Cement Ratio       0.56         MEX 210       45       15       CONCRETE PLACED         MRDA 64       26       To Last       0       yd³         This Report       55       yd³       Total       55       yd³         General Pour Location,       Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm       Placed Location       Abutment 1, west wing wall         Dosed on site with 15 ounces of air entrainer, reved 75 times before starting placement, air in spec.       Remarks       Remarks       Remarks         1       1:20       1:55       4.5       4.7%       144.1       78       E  | • •   |              |             | <u> </u>    |              |          | -                  |                           | ·                  |                 |                   |  |  |  |
| Admixtures         Product Name       Plant, Load:<br>Total Oz       On Site, Load:<br>Total Oz       Water/Cement Ratio       0.56         MEX 210       45       15         WRDA 64       26       Total Oz       Total Oz         WRDA 64       26       Total Oz       Total Oz         Total Oz       45       15       CONCRETE PLACED         WRDA 64       26       Total S       yd³         This Report       55       yd³         General Pour Location,<br>Description & Weather Info       Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm         Placed Location       Abutment 1, west wing wall       Dosed on site with 15 ounces of air entrainer, reved 75 times before starting Remarks placement, air in spec.         Cylinder       Time       Slump       Air       Unit Wt       Temp (Øays)       Remarks         1       1:20       1:55       4.5       4.7%       144.1       78       Image: Comp (Carrier Carrier Carr  |   | 1            |             | n l         | N            |          | -                  | 290                       | ·                  |                 |                   |  |  |  |
| Plant, Load:       On Site, Load:       Water/Cement Ratio       0.56         AMEX 210       45       15         WRDA 64       26   |   |              |             | ·····   ·   | <u> </u>     |          |                    |                           | ·                  |                 |                   |  |  |  |
| Plant, Load:       On Site, Load:       Water/Cement Ratio       0.56         AMEX 210       45       15         WRDA 64       26   |   |              | ^           | desixturo   |              |          |                    |                           |                    |                 | 1                 |  |  |  |
| Product Name         Total Oz         Total Oz         Total Oz         Water/Cementicious         0.45           AMEX 210         45         15         15         Image: Concentry of the second  |   |              | anixure     |             | Load:        |          | ite Load:          |                           | Mator/Con          | nont Patio 0.56 |                   |  |  |  |
| AMEX 210       45       15         WRDA 64       26       15         CONCRETE PLACED       To Last       0       yd³         This Report       55       yd³         General Pour Location,<br>Description & Weather Info       Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm         Placed Location       Abutment 1, west wing wall         Dosed on site with 15 ounces of air entrainer, reved 75 times before starting Remarks placement, air in spec.         Cylinder       Time         Number       Batched       Placed         1       1:20       1:55       4.5       4.7%         2       1:20       1:55       4.5       4.7%       144.1       78  |   | Product Name |             |             |              |          |                    | -                         |                    |                 |                   |  |  |  |
| WRDA 64       26       CONCRETE PLACED         Image: Stress of the |   |              |             |             |              |          | +                  |                           |                    |                 | menticious   0.45 |  |  |  |
| General Pour Location,  |   |              |             |             |              |          | 15                 | l ŀ                       | CONC               |                 |                   |  |  |  |
| General Pour Location,<br>Description & Weather Info       Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm         Placed Location       Abutment 1, west wing wall         Dosed on site with 15 ounces of air entrainer, reved 75 times before starting<br>placement, air in spec.         Cylinder       Time         Slump       Air       Unit Wt       Temp<br>(Ibs/yd)       Requested Testing Age<br>(Days)       Remarks         1       1:20       1:55       4.5       4.7%       144.1       78       Image: Content of the starting of the start of the s  |   | WILDA 04     |             |             |              |          |                    |                           | ╎┟                 |                 |                   |  |  |  |
| Total 55 yd³General Pour Location,<br>Description & Weather InfoStructure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, CalmPlaced LocationAbutment 1, west wing wallDosed on site with 15 ounces of air entrainer, reved 75 times before starting<br>Remarks placement, air in spec.Cylinder<br>NumberTimeSlump<br>(in)Air<br>(lbs/yd)Temp<br>(F)Requested Testing Age<br>(Days)Remarks11:201:554.54.7%144.178Image: Colspan="6">Colspan="6">Total 55yd³  | ··· ··  |              |             |             |              |          |                    | <u> </u>                  |                    |                 |                   |  |  |  |
| General Pour Location,<br>Description & Weather Info Structure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, Calm         Placed Location Abutment 1, west wing wall         Dosed on site with 15 ounces of air entrainer, reved 75 times before starting<br>Remarks placement, air in spec.         Cylinder Time Slump Air Unit Wt Temp Requested Testing Age (bays)         Number       Batched       Placed       (in)       (%)       (lbs/yd)       (F)       Requested Testing Age (Days)       Remarks         1       1:20       1:55       4.5       4.7%       144.1       78       144.1       78  |   |              |             |             |              |          |                    |                           |                    | •               |                   |  |  |  |
| Description & Weather InfoStructure XYZ, Abutments 1 & 2 wing walls, Low/High 46/75, CalmPlaced LocationAbutment 1, west wing wallDosed on site with 15 ounces of air entrainer, reved 75 times before starting<br>placement, air in spec.CylinderTimeSlumpAirUnit WtTemp<br>Requested Testing Age<br>(Days)RemarksOutputSlumpAirUnit WtTemp<br>Requested Testing Age<br>(Days)Remarks11:201:554.54.7%144.178CylinderTimeSlumpAirUnit WtTemp<br>Requested Testing Age<br>(Days)Remarks11:201:554.54.7%144.178   |   |              |             |             |              |          |                    |                           |                    |                 |                   |  |  |  |
| Placed LocationAbutment 1, west wing wallDosed on site with 15 ounces of air entrainer, reved 75 times before starting<br>placement, air in spec.Cylinder<br>NumberTime<br>BatchedSlump<br>(in)Air<br>(%)Unit Wt<br>(lbs/yd)Temp<br>(F)Requested Testing Age<br>(Days)Remarks11:201:554.54.7%144.178121:201:554.54.7%144.1781   |   |              |             |             |              |          |                    |                           |                    |                 |                   |  |  |  |
| Dosed on site with 15 ounces of air entrainer, reved 75 times before starting<br>Remarks placement, air in spec.CylinderTimeSlumpAirUnit WtTemp<br>(lbs/yd)Requested Testing Age<br>(Days)RemarksNumberBatchedPlaced(in)(%)144.17811:201:554.54.7%144.178   | Descript  | ion & Weat   | ther Info S | tructure >  | (YZ, Abu     | tments : | <u>1 &amp; 2 w</u> | ing walls, L              | ow,                | /High 46/75, Ca | alm               |  |  |  |
| Dosed on site with 15 ounces of air entrainer, reved 75 times before starting<br>Remarks placement, air in spec.CylinderTimeSlumpAirUnit WtTemp<br>(lbs/yd)Requested Testing Age<br>(Days)RemarksNumberBatchedPlaced(in)(%)144.17811:201:554.54.7%144.178   |   | _            |             |             |              |          |                    |                           |                    |                 |                   |  |  |  |
| Remarks placement, air in spec.CylinderTimeSlumpAirUnit WtTemp<br>(lbs/yd)Requested Testing Age<br>(Days)RemarksNumberBatchedPlaced(in)(%)(lbs/yd)(F)(Days)Remarks11:201:554.54.7%144.17821:201:554.54.7%144.178  |   | Placed       |             |             |              |          |                    |                           |                    | 175.1           |                   |  |  |  |
| Cylinder<br>NumberTimeSlump<br>(in)Air<br>(%)Unit Wt<br>(lbs/yd)Temp<br>(F)Requested Testing Age<br>(Days)Remarks11:201:554.54.7%144.178121:201:554.54.7%144.1781   |   |              |             |             |              |          | es or a            | ir entrainer              | , ге               | ved 75 times b  | etore starting    |  |  |  |
| Number         Batched         Placed         (in)         (%)         (lbs/yd)         (F)         Requested resting Age<br>(Days)         Remarks           1         1:20         1:55         4.5         4.7%         144.1         78   <   |   |              | Remarksjp   | lacement    | , air in sj  | ec.      |                    |                           |                    |                 |                   |  |  |  |
| Number         Batched         Placed         (in)         (%)         (lbs/yd)         (F)         Requested resting Age<br>(Days)         Remarks           1         1:20         1:55         4.5         4.7%         144.1         78   <   | Cylinder  | Tir          | 20          | Slump       |              | e   11   |                    | Tomp                      |                    |                 |                   |  |  |  |
| 1         1:20         1:55         4.5         4.7%         144.1         78           2         1:20         1:55         4.5         4.7%         144.1         78   | •   |              |             |             |              |          |                    |                           |                    |                 | Remarks           |  |  |  |
| 2 1:20 1:55 4.5 4.7% 144.1 78   |   |              |             |             | -            |          |                    |                           |                    | (Days)          |                   |  |  |  |
|   |   |              |             |             |              |          |                    |                           | -                  |                 |                   |  |  |  |
|   | 3   | 1:20         | 1:55        | 4.5         | _            |          | 144.1              | 78                        |                    |                 |                   |  |  |  |
| 4         1:20         1:55         4.5         4.7%         144.1         78   |   |              |             | 4           | _            |          |                    |                           |                    |                 |                   |  |  |  |
| 5         1:20         1:55         4.5         4.7%         144.1         78   |   |              |             |             |              |          |                    |                           |                    |                 |                   |  |  |  |
|   |   |              |             |             |              |          |                    |                           |                    |                 |                   |  |  |  |
|   |   |              |             |             |              | -+       |                    |                           |                    |                 |                   |  |  |  |
|   |   |              |             | 1           |              |          |                    |                           |                    |                 |                   |  |  |  |
|   |   |              |             | 1           |              |          |                    |                           | -                  |                 | ····              |  |  |  |
|   |   |              |             | 1           |              |          |                    |                           |                    | i               |                   |  |  |  |
|   |   |              |             |             |              |          |                    |                           |                    | 1               |                   |  |  |  |
|   |   |              |             | 1           | Î            | i        |                    |                           |                    |                 |                   |  |  |  |

Concrete Cylinder Transmittal

| DEPARTMENT                | )                     |                          |           |                             |           |           |                    |                      |                 |                  |  |  |
|---------------------------|-----------------------|--------------------------|-----------|-----------------------------|-----------|-----------|--------------------|----------------------|-----------------|------------------|--|--|
|                           | Project No.           |                          | B123      |                             |           | _         | F                  | ielo                 | d Report No     | 1                |  |  |
|                           | nt Engineer           | -                        | A Ba      |                             |           | _         |                    |                      | Date Placed     | 8/31/2018        |  |  |
|                           | te Supplier           |                          | ABC Co    |                             | -         | _         |                    |                      | ncrete Class    | A                |  |  |
|                           | ting Agency           |                          | Noi       |                             |           | _         | Lab                | Mi                   | x Design No     | 2018-001         |  |  |
| Test                      | er/Cert no.           |                          | F. Darcy  | y #123                      |           | _         |                    |                      |                 |                  |  |  |
|                           |                       |                          |           |                             |           |           |                    | _                    |                 |                  |  |  |
| 14                        |                       | 6                        |           | Heated                      | Mix De    | -         | This Load<br>10 CY |                      | Stockpile       | Absorption       |  |  |
| ltem                      |                       | Source                   |           | (Y/N) 1 CY Batch            |           |           |                    | _                    | Moisture        |                  |  |  |
| Crs Agg (Pit Nar          |                       | Arm Pit<br>Best Pit      | — I       | <u>N</u> <u>526</u><br>1727 |           |           | 17610              | -                    | 2.0%            | 0.01152          |  |  |
| Fine Agg (Pit Nar         |                       |                          | <u> </u>  |                             |           |           |                    | -                    | 3.0%            | 0.00827          |  |  |
| Cement/Ty                 | ·                     | Holcim I-II<br>Bridger F |           |                             |           |           | 5260               | -                    |                 | Water Added On   |  |  |
| Fly Ash/Cla<br>Silica Fur |                       |                          |           |                             | 13        |           | 1320               | -                    |                 |                  |  |  |
|                           | Water City of Anytown |                          |           |                             |           |           | 290                | -                    |                 | Site             |  |  |
| VVat                      | Water City of Anytown |                          | <u> </u>  |                             |           | 290       | -                  |                      | 15              |                  |  |  |
|                           |                       |                          |           |                             |           |           |                    |                      |                 |                  |  |  |
|                           |                       | Ac                       | dmixtur   |                             |           |           |                    | 11                   |                 |                  |  |  |
|                           |                       |                          |           | 1                           | nt, Load: |           | Site, Load:        | 11                   |                 | ment Ratio 0.56  |  |  |
|                           | Product N             |                          |           |                             | otal Oz   | T         | otal Oz            | 41                   | Water/Cei       | menticious 0.45  |  |  |
|                           | AMEX 2                |                          |           |                             | 45        | -         | 0                  |                      | CONCRETE PLACED |                  |  |  |
|                           | WRDA                  | 64                       |           | 26                          | -         | 0         | IJ                 |                      |                 |                  |  |  |
|                           |                       |                          |           |                             |           | -         |                    | 11                   | To La           |                  |  |  |
|                           |                       |                          |           |                             | -         |           |                    | This Repo            |                 |                  |  |  |
|                           |                       |                          |           |                             |           | -         |                    |                      | Tot             | al <u>55</u> yd³ |  |  |
| Gei                       | neral Pour L          | ocation,                 |           |                             |           |           |                    |                      |                 |                  |  |  |
| Descript                  | tion & Weat           | ther Info St             | ructure   | XYZ, Ab                     | utment    | s 1 & 2 w | ving walls, L      | .ow                  | /High 46/75, C  | alm              |  |  |
|                           |                       |                          |           |                             |           |           |                    |                      |                 |                  |  |  |
|                           | Placed                | Location A               | butmen    | it 2, east                  | wing w    | all       |                    |                      |                 |                  |  |  |
|                           |                       |                          |           |                             |           |           |                    |                      |                 |                  |  |  |
|                           |                       | Remarks A                | ll air en | trainer f                   | or loads  | 3-6 adde  | ed at the pl       | ant                  | ٠               | · <b></b> · · -  |  |  |
|                           |                       |                          | -1        |                             |           |           |                    |                      |                 |                  |  |  |
| Cylinder                  |                       | me                       | Slum      |                             |           | Unit Wt   | Temp               | Requested Testing Ag |                 | Remarks          |  |  |
| Number                    | Batched               | Placed                   | (in)      |                             |           | (lbs/yd)  | (F)                | _                    | (Days)          |                  |  |  |
| 1                         | 3:00                  | 3:25                     | 5         |                             | .8%       | 144       | 80                 |                      |                 |                  |  |  |
| 2                         | 3:00                  | 3:25                     | 5         |                             | .8%       | 144       | 80                 | <u> </u>             |                 |                  |  |  |
| 3                         | 3:00                  | 3:25                     | 5         |                             | .8%       | 144       | 80                 | -                    |                 |                  |  |  |
| 4 5                       | 3:00                  | 3:25                     | 5         |                             | .8%       | 144       | 80                 |                      |                 |                  |  |  |
|                           | 3:00                  | 3:25                     | 5         | 4.                          | .8%       | 144       | 80                 | -                    |                 |                  |  |  |
|                           | ·                     |                          |           |                             |           |           |                    | $\vdash$             |                 |                  |  |  |
|                           |                       |                          |           |                             |           |           |                    | -                    |                 |                  |  |  |
|                           |                       |                          |           |                             |           |           |                    | -                    |                 |                  |  |  |
|                           |                       |                          |           |                             |           |           |                    | $\vdash$             |                 |                  |  |  |
|                           |                       |                          |           |                             |           |           | <u> </u>           |                      |                 |                  |  |  |
|                           |                       |                          |           |                             |           |           |                    |                      |                 |                  |  |  |
| l                         |                       |                          |           |                             |           |           |                    |                      |                 |                  |  |  |

| Basic Project Info            | rmation           |
|-------------------------------|-------------------|
| Project Number:               | 8654321           |
| Project Name:                 | Bridge to Nowhere |
| Resident Engineer:            | Theodore Wells    |
| Engineer's Town:              | Rocketville       |
| Concrete Class:               | Silica Fume       |
| Max w/c-F.A. ratio:           | 0.4               |
| Fine Aggregate Source:        | Some Pit          |
| Coarse Aggregate Source:      | Other Pit         |
| Cement Type:                  | 1-11              |
| Cement Supplier/Manufacturer: | Holcim            |
| Fly Ash Class:                |                   |
| Fly Ash Source:               |                   |
| Fly Ash to Cement Ratio:      |                   |
| Silica Fume Source:           | Force 10,000 D    |
| Fiber Source:                 | Grace             |
| Concrete Supplier:            | Funtime Concrete  |
| Water Source:                 | Deep Well         |
| Is Water Potable?             | No                |
|                               |                   |

| All information can be found on the | he mix design from | 1 the Lab                |
|-------------------------------------|--------------------|--------------------------|
| Lab Mix Design #:                   | 2018-002           |                          |
| Fine Aggregate Absorption:          | 0.786%             | Enter values under 1% as |
| Coarse Aggregate Absorption:        | 0.875%             | decimal (0.5% as 0.005)  |
| Fine Aggregate (lb/CY):             | 1131               | dry weight               |
| Coarse Aggregate (Ib/CY):           | 1693               | dry weight               |
| Cement (lb/CY):                     | 658                | _                        |
| Lithium Used:                       | No                 |                          |
| Air Content Correction Factor:      |                    | %                        |
| Silica Fume Info (                  | if needed)         |                          |
| Silica Fume (lb/CY):                | 53                 |                          |
| Fibers (lb/CY):                     | 2                  |                          |
| Additives (as listed o              | on mix design)     |                          |
| Name                                | Quantity *         |                          |
| ADVA 140M                           | 20                 | oz/100 cwt               |
| WRDA 64                             | 6                  | oz/100 cwt               |
|                                     |                    | oz/100 cwt               |
|                                     |                    | oz/100 cwt               |
|                                     |                    |                          |

#### Notes (Please Read):

> Mixes with medium aggregate are not supported in this form.

> All info on this page can be entered before placement starts.

> Leave the field blank if you aren't using that source or product.

> When information is added in the "Basic Project Information" section other fields of this entire file will be populated. An error on this tab will leave fields unavailable or add unnecessary fields on other tabs.

> "Concrete Class", "Fly Ash to Cement Ratio", "Is water potable?", and "Lithium Used" have drop down menus, select from the options shown.

 "Max w/c-F.A. ratio" is auto-populated based on Class selected. For SFMC the cement plus fly ash portion includes the silica solids.
 > Assume 1:1 fly ash replacement ratio unless told otherwise.
 In-Spec Test Limits \*

|            | Min  | Max    | * These limits are auto populated    |
|------------|------|--------|--------------------------------------|
| Slump (in) | 4.0  | 8.0    | based on the class of concrete. If   |
| Air        | 4.5% | 7.5%   | necessary, other values can be input |
| Temp       | 50°F | 85 ° F | here for special mixes.              |

### CONCRETE BATCH SHEET

| 1               | CY          | 1               | 1/4        | 1/2     | ,        | 1        | 2       | Г                                       | 3        | 4       |               | 5        | 6       | Т           | 7        | 8       |                 | 10    |
|-----------------|-------------|-----------------|------------|---------|----------|----------|---------|---|----------|---------|---------------|----------|---------|-------------|----------|---------|-----------------|-------|
| ) Is            | Cement      | +               | 165        | 329     |          | 658      | 131     |   | 1974     | 263     |               | 3290     | 394     | <u> </u>    | 4606     | 526     | 4               | 6580  |
| Solids<br>(lbs) |             | 11/11           | ann        | 11111   | 1111     | (11111)  | 1110    | 100                                     | 11111    |         | 11111         | 111111   | 11111   | 111.11      | 111111   | 11111   | 100             | 0000  |
| ο Ξ             | Silica Furn | 2               | 13         | 27      | 0000     | 53       | 100     | 5                                       | 159      | 212     | 2000          | 265      | 318     | 00000       | 371      | 424     | 11111           | 530   |
|                 | Fibers      | 10/11           | 0/111      | 11111   | 1111     | 11/2/11  | 1112    |   | 18/11    | 118     |               | 10/11    | 11/12   | _           | 124/11   | 11/16   |                 | 20    |
|                 | 0.0%        |                 | 283        | 566     |          | 1,131    | 2,26    |   | 3,393    | 4,52    | 1.2.2.2.2.2.2 | 5,655    | 6,78    | _           | 7,917    | 9,04    |                 | 11,31 |
|                 | ///0.5%//   | 11.11           | 284        | 569     |          | 1,137//  | 2,27    |   | 3,410 // | //4,54  |               | 5,683    | 6,82    |             | 7,957    | 9,09    |                 | 11,36 |
|                 | 1.0%        |                 | 286        | 572     |          | 1,142    | 2,28    |   | 3,427    | 4,56    |               | 5,712    | 6,85    |             | 7,996    | 9,13    |                 | 11,30 |
|                 | ////1.5%//  | 11.93           | 287        | 574     |          | 1,148    | 2,29    |   | 3,444 // | 4,50    |               | 5,740    | 6,88    |             | 8,036    | 9,18    |                 | 11,42 |
| s)              | 2.0%        | 11091           | 289        | 577     |          | 1,154    | 2,30    |   | 3,461    | 4,61    |               | 5,768    | 6,92    |             | 8,075    | 9,22    |                 | 11,53 |
| (Ibs)           | /// 2.5% // | 11 03           | 290        | 580     |          | 1,159//  | 2,30    |   | 3,478 // | 4,63    |               | 5,796    | 6,95    | 1.1.1.1.1   | 8,115    | 9,22    |                 | 11,59 |
|                 | 3.0%        | 1191            | 291        | 583     |          | 1,165    | 2,33    |   | 3,495    | 4,66    |               | 5,825    | 6,99    |             | 8,155    | 9,31    |                 | 11,64 |
| AGGREGATE       | ////3.5%//  | 11.71           | 293        | 586     |          | 1,171    | //2,34  |   | 3,512    | 4,68    | - 2 2 - 2 2   | 5,853    | 7,02    |             | 8,194    | 9,36    |                 | 11,70 |
| A               | 4.0%        | 11-11           | 294        | 589     |          | 1,176    | 2,35    |   | 3,529    | 4,70    |               | 5,881    | 7,02    |             | 8,234    | 9,41    |                 | 11,76 |
| E               | 4.5%        | 11.71           | 296        | 591     | 1        | 1,182//  | 2,35    |   | 3,546    | 4,72    |               | 5,909    | 7,09    | 1.0.0       |          | 9,45    | 1.1.1           | 11,70 |
| R               | 5.0%        | 11 26           | 297        | 594     |          | 1,182    |         |   |          |         |               |          |         |             | 8,273    | 1       |                 |       |
| U<br>U          | 5.5%        | 11.20           |            |         |          |          | 2,37    |   | 3,563    | 4,75    | 1 4 4 4 4 4 4 | 5,938    | 7,12    |             | 8,313    | 9,50    | 1.1.1           | 11,87 |
| AC I            |             | 11.20           | 299<br>300 | 597     |          | 1,193    | 2,38    |   | 3,580 // | //4,77  |               | 5,966    | 7,15    |             | 8,352    | 9,54    |                 | 11,93 |
| ш               | 6.0%        | 11.20           |            | 600     |          | 1,199    | 2,39    |   | 3,597    | 4,79    |               | 5,994    | 7,19    |             | 8,392    | 9,59    |                 | 11,98 |
| FINE            | 7.0%        | 1.00            | 301        | 603     |          | 1,205    | //2,40  |   | 3,614 // | 4,81    |               | 6,023    | 7,22    |             | 8,432    | 9,63    |                 | 12,04 |
| Ē               | 7.0%        | 1100            | 303        | 606     | 10. 21   | 1,210    | 2,42    | 1.10                                    | 3,631    | 4,84    |               | 6,051    | 7,26    | 1.4.4.1.4.1 | 8,471    | 9,68    |                 | 12,10 |
|                 | 7.5%        | 11/2            | 304        | 608     |          | 1,216//  | //2,43  |   | 3,647 // | 4,86    | 1             | 6,079    | 7,29    |             | 8,511    | 9,72    |                 | 12,15 |
|                 | 8.0%        | 1191            | 306        | 611     |          | 1,221    | 2,44    |   | 3,664    | 4,88    | 11 11         | 6,107    | 7,32    |             | 8,550    | 9,77    |                 | 12,21 |
|                 | 8.5%        | 1101            | 307        | 614     | _        | 1,227//  | //2,45  |   | 3,681//  | //4,90  |               | 6,136 // | 7,36    |             | 8,590    | 9,81    |                 | 12,27 |
|                 | 9.0%        | _               | 308        | 617     | _        | 1,233    | 2,46    |   | 3,698    | 4,93    |               | 6,164    | 7,39    |             | 8,630    | 9,86    |                 | 12,32 |
|                 | 0.0%        | 11 32           | 423        | 847     | 19.00    | 1,693    | 3,38    |   | 5,079    | 6,77    |               | 8,465    | 10,1    |             | 11,851   | 13,54   |                 | 16,93 |
| (s              | ////1.0%//  | 11.19           | 427        | 855     |          | 1,710 // | 2,3,42  |   | 5,130 // | 6,84    | _             | 8,550 // | / 10,2  |             | 1,970    | 13,67   |                 | 17,09 |
| AGGREGATE (lbs) | 1.5%        | 11 11           | 429        | 860     | Sec. 13. | 1,718    | 3,43    |   | 5,155    | 6,87    |               | 8,592    | 10,3:   | 1.4.4.4     | 12,029   | 13,74   |                 | 17,18 |
|                 | ////2.0%//  | 11.72           | 431        | 864     |          | 1,727    | //,3,45 |   | 5,181 🕖  | 2,6,90  |               | 8,634 // | / 10,3  |             | 12,088   | 13,81   |                 | 17,26 |
|                 | 2.5%        |                 | 434        | 868     |          | 1,735    | 3,47    |   | 5,206    | 6,94    | 1             | 8,677    | 10,4    |             | L2,147   | 13,88   |                 | 17,35 |
|                 | ////3.0%//  | 1.10            | 436        | 872     | 92.75    | 1,744    | //3,48  | 1                                       | 5,231 // | 1/6,97  | 1             | 8;719%   | / 10,4  | 53///1      | 12,207// | / 13,99 | 50% <u>//</u> : | 17,43 |
| Ë               | 3.5%        |                 | 438        | 877     |          | 1,752    | 3,50    |   | 5,257    | 7,00    | 9             | 8,761    | 10,5    | 14 1        | 12,266   | 14,01   | 18 :            | 17,52 |
| R.              | ///4.0%//   | 1,11            | 440 ///    | ///881  | 91.11    | 1,761    | // 3,52 | 1////////////////////////////////////// | 5,282    | 7,04    | 3/2 /2        | 8,804    | 10,5    | 542 21      | 12,325   | 14,08   | 36              | 17,60 |
| Se l            | 4.5%        |                 | 442        | 885     |          | 1,769    | 3,53    |   | 5,308    | 7,07    | 7             | 8,846    | 10,6    | 15 1        | 12,384   | 14,15   | i3 :            | 17,69 |
| Ă               | ///.5.0%//  | [] []]          | 444 ///    | 889     | 11.11    | 1,778    | 3,55    |   | 5,333    | 7,11    | 1/2 1/2       | 8,888    | 10,6    | 56 1        | 12,444   | 14,22   | 1/ /:           | 17,77 |
| ш               | 5.5%        |                 | 446        | 894     | ·        | 1,786    | 3,57    |   | 5,358    | 7,14    |               | 8,931    | 10,7    |             | 12,503   | 14,28   | 39 :            | 17,86 |
| SS              | ////6.0%//  | [] []]          | 448 ///    | /// 898 | 11, 11   | 1,795 // | 3,58    | 97.77                                   | 5,384    | / 7,17  | 8/1/16        | 8,973    | 10,71   | 572 61      | 2,562    | 14,35   | 57/2/2          | 17,94 |
| COARSE          | 6.5%        |                 | 450        | 902     |          | 1,803    | 3,60    | 6                                       | 5,409    | 7,21    | 2             | 9,015    | 10,8    | 18 1        | 2,621    | 14,42   | 24 1            | 18,03 |
| 0               | ///7.0%//   | 1.77            | 453        | ///,906 | 1111     | 1,812    | 3,62    | 3/2//                                   | 5,435    | /27,24  | 6///          | 9,058    | 10,8    | 59 1        | 2,681    | 14,49   | 2               | 18,11 |
|                 | 7.5%        |                 | 455        | 911     |          | 1,820    | 3,64    | _                                       | 5,460    | 7,28    | 0             | 9,100    | 10,9    | 20 1        | 2,740    | 14,56   | 50 I            | 18,20 |
|                 | ///8.0%//   | 1.11            | 457///     | ///915  | 911.91   | 1,828//  | //3,65  | 7///                                    | 5,485    | 7,31    | 4/2/2         | 9,142    | 10,97   | 71          | 12,799   | 14,62   | 8               | 18,28 |
|                 | COARSE %    |                 |            |         |          |          |         | FI                                      | NE MOIS  | TURE C  | ONTEN         | Τ%       |         |             |          |         |                 |       |
|                 |             | 0.0%            | 0.5%       | 1.0%    | 1.5%     | -        | 2.5%    | 3.0%                                    | 3.5%     | 4.0%    | 4.5%          | 5.0%     | 5.5%    | 6.0%        | 6.5%     | 7.0%    | 8.0%            | 9.0   |
| ~               | 0.0%        | 37              | 36         | 36      | 35       | 34       | 34      | 33                                      | 32       | 32      | 31            | 30       | 30      | 29          | 28       | 28      | 26              | 29    |
| C               | //1.0%///   | /35//,          | //34///    | //34/// | //33//   | //32//   | //32//, | //31//                                  | //30//   | //30/// | //29//        | //28//   | //28//  | //27//      | //26//   | //25//, | //24//          | 12    |
| <u> </u>        | 1.5%        | 34              | 33         | 33      | 32       | 31       | 31      | 30                                      | 29       | 29      | 28            | 27       | 27      | 26          | 25       | 24      | 23              | 22    |
| per             | //2.0%///   | /33///          | //32//     | //32//  | //31//   | //30///  | //30//, | //29//                                  | //28//,  | //28//, | //27///       | //26//   | //26//  | /25/        | //24//   | /23//   | 1/12/           | //2   |
| s               | 2.5%        | 32              | 31         | 31      | 30       | 29       | 29      | 28                                      | 27       | 27      | 26            | 25       | 24      | 24          | 23       | 22      | 21              | 20    |
| WATER (Gallons  | /3.0%//     | /31//           | /30//      | //30//  | //29//   | //28//   | //28//  | //27//                                  | //26//   | //25//, | //25//        | 1/24/1,  | //23//  | //23//      | 1/12//   | //21//  | /20//           | //1   |
| ĭ I             | 3.5%        | 30              | 29         | 29      | 28       | 27       | 27      | 26                                      | 25       | 24      | 24            | 23       | 22      | 22          | 21       | 20      | 19              | 18    |
| ja l            | /4,0%///    | /29//           | //28//     | //28//, | //27//   | //25//,  | //26/// | //25//                                  | //24//   | //23//, | //23//        | //22///  | //21//. | //21//      | //20//   | //19//  | //18//          | //    |
| 2               | 4.5%        | 28              | 27         | 27      | 26       | 25       | 25      | 24                                      | 23       | 22      | 22            | 21       | 20      | 20          | 19       | 18      | 17              | 10    |
| R.              | //5:0%///   | /27//           | //26//     | //26//, | //25//   | //24//,  | //23//  | //23//                                  | //22//   | //21/// | //21//        | //20//   | /19/    | //19//      | //18//   | //17//  | //16//          | //1   |
| H H             | 5.5%        | 26              | 25         | 25      | 24       | 23       | 22      | 22                                      | 21       | 20      | 20            | 19       | 18      | 18          | 17       | 16      | 15              | 14    |
| S I             | 6.0%        | 25              | //24//     | //23//  | //23//   | //22//   | //21//  | //21//                                  | //20//   | //19//  | //19//        | //18//   | //11//, | //17//      | //16//   | //15//  | //14//          | 1/1   |
| 3               | 6.5%        | 24              | 23         | 22      | 22       | 21       | 20      | 20                                      | 19       | 18      | 18            | 17       | 16      | 16          | 15       | 14      | 13              | 17    |
|                 | 7.0%//      | (23/)           | //22//     | //21//, | //21//   | //20//   | //19//, | //19//                                  | //18//   | //11//  | //17//        | //16//   | //15//  | 1/15//      | //14//   | //13//, | ///             | //11  |
|                 | 7.5%        | 22              | 21         | 20      | 20       | 19       | 18      | 18                                      | 17       | 16      | 16            | 15       | 14      | 14          | 13       | 12      | 11              | 10    |
|                 | //8.0%///   | /21//           | /20//      | //19//  | //19//   | //18//   | //17//, | //17//                                  | /16/     | //15//  | //15//        | //14//.  | //19//  | //13//      | //12//   | //11//  | //10//          | ///9  |
|                 |             |                 |            | -1-0-   | 4.5      | VA 140M  |         | WRDA                                    | 50       |         |               |          |         |             |          |         |                 |       |
| 1               | Admixture   | 19 <b>  1</b> 3 | thium (o   | 7/0/11  |          |          |         |   |          |         |               |          |         |             |          |         |                 |       |

Note: If lithium is used in the mix, it's included in water calculations

Concrete Cylinder Transmittal

|                   | ')<br>Dana ila an inta |            | DCEA     | 224            |           |           | -            | : . I .I                       | Descent Ma       |                   |  |          |  |   |    |   |      |  |  |   |
|-------------------|------------------------|------------|----------|----------------|-----------|-----------|--------------|--------------------------------|------------------|-------------------|--|----------|--|---|----|---|------|--|--|---|
|                   | Project No.            |            | B654     | 321<br>e Wells |           | -         | 4            |                                | Report No.       | 1                 |  |          |  |   |    |   |      |  |  |   |
|                   | nt Engineer            |            |          |                |           | -         |              |                                | Date Placed      | <u>9/1/2018</u>   |  |          |  |   |    |   |      |  |  |   |
|                   | te Supplier            |            |          | Concrete       | 2         | -         | Lab          |                                |                  | Silica Fume       |  |          |  |   |    |   |      |  |  |   |
|                   | ing Agency             |            | No       |                |           | -         | Lao          | IVIIX                          | Design No.       | 2018-002          |  |          |  |   |    |   |      |  |  |   |
| lest              | er/Cert no.            | K          | Compt    | on #007        |           | -         |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          | Heated         | Mix De    | esign:    | This Load    | Т                              | Stockpile        | A 1               |  |          |  |   |    |   |      |  |  |   |
| ltem              |                        | Source     |          | (Y/N)          | 1 CY B    | atch      | 6 CY         | Moisture                       |                  | Absorption        |  |          |  |   |    |   |      |  |  |   |
| Crs Agg (Pit Nan  | ne) C                  | Other Pit  |          | N              | 65        | 8         | 10564        |                                | 4.0%             | 0.00875           |  |          |  |   |    |   |      |  |  |   |
| Fine Agg (Pit Nar | ne) S                  | ome Pit    | — I      | N              | 169       | 93        | 7057         |                                | 4.0%             | 0.00786           |  |          |  |   |    |   |      |  |  |   |
| Cement/Ty         | pe Hol                 | lcim I-II  |          | Holcim I-I     |           | cim I-II  |              | im I-II                        |                  |                   |  | cim I-II |  | _ | 65 | 8 | 3948 |  |  | _ |
| Fly Ash/Cla       | ss                     |            | 20       |                |           |           |              |                                |                  | Water Added On    |  |          |  |   |    |   |      |  |  |   |
| Silica Fun        | ne Ford                | e 10,000 D | <u>.</u> |                | 53        | 3         | 318          | •                              |                  | Site              |  |          |  |   |    |   |      |  |  |   |
| Wat               | er De                  | eep Well   |          |                |           | —         | 125          |                                |                  | 25                |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        | A          | dmixtur  | es             |           |           |              | ٦ſ                             |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          | Plar           | nt, Load: | On S      | Site, Load:  | 11                             | Water/Cer        | nent Ratio 0.46   |  |          |  |   |    |   |      |  |  |   |
|                   | Product N              |            | Тс       | tal Oz         | Т         | otal Oz   |              | Water/Cer                      |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   | ADVA 14                | 0M         |          |                | 792       |           | 0            | 1 L                            |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   | WRDA (                 |            | 234      |                | 0         |           | CONC         | CRETE PLACED                   |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              | IΓ                             | To La            | styd³             |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              |                                | This Repo        |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                | _         |           |              | Tota                           | al <u>30</u> yd³ |                   |  |          |  |   |    |   |      |  |  |   |
| Ger               | peral Pour L           | ocation IS | tructure | ITW E          | asthoun   | dlane 1   | emn 40-55    | Ca                             | lm Dark Bega     | n pour at Abut 2, |  |          |  |   |    |   |      |  |  |   |
|                   | ion & Weat             |            |          |                |           | a conc, i | cmp 40 00    | ,                              |                  | n pour ur nour 2, |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
| 8                 | Placed                 | Location A | butmer   | nt 2           |           |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           | •.           | ,                              |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        | Remarks    | ontract  | or addec       | 1 too mu  | ich wate  | r on site, w | /c ra                          | atio too high, h | land slapped.     |  |          |  |   |    |   |      |  |  |   |
| Cylinder          | Tir                    | ne         | Slum     |                | Air       | Unit Wt   | Temp         | Requested Testing Acc          |                  |                   |  |          |  |   |    |   |      |  |  |   |
| Number            | Batched                | Placed     | (in)     | · ·            |           | (lbs/yd)  | (F)          | Requested Testing Ag<br>(Days) |                  | Remarks           |  |          |  |   |    |   |      |  |  |   |
| 1                 | 2:00                   | 2:45       | 6.5      |                | .5%       | 138.4     | 65           |                                | 2                | 1                 |  |          |  |   |    |   |      |  |  |   |
| 2                 | 2:00                   | 2:45       | 6.5      |                | .5%       | 138.4     | 65           | <b> </b>                       | 3                |                   |  |          |  |   |    |   |      |  |  |   |
| 3                 | 2:00                   | 2:45       | 6.5      |                | .5%       | 138.4     | 65           |                                | 5                |                   |  |          |  |   |    |   |      |  |  |   |
| 4                 | 2:00                   | 2:45       | 6.5      |                | .5%       | 138.4     | 65           |                                | 7                | 31                |  |          |  |   |    |   |      |  |  |   |
| 5                 | 2:00                   | 2:45       | 6.5      |                | .5%       | 138.4     | 65           |                                | 28               |                   |  |          |  |   |    |   |      |  |  |   |
| 6                 | 2:00                   | 2:45       | 6.5      | 4              | .5%       | 138.4     | 65           |                                | 28               |                   |  |          |  |   |    |   |      |  |  |   |
| 7                 | 2:00                   | 2:45       | 6.5      | 4              | .5%       | 138.4     | 65           |                                | 28               |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                | _         |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |
|                   |                        |            |          |                |           |           |              |                                |                  |                   |  |          |  |   |    |   |      |  |  |   |

### MEASURING LENGTH OF DRILLED CONCRETE CORES

- Scope: This method covers the procedure for determining the length of a core which is drilled from concrete pavement. This procedure is identical to ASTM C174.
- Use: This method is used to determine the length of concrete cores taken at the project site for the purpose of determining specification compliance for concrete thickness including quality acceptance and/or quality control samples when applicable.
- Apparatus: As per ASTM C174.

Reference

Documents:ASTM C174Standard Test Method for Measuring Thickness of<br/>Concrete Elements Using Drilled Concrete CoresWYDOT<br/>WYDOT 800.0Current WYDOT Standard Specifications <br/>Random Number Selections for Density and Gradation<br/>Testing

- ♦ Refer to "For All Concrete Sections" notation in Table of Contents 400 Pavements.
- Sampling: As per ASTM C174.

The WYDOT engineer will randomly select representative locations using a table of random numbers in accordance with WYDOT 800.0.

Do not attempt coring without water. Ensure the coring drill is perpendicular to the surface during and after coring. Take the concrete core samples at least 2 feet away from all joints and edges of pavement to ensure drilling will not damage dowel bars or tie steel.

The contractor or his representative will core in the presence of the WYDOT representative in accordance with *WYDOT Standard* Specifications. The WYDOT representative will measure the concrete core specimens.

Procedure: If the base material is bonded to the bottom surface of the concrete, remove the bonded particles by wedging, by chisel and hammer, or by careful wire brushing. Do not use cores that show abnormal defects or that have been damaged appreciably in the drilling operation.

Measure the core in accordance with ASTM C174.

Sum the individual sublot core values and round the lot mean thickness to the nearest 0.10 inch. Refer to *WYDOT Standard Specifications*.

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### MAKING AND CURING CONCRETE CYLINDERS

- Scope: This method covers procedures for molding and curing concrete cylinders at the project site. This section applies to projects without Quality Control (QC) / Quality Acceptance (QA), for QC / QA projects which include *WYDOT Standard Specifications*. Included are references from ASTM C31.
- Use: This procedure is used for molding and curing concrete cylinders for the purpose of acquiring samples for acceptance testing and for determining form removal time or determining when a structure may be put into service.

Reference

|  | ng and Curing Concrete Test  |
|--|--|
| 1  | nsity (Unit Weight) Vield and  |
| Air Content (Gravimetric) of   |  |
| C172 Standard Practice for Samplin   | ng Freshly Mixed Concrete  |
| Γ Current WYDOT Standard Sp  | pecifications 🛠  |
| Г 477.0 Field Sampling Fresh Concre  | ete  |
| T T-109 Concrete Placing Report  |  |
| T T-128Construction Test Requirement   | nts  |
| Specimens in the FieldC138Standard Test Method for Der<br>Air Content (Gravimetric) of CC172Standard Practice for SamplinC172Standard Practice for SamplinTCurrent WYDOT Standard SpF 477.0Field Sampling Fresh ConcreT T-109Concrete Placing Report | nsity (Unit Weight), Yield,<br>Concrete<br>ing Freshly Mixed Concrete<br>pecifications <b>*</b><br>ete |

- ✤ Refer to "For All Concrete Sections" notation in Table of Contents 400 Pavements.
- Apparatus: As per ASTM C172.
- Sample: Representative composite samples will be as per ASTM C172. Sampling and testing rate requirements will be itemized on the WYDOT Form T-128, *Construction Test Requirements.*

Make at least one set per sublot, a set is defined as three cylinders for 28 day QC / QA and non QC / QA testing. Make a sufficient number of cylinders if early breaks are requested. Follow the procedure for sampling concrete as outlined in WYDOT 477.0.

Obtain the samples for compressive strength for structural concrete as per *WYDOT Standard Specifications*.

Unit weight, slump, air content and temperature will be measured from the same composite sample of concrete when compressive strength test specimens are made.

Sampling and testing information will be reported on WYDOT Form T-109.

WYDOT 485.0 (Rev. 10-18)

Procedure: After sampling the concrete place the cylinder can on a level rigid surface, free from vibration or other disturbance, and as close as possible to the planned place of storage. The appropriate methods of consolidation are as per ASTM C31.

Rodding: As per ASTM C31.

Vibrating: As per ASTM C31.

Finishing: As per ASTM C31.

Curing: Non - QC / QA:

After molding, cylinders shall be immediately stored at the project site in an environment which provides a temperature range of 60 °F to 80 °F and in a moist environment which will prevent any loss of moisture. The 48 hour initial cure limit does not apply for QC /  $QA^1$ . The cylinders shall remain in this environment until transport.

After set WYDOT will transport the quality acceptance (QA) cylinders to the WYDOT Materials Program in Cheyenne for testing or to an alternate location as determined by the WYDOT engineer where the cylinders will be placed in a standard cure environment. The cylinders shall remain in their molds until they are received by the testing laboratory. The 4 hour maximum transportation time limit does not apply.

Cylinders which will be used for determining form removal time or determining when a structure may be put into service will remain in the same environment as the placed concrete until tested.

QC / QA Projects

The contractor will provide a location with the above conditions at the project site for storing the cylinders during initial curing.

<sup>&</sup>lt;sup>1</sup> WYDOT does not require that standard cure facilities be located at project sites. Therefore, it is understood that under some circumstances the contractor may not be capable of placing cylinders in standard cure within 48 hours.

### MAKING AND CURING CONCRETE BEAMS

- Scope: This method covers procedures for molding and curing concrete beams for mix designs and the project site upon request. This section applies to projects with Quality Control (QC) / Quality Acceptance (QA) for Portland Cement Concrete Pavement (PCCP). Included are references from ASTM C31.
- Use: This procedure is used for molding and curing concrete beams for the purpose of acquiring samples for acceptance testing and for determining the 28 day flexural strength of the concrete pavement.

This procedure is typically used for Mix Design only as per *WYDOT Standard Specifications*. If requested and approved by the WYDOT Materials Program to use concrete beams in the field throughout a project, and dependent on the Level of Control of the project, use the procedure approved and specified.

### Reference

| Documents: | ASTM C31    | Standard Practice for Making and Curing Concrete Test<br>Specimens in the Field                     |
|------------|-------------|---|
|            | ASTM C138   | Standard Test Method for Density (Unit Weight), Yield,<br>and Air Content (Gravimetric) of Concrete |
|            | ASTM C172   | Standard Practice for Sampling Freshly Mixed Concrete   |
|            | WYDOT       | Current WYDOT Standard Specifications *   |
|            | WYDOT 471.0 | WYDOT Concrete Mix Design Procedure   |
|            | WYDOT 474.0 | Flexural Strength of Portland Cement Concrete Beams   |
|            | WYDOT 475.0 | Correlation of Compressive Strength to Flexural Strength  |
|            | WYDOT 477.0 | Field Sampling Fresh Concrete   |
|            | WYDOT T-109 | Concrete Placing Report   |
|            | WYDOT T-128 | Construction Test Requirements  |
|            |             | 1   |

✤ Refer to "For All Concrete Sections" notation in Table of Contents – 400 Pavements.

Apparatus: As per ASTM C31.

Sampling: As per ASTM C172.

Follow the Mix Design procedure as outlined in WYDOT 471.0.

Make at least one set per sublot, a set is defined as three beam molds for 28 day QC / QA testing and to make a sufficient number of beams for early breaks. Follow the procedure for sampling concrete as outlined in WYDOT 477.0.

Procedure: Follow procedures in ASTM C138.

Rodding:As per ASTM C31.Vibrating:As per ASTM C31.

Finishing: As per ASTM C31.

Apply curing compound to the exposed surface immediately. If the curing compound is not readily available, protect the exposed surface from evaporation using wet burlap, plastic sheeting or an impervious material until the curing compound is applied.

Curing: After molding, beams will be immediately stored at the project site in an environment which provides a temperature range of 60 °F to 80 °F and in an environment which will prevent any loss of moisture. The 48 hour initial cure limit does not apply<sup>1</sup>.

> The contractor will provide a location with the above conditions at the project site for storing the beams during initial curing.

> Beams will remain in the molds until received by the WYDOT Materials Program.

Commentary: ASTM C31 states that for cylinders and beams which are to be transported after 48 hours, a standard cure environment will be required at the project site in addition to the initial curing environment of 60 °F to 80 °F. A standard cure requires the beams to be removed from the molds and placed in an environment which provides free water on the cylinders at all times at a temperature of 73.4 °F  $\pm$  3 °F. However ASTM C31, allows for the cylinders and beams to remain in the 60 °F to 80 °F environment in the molds until transport, thereby eliminating the requirement for a standard cure facility on the project site.

According to ASTM C31, one possible method for preventing moisture loss from samples during initial curing, is to store the samples in heavyweight closed plastic bags. The 4 hour maximum transportation time limit does not apply.

Report: Sampling and testing information will be reported on Form T-109.

<sup>1</sup> WYDOT does not require that standard cure facilities be located at project sites. Therefore, it is understood that under some circumstances the contractor may not be capable of placing cylinders in standard cure within 48 hours.

### STRUCTURAL CONCRETE / PCCP YIELD PROCEDURE

- Scope: This procedure provides formulas for calculating yield and relative yield of structural concrete and Portland Cement Concrete Pavement (PCCP). Yield is defined in ASTM C138 as the volume of concrete produced from the mixture of known quantities of the component materials.
- Use: This procedure is used for Quality Control (QC) purposes with structural concrete and for informational purposes on Portland Cement Concrete Pavement (PCCP).

This procedure is used in conjunction with WYDOT 479.0 and WYDOT 481.0.

Reference

| ASTM C138   | Standard Test Method for Density (Unit Weight), Yield, and |  |  |  |  |
|-------------|--|--|--|--|--|
|             | Air Content (Gravimetric) of Concrete                      |  |  |  |  |
| WYDOT       | Current WYDOT Standard Specifications �                    |  |  |  |  |
| WYDOT 479.0 | Unit Weight (Density) of Concrete                          |  |  |  |  |
| WYDOT 481.0 | Air Content of Freshly Mixed Concrete                      |  |  |  |  |
| WYDOT 816.0 | Sieve Analysis of Concrete Aggregate                       |  |  |  |  |
| WYDOT T-109 | Concrete Placing Report                                    |  |  |  |  |
|             | WYDOT 479.0<br>WYDOT 481.0<br>WYDOT 816.0                  |  |  |  |  |

- ✤ Refer to "For All Concrete Sections" notation in Table of Contents 400 Pavements.
- Procedure: Yield is the volume of concrete represented by the weight of concrete materials batched:

$$Y_F = \frac{W_T}{U_F}$$

Where:  $Y_F$  = Volume of field yield ft<sup>3</sup>;  $W_T$  = Total weight of constituent materials batched including aggregate, cement, fly ash and water expressed in lb;  $U_F$  = Fresh density (unit weight) of concrete lb/ft<sup>3</sup>.

Relative yield is the ratio of the actual volume of concrete obtained to the volume as designated for the batch; calculated as follows:

$$R_Y = \frac{Y_F}{Y_T}$$

Where:  $R_Y$  = Relative yield;  $Y_T$  = Volume of designated concrete batch.

Method: Yield will be calculated simultaneously with those batches on which routine consistency tests are performed.

Yield will only be determined on batches on which the delivered load is 75% or greater of the rated capacity of the truck mixer or agitator.

Variation will be determined, from theoretical yield to field yield, on a percentage basis as follows:

$$V = \frac{Y_T - Y_F}{Y_T} \ge 100$$

Where: V = Variation (%);  $Y_T = Theoretical yield (the intended amount batched ft<sup>3</sup>$ from batch tickets).

Example:  $7 \text{ yd}^3$  is batched;

| Batch Ticket: | Sand          | = | 8,432.3  | lb                                |
|---------------|---------------|---|----------|-----------------------------------|
|               | Rock          | = | 12,634.1 | lb                                |
|               | Water / Batch | = | 1,714.3  | lb                                |
|               | Water / Site  | = | 75.8     | lb                                |
|               | Cement        | = | 4,166.0  | lb                                |
|               | Total         | = | 27,022.5 | lb (for 7 yd <sup>3</sup> batch); |

Total weight of the batch is 27,022.5 lb The measured density (unit wt.) is 144.5 lb/ft<sup>3</sup>;

Density (unit weight) is reported to the nearest 0.1 lb/ft<sup>3</sup>;

Theoretical yield:  $Y_T = 7 \text{ yd}^3 \text{ x } 27 \text{ ft}^3/\text{yd}^3 = 189.0 \text{ ft}^3$ 

Theoretical yield is calculated from the products mix design specific gravity multiplied by  $62.4 \text{ lb/ft}^3$ ;

Yield:

$$Y_F = \frac{W_T}{U_F} = 187.0 = \frac{27,022.5}{144.5}$$

Yield is reported to the nearest 0.1 ft<sup>3</sup>;

Where:  $Y_{\rm F} = 187.0$  ft<sup>3</sup>  $W_T = 27,022.5$  lb  $U_F = 144.5$  lb/ft<sup>3</sup>

Relative Yield:

$$R_Y = \frac{Y_F}{Y_T} = 0.99 = \frac{187.0}{189.0}$$

Relative yield is reported to the nearest 0.01.

Where:  $R_Y$  = Relative yield;

 $Y_T$  = Volume of designated concrete batch;

Relative yield larger than 1.0 indicates excess of concrete, less than 1.0 indicates the batch is short.

Variation:

$$V = \frac{Y_T - Y_F}{Y_T} \ge 100 = 1.1\% = \frac{189.0 - 187.0}{189.0} \ge 100$$

If variation is within 2.0%, simply record this data on Form T-109, *Concrete Placing Report* in the Remarks section.

If variation is greater than 2.0% or less than -2.0% for two consecutive tests, follow Schedule "A". Small placements may warrant Schedule "A" requirements after one variant yield test. Report in the Remarks section of Form T-109, *Concrete Placing Report*.

If variation continues after Schedule "A" requirements have successfully been completed, follow Schedule "B".

If after Schedule "B" requirements have successfully been completed and yield variation remains, invoke Schedule "C".

Questions: Anything related to the Schedules may be directed to the WYDOT Materials Program.

Schedule "A":

- 1. Contact the WYDOT Materials Program, Concrete Section with information of variations. The Concrete Section will re-check the mix design and notify the engineer of any deviations.
- 2. Check the batch plant. Check and calibrate aggregate and cement scales, water meters and dispensers. Check aggregate stockpile moisture contents and expansion of laboratory mix design to batch sheets.
- 3. Check transport and/or ready-mix trucks to insure compliance with specifications, proper clean-out, and truck water meters.
- 4. Make minor adjustments in air content.
- 5. Compare total net water used per unit volume from Form T-109, *Concrete Placing Report* with lab mix design net water.

Schedule "B":

1. Submit samples of project aggregate, cement, fly ash and admixtures to the WYDOT Materials Program to check specific gravities, absorption and re-run mix design.

Schedule "C":

- 1. Adjust the mix design to reduce yield variation to within the 2% variation limit. This will be done by proportionally adjusting all concrete components fine aggregate, coarse aggregate, cement and fly ash. The adjustment would be of a temporary nature.
- 2. Re-adjustment may be necessary dependent on duration of the placement and variation in the batch plant.

Discussion: It should be noted that the following conditions will affect yield:

- 1. The difference between field air content and lab mix design air content will vary yield in direct proportion to the difference in air content (e.g. lab mix design air content of 5.5% vs. field air content of 4.0% will result in 1.5% variation in yield) as per *WYDOT Standards*.
- 2. A change of 1.0% moisture content of either the sand (FA) or rock (CA) will vary yield by approximately 1.0% if not accounted for (determine % moisture as per WYDOT 816.0).
- 3. Variations in aggregate (i.e. specific gravity, absorption) will result in variation in yield.
- 4. A change in the water/cement ratio of 0.01 will vary yield by approximately 0.5%.
- 5. Form errors or grade miscalculations may result in yield variation from contractor's viewpoint.
- 6. Allowable variations in batch plant scale accuracy will affect yield.

All of these factors may have additive affects on yield and will vary constantly during the project. It is the WYDOT Materials Program intent to minimize yield variations and adjustments necessary to compensate for them. The 2% allowable variation and procedures in Schedule "A" should accomplish this. Performance of Schedule "A" items should not be limited only to periods of yield variation. These items should be performed routinely. The emphasis of this procedure will result in increased attention on the batch plant and more scale maintenance may be required.

### **RANDOM NUMBER SELECTION FOR DENSITY AND GRADATION TESTING**

- Scope: This procedure describes the process for randomly selecting test locations for density tests and the test tonnage for gradation tests.
- Use: Brief narratives and examples of the use of spreadsheet random number functions and of random number tables are included.

### Reference

| Documents: | WYDOT 401.4.7.4  | WYDOT Standard Specifications   |
|------------|------------------|---------------------------------|
|            | WYDOT 401.4.7.5  | WYDOT Standard Specifications   |
|            | WYDOT 401.4.12-1 | WYDOT Standard Specifications   |
|            | WYDOT 401.4.12-2 | WYDOT Standard Specifications   |
|            | WYDOT T-312      | Density Random Number Selection |

### Procedure: Density Tests

- 1. Determine the total production of material for one day. This information can be obtained from the daily weight tickets.
- 2. Determine the total linear distance paved and the total width paved. This information can be obtained from the weight tickets or from the paving inspector.
- 3. Determine the number and size of lots needed for one day's production. Determine the number of sublots per lot. These are determined from *WYDOT Standard Specifications* Section 401.4.7.5, or Table 401.4.12-1, depending on which controls the plant mix production being evaluated.
- 4. Determine the lot size in linear feet and the length of section that is represented by each test.
  - a. Determine the length per lot by dividing the number of linear feet paved by the number of lots represented.
  - b. Determine the length represented by each test by dividing the feet represented per lot by the number of sublots per lot.
  - c. Determine the stations representing each lot and sublot based on the section lengths and the beginning station.
- 5. Perform the following location selection separately for each test, each sublot. An example of this procedure is provided below.
  - a. Select a random number between 0 and 1 as described in the "Density Random Number Selection" of this section.
  - b. Determine a test station. Multiply the random number between 0 and 1 by the length represented per test and add it to the beginning station of the section represented.
  - c. Select another random number between 0 and 1 as described in the "Density Random Number Selection" of this section.

- d. Determine the transverse distance. Subtract 2 feet from the width of the ribbon and then multiply this width by the random number between 0 and 1. Add 1 foot to the result and measure in that distance from the outer edge of the ribbon to determine the test location at the test station selected in "5.b." above.
- Example: This demonstrates one possible spreadsheet layout for calculating the station and distance from the outer edge of the ribbon for density core sampling.

|        |        |             |                | ]         | Longitudinal | Length* |               |
|--------|--------|-------------|----------------|-----------|--------------|---------|---------------|
| Lot    | Sublot | Begin       | End            | Net       | Random       | Random  | Station       |
| Number | Number | Station     | <b>Station</b> | Length    | Number       | Number  | Tested        |
| 1      | 1      | 0+00        | 50 + 00        | 5,000     | 0.870        | 4,348   | 43+48         |
| 1      | 2      | 50 + 00     | 100 + 00       | 5,000     | 0.894        | 4,470   | 94+70         |
| 1      | 3      | 100 + 00    | 150+00         | 5,000     | 0.961        | 4,803   | 148+03        |
| 1      | 4      | 150+00      | 200+00         | 5,000     | 0.545        | 2,723   | 177+23        |
| 1      | 5      | 200+00      | 250+00         | 5,000     | 0.200        | 1,000   | 210+00        |
|        |        |             |                |           |              |         |               |
|        |        |             |                |           | Width        | Dist    | ance          |
|        |        | Ribbon      | Ribbon         | Transvers | e 2 ft       | Fr      | om            |
| Lot    | Sublot | Width       | Width          | Random    | *Random      | ı Rit   | bon           |
| Number | Number | <u>1 ft</u> | <u>2 ft</u>    | Number    | Number       | Edg     | <u>ge, ft</u> |
| 1      | 1      | 12          | 10             | 0.261     | 2.61         | 3.61    |               |
| 1      | 2      | 12          | 10             | 0.064     | 0.64         | 1.64    |               |
| 1      | 3      | 12          | 10             | 0.766     | 7.66         | 8.      | 66            |
| 1      | 4      | 12          | 10             | 0.500     | 5.00         | 6.      | 00            |
| 1      | 5      | 12          | 10             | 0.873     | 8.73         | 9.      | 73            |

The numbers generated above are generated by the formulas below.

| Lot<br><u>Number</u><br>1<br>1<br>1 | Sublot<br><u>Number</u><br>1<br>2<br>3 | Begin<br><u>Station</u><br>0<br>5000<br>10000 | End<br><u>Station</u><br>5000<br>10000<br>15000 | Net<br><u>Length</u><br>=D2-C2<br>=D3-C3<br>=D4-D4         | Congitudinal<br>Random<br><u>Number</u><br>=Rand()<br>=Rand()<br>=Rand() | $\frac{\text{Number}}{=\text{E2*F2}} = \\ = \text{E3*F3} = \\ $ | Station<br><u>Tested</u><br>G2+C2<br>G3+C3<br>G4+C4 |
|-------------------------------------|--|---|---|--|--|---|---|
| Lot<br><u>Number</u><br>1<br>1      | Sublot<br><u>Number</u><br>1<br>2      | Ribbon<br>Width<br><u>1 ft</u><br>12<br>12    | Ribbon<br>Width<br>2  ft<br>=C7-2<br>=C8-2      | Transvers<br>Random<br><u>Number</u><br>=Rand()<br>=Rand() | *Random<br><u>Number</u><br>=D7*E7                                       | Distant<br>From<br>RibboEdge=1+F=1+F                            | n<br>on<br><u>ft</u><br>77                          |
| 1<br>1                              | 2 3                                    | 12  | =C8-2<br>=C9-2                                  | =Rand()<br>=Rand()   |  | =1+F<br>=1+F  |   |

An example worksheet T-312, *Density Random Number Selection Worksheet* is shown at the end of this section.

Gradation Tests

- 1. Determine the number and size of lots and sublots needed. This is determined according to *WYDOT Standard Specifications* Section 401.4.7.4 or Table 401.4.12-2 for Plant Mix Pavements, depending on which one controls the aggregate production being evaluated. The total amount of material used on the project may be taken from the Plans (TEQ) or from revised quantity estimates.
- 2. Determine a random number between 0 and 1 as described in the "Density Random Number Selection" of this section for each sublot.
- 3. Determine the tonnage to sample. Multiply the random number by the tons represented, per sublot, and add to the beginning tonnage for the sublot.

| Lot    | Sublot | Random | Tonnage R | Tonnage |       |         |
|--------|--------|--------|-----------|---------|-------|---------|
| Number | Number | Number | Beginning | Ending  | Net   | Sampled |
| 1      | 1      | 0.265  | 0         | 1,000   | 1,000 | 265     |
| 1      | 2      | 0.941  | 1,000     | 2,000   | 1,000 | 1,941   |
| 1      | 3      | 0.528  | 2,000     | 3,000   | 1,000 | 2,528   |
| 1      | 4      | 0.067  | 3,000     | 4,000   | 1,000 | 3,067   |
| 1      | 5      | 0.884  | 4,000     | 5,000   | 1,000 | 4,884   |
| 4      | 1      | 0.558  | 14,700    | 15,385  | 685   | 15,083  |
| 4      | 2      | 0.138  | 15,385    | 16,070  | 685   | 15,480  |
| 4      | 3      | 0.597  | 16,070    | 16,755  | 685   | 16,479  |
| 4      | 4      | 0.689  | 16,755    | 17,440  | 685   | 17,227  |
| 4      | 5      | 0.092  | 17,440    | 18,125  | 685   | 17,503  |
| 4      | 6      | 0.617  | 18,125    | 18,810  | 685   | 18,548  |
| 4      | 7      | 0.416  | 18,810    | 19,495  | 685   | 19,095  |

This procedure is demonstrated by the following examples:

### Random Number Selection

One may use the random function of a spreadsheet, the random number on a calculator, or random number tables to generate random numbers. Use of a spreadsheet and of random number tables is described here.

Use a random function on a spreadsheet. Most spreadsheets have a random number generator function. A spreadsheet may be set up that generates random numbers and calculates the tonnage to sample. An example of such a spreadsheet, with both numbers and formulas displayed, was used to calculate some of the above tonnages as follows:

| Random        |                  |        |            |                |
|---------------|------------------|--------|------------|----------------|
| <u>Number</u> | <b>Beginning</b> | Ending | <u>Net</u> | Sample Sample  |
| 0.558         | 14,700           | 15,385 | 685        | 15,083         |
| 0.138         | 15,385           | 16,070 | 685        | 15,480         |
| 0.597         | 16,070           | 16,755 | 685        | 16,479         |
|               |                  |        |            |                |
| Random        |                  |        |            |                |
| <u>Number</u> | <b>Beginning</b> | Ending | Net        | <u>Sample</u>  |
| =Rand()       | 14,700           | 15,385 | =C2-B2     | =(C2-B2)*A2+B2 |
| =Rand()       | 15,385           | 16,070 | =C3-B3     | =(C3-B3)*A3+B3 |
| =Rand()       | 16,070           | 16,755 | =C4-B4     | =(C4-B4)*A4+B4 |
|               |                  |        |            |                |

Use a random number table, such as the ones included in this procedure. The tables are set up with the columns and rows assembled in groups of either five or seven, since most lots are comprised of five or seven sublots. Enter the random number table at any point, but do not enter it in the same place twice. Once entering the table, arbitrarily choose random numbers from the table, one random number for each sublot. This may be accomplished by selecting the group of random numbers, either row or column, in which the entry number is included (see the provided example).

Avoid simply entering the table randomly five or seven times to get five or seven numbers.

### Random Numbers

|   | 0.648       | 0.820     | 0.741      | 0.306 | 0.309 | 0.294     | 0.477 | 0.496 | 0.586 | 0.376 |
|---|-------------|-----------|------------|-------|-------|-----------|-------|-------|-------|-------|
|   | 0.574       | 0.754     | 0.245      | 0.930 | 0.194 | 0.258     | 0.913 | 0.308 | 0.554 | 0.915 |
|   | 0.433       | 0.192     | 0.467      | 0.373 | 0.318 | 0.180     | 0.552 | 0.144 | 0.123 | 0.565 |
|   | 0.412       | 0.518     | 0.576      | 0.457 | 0.914 | 0.849     | 0.743 | 0.757 | 0.299 | 0.190 |
|   | 0.845       | 0.557     | 0.540      | 0.776 | 0.075 | 0.106     | 0.781 | 0.083 | 0.346 | 0.309 |
|   |             |           |            |       |       |           |       |       |       |       |
|   | 0.713       | 0.121     | 0.704      | 0.223 | 0.377 | 0.795     | 0.780 | 0.346 | 0.587 | 0.021 |
|   | 0.112       | 0.635     | 0.728      | 0.408 | 0.854 | 0.509     | 0.668 | 0.635 | 0.559 | 0.137 |
|   | 0.107       | 0.170     | 0.026      | 0.240 | 0.034 | 0.951     | 0.305 | 0.808 | 0.501 | 0.739 |
|   | 0.579       | 0.124     | 0.648      | 0.446 | 0.783 | 0.203     | 0.609 | 0.733 | 0.818 | 0.571 |
|   | 0.888       | 0.802     | 0.828      | 0.072 | 0.403 | 0.112     | 0.626 | 0.427 | 0.145 | 0.736 |
|   |             |           |            |       |       |           |       |       |       |       |
|   | 0.260       | 0.320     | 0.952      | 0.342 | 0.922 | 0.636     | 0.956 | 0.228 | 0.965 | 0.094 |
|   | 0.319       | 0.839     | 0.748      | 0.009 | 0.356 | 0.313     | 0.560 | 0.668 | 0.858 | 0.181 |
|   | 0.200       | 0.831     | 0.947      | 0.109 | 0.314 | 0.301     | 0.115 | 0.453 | 0.154 | 0.447 |
|   | 0.517       | 0.632     | 0.400      | 0.004 | 0.637 | 0.295     | 0.459 | 0.614 | 0.194 | 0.212 |
|   | 0.710       | 0.216     | 0.946      | 0.231 | 0.532 | 0.179     | 0.631 | 0.168 | 0.170 | 0.586 |
| Е | nter at 0.3 | 23 and ch | oose eithe |       |       |           |       |       |       |       |
|   | r five num  |           |            |       |       |           |       |       |       |       |
|   | 0.922       | 0.933     | 0.005      | 0.647 | 0.214 | 0.715     | 0.109 | 0.373 | 0.513 | 0.074 |
| Γ | 0.427       | 0.323     | 0.556      | 0.308 | 0.839 | 0.377     | 0.867 | 0.274 | 0.241 | 0.102 |
|   | 0.915       | 0.242     | 0.041      | 0.916 | 0.409 | 0.588     | 0.358 | 0.348 | 0.149 | 0.275 |
|   | 0.027       | 0.208     | 0.765      | 0.926 | 0.059 | 0.893     | 0.893 | 0.160 | 0.650 | 0.572 |
|   | 0.714       | 0.981     | 0.826      | 0.763 | 0.185 | 0.581     | 0.286 | 0.763 | 0.207 | 0.047 |
|   | 0.71        | 0.901     | 0.020      | 0.705 | 0.105 | 0.001     | 0.200 | 0.702 | 0.207 | 0.017 |
|   | 0.565       | 0.109     | 0.896      | 0.829 | 0.783 | 0.573     | 0.041 | 0.298 | 0.149 | 0.861 |
|   | 0.733       | 0.247     | 0.526      | 0.105 | 0.842 | 0.352     | 0.785 | 0.584 | 0.390 | 0.118 |
|   | 0.865       | 0.856     | 0.312      | 0.945 | 0.286 | 0.308     | 0.247 | 0.403 | 0.573 | 0.970 |
|   | 0.593       | 0.699     | 0.699      | 0.009 | 0.633 | 0.830     | 0.792 | 0.802 | 0.339 | 0.488 |
|   | 0.544       | 0.965     | 0.010      | 0.850 | 0.767 | 0.030     | 0.126 | 0.431 | 0.831 | 0.344 |
|   | 0.511       | 0.705     | 0.010      | 0.050 | 0.707 | 0.275     | 0.120 | 0.151 | 0.051 | 0.511 |
|   | 0.348       | 0.400     | 0.155      | 0.220 | 0.944 | 0.309     | 0.783 | 0.526 | 0.262 | 0.488 |
|   | 0.050       | 0.511     | 0.006      | 0.649 | 0.787 | 0.009     | 0.707 | 0.445 | 0.311 | 0.857 |
|   | 0.616       | 0.480     | 0.038      | 0.997 | 0.534 | 0.240     | 0.665 | 0.294 | 0.519 | 0.317 |
|   | 0.994       | 0.921     | 0.427      | 0.476 | 0.452 | 0.195     | 0.358 | 0.237 | 0.440 | 0.511 |
|   | 0.768       | 0.932     | 0.561      | 0.194 | 0.452 | 0.734     | 0.628 | 0.959 | 0.754 | 0.467 |
|   | 0.700       | 0.752     | 0.501      | 0.174 | 0.451 | 0.754     | 0.020 | 0.757 | 0.754 | 0.407 |
|   | 0.962       | 0.510     | 0.680      | 0.826 | 0.460 | 0.759     | 0.514 | 0.151 | 0.151 | 0.626 |
|   | 0.370       | 0.247     | 0.168      | 0.820 | 0.458 | 0.759     | 0.983 | 0.328 | 0.657 | 0.020 |
|   | 0.376       | 0.665     | 0.635      | 0.155 | 0.458 | 0.882     | 0.983 | 0.095 | 0.378 | 0.311 |
|   | 0.330       | 0.605     | 0.033      | 0.135 | 0.954 | 0.013     | 0.198 | 0.093 |       |       |
|   |             |           |            |       |       |           |       |       | 0.751 | 0.724 |
|   | 0.617       | 0.017     | 0.624      | 0.547 | 0.749 | <br>0.603 | 0.722 | 0.827 | 0.696 | 0.783 |
|   |             |           |            |       |       |           |       |       |       |       |

Enter at 0.912 and use five number row for the

longitudinal density locations and use adjacent row for

the five transverse values.

# Random Numbers

| 0.978 | 0.919 | 0.371 | 0.886 | 0.843 | 0.999   | 0.756 | 0.957  | 0.181 | 0.179 |
|-------|-------|-------|-------|-------|---------|-------|--------|-------|-------|
| 0.528 | 0.844 | 0.550 | 0.693 | 0.350 | 0.939   | 0.946 | 0.297  | 0.160 | 0.335 |
| 0.734 | 0.817 | 0.067 | 0.626 | 0.873 | 0.175   | 0.819 | 0.190  | 0.837 | 0.172 |
| 0.896 | 0.443 | 0.190 | 0.172 | 0.427 | 0.170   | 0.394 | 0.915  | 0.164 | 0.986 |
| 0.591 | 0.585 | 0.650 | 0.564 | 0.242 | 0.054   | 0.834 | 0.799  | 0.014 | 0.489 |
| 0.071 | 0.000 | 0.000 | 01001 | 01212 | 01001   | 0.000 | 0.777  | 01011 | 01102 |
| 0.923 | 0.963 | 0.389 | 0.085 | 0.484 | 0.676   | 0.496 | 0.542  | 0.314 | 0.315 |
| 0.800 | 0.997 | 0.219 | 0.032 | 0.171 | 0.987   | 0.839 | 0.708  | 0.403 | 0.186 |
| 0.321 | 0.983 | 0.375 | 0.279 | 0.813 | 0.759   | 0.677 | 0.862  | 0.696 | 0.638 |
| 0.391 | 0.481 | 0.035 | 0.881 | 0.004 | 0.663   | 0.779 | 0.993  | 0.866 | 0.158 |
| 0.454 | 0.783 | 0.690 | 0.934 | 0.850 | 0.688   | 0.237 | 0.734  | 0.112 | 0.249 |
|       |       |       |       |       |         |       |        |       |       |
| 0.299 | 0.679 | 0.590 | 0.185 | 0.537 | 0.893   | 0.787 | 0.787  | 0.971 | 0.005 |
| 0.897 | 0.306 | 0.928 | 0.133 | 0.399 | 0.253   | 0.695 | 0.988  | 0.421 | 0.445 |
| 0.052 | 0.313 | 0.298 | 0.479 | 0.989 | 0.562   | 0.509 | 0.006  | 0.877 | 0.249 |
| 0.655 | 0.778 | 0.033 | 0.236 | 0.036 | 0.411   | 0.637 | 0.131  | 0.392 | 0.265 |
| 0.648 | 0.324 | 0.044 | 0.642 | 0.828 | 0.164   | 0.692 | 0.922  | 0.532 | 0.753 |
|       |       |       |       |       |         |       |        |       |       |
| 0.915 | 0.042 | 0.080 | 0.802 | 0.106 | 0.798   | 0.632 | 0.784  | 0.774 | 0.875 |
| 0.912 | 0.665 | 0.532 | 0.413 | 0.984 | 0.996   | 0.175 | 0.452  | 0.363 | 0.532 |
| 0.520 | 0.459 | 0.476 | 0.396 | 0.356 | 0.510   | 0.056 | 0.612  | 0.913 | 0.153 |
| 0.227 | 0.363 | 0.035 | 0.648 | 0.959 | 0.486   | 0.603 | 0.739  | 0.642 | 0.950 |
| 0.969 | 0.804 | 0.009 | 0.197 | 0.209 | 0.113   | 0.390 | 0.409  | 0.372 | 0.264 |
|       |       |       |       |       |         |       |        |       |       |
| 0.015 | 0.346 | 0.741 | 0.415 | 0.986 | 0.386   | 0.316 | 0.957  | 0.336 | 0.789 |
| 0.676 | 0.996 | 0.858 | 0.911 | 0.374 | 0.977   | 0.828 | 0.733  | 0.140 | 0.742 |
| 0.276 | 0.592 | 0.107 | 0.703 | 0.361 | 0.572   | 0.527 | 0.683  | 0.959 | 0.310 |
| 0.527 | 0.058 | 0.181 | 0.932 | 0.852 | 0.337   | 0.556 | 0.992  | 0.281 | 0.252 |
| 0.180 | 0.326 | 0.350 | 0.176 | 0.709 | 0.534   | 0.880 | 0.949  | 0.295 | 0.709 |
|       |       |       |       |       |         |       |        |       |       |
| 0.208 | 0.484 | 0.516 | 0.498 | 0.387 | 0.737   | 0.005 | 0.605  | 0.059 | 0.835 |
| 0.262 | 0.237 | 0.896 | 0.640 | 0.266 | 0.523   | 0.378 | 0.804  | 0.697 | 0.690 |
| 0.537 | 0.482 | 0.546 | 0.663 | 0.956 | 0.288   | 0.458 | 0.712  | 0.769 | 0.308 |
| 0.445 | 0.865 | 0.196 | 0.970 | 0.624 | 0.496   | 0.285 | 0.145  | 0.488 | 0.683 |
| 0.766 | 0.447 | 0.039 | 0.672 | 0.919 | 0.303   | 0.742 | 0.389  | 0.474 | 0.746 |
| 0.017 | 0.501 | 0.010 | 0.7.0 | 0.000 | 0 5 4 1 | 0.420 | 0.0.00 | 0.602 | 0.000 |
| 0.017 | 0.531 | 0.213 | 0.768 | 0.826 | 0.541   | 0.430 | 0.360  | 0.693 | 0.998 |
| 0.723 | 0.786 | 0.653 | 0.771 | 0.929 | 0.860   | 0.117 | 0.259  | 0.726 | 0.807 |
| 0.115 | 0.124 | 0.132 | 0.279 | 0.547 | 0.182   | 0.385 | 0.156  | 0.378 | 0.304 |
| 0.476 | 0.978 | 0.994 | 0.989 | 0.507 | 0.601   | 0.010 | 0.374  | 0.848 | 0.293 |
| 0.261 | 0.943 | 0.683 | 0.657 | 0.399 | 0.929   | 0.499 | 0.536  | 0.201 | 0.738 |

## Random Numbers

| 0.435 | 0.654 | 0.436 | 0.766 | 0.995 | 0.111 | 0.452 | 0.760 | 0.852 | 0.534 | 0.224 | 0.427 | 0.781 | 0.729 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.576 | 0.863 | 0.370 | 0.449 | 0.722 | 0.710 | 0.411 | 0.005 | 0.319 | 0.463 | 0.960 | 0.010 | 0.385 | 0.045 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.303 | 0.634 | 0.002 | 0.221 | 0.111 | 0.875 | 0.045 | 0.935 | 0.868 | 0.669 | 0.288 | 0.909 | 0.794 | 0.648 |
| 0.722 | 0.503 | 0.455 | 0.761 | 0.379 | 0.558 | 0.396 | 0.027 | 0.589 | 0.918 | 0.256 | 0.860 | 0.702 | 0.927 |
| 0.296 | 0.140 | 0.230 | 0.735 | 0.056 | 0.755 | 0.705 | 0.498 | 0.184 | 0.338 | 0.416 | 0.772 | 0.465 | 0.705 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.369 | 0.653 | 0.422 | 0.919 | 0.466 | 0.686 | 0.078 | 0.292 | 0.808 |       | 0.405 | 0.725 | 0.041 | 0.678 |
| 0.864 | 0.636 | 0.676 | 0.453 | 0.092 | 0.161 | 0.687 | 0.451 | 0.654 | 0.554 | 0.638 | 0.920 | 0.770 | 0.989 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.046 | 0 (17 | 0.000 | 0 474 | 0.202 | 0 105 | 0.004 | 0765  | 0.202 | 0.024 | 0 ((1 | 0.422 | 0 452 | 0.050 |
| 0.246 | 0.617 | 0.960 | 0.474 | 0.382 |       | 0.994 | 0.765 | 0.393 | 0.234 | 0.661 | 0.432 |       | 0.950 |
| 0.429 | 0.990 | 0.903 | 0.576 | 0.596 | 0.235 | 0.354 | 0.366 | 0.935 | 0.301 | 0.070 | 0.816 | 0.981 | 0.951 |
| 0.915 | 0.480 | 0.632 | 0.680 | 0.252 | 0.248 | 0.575 | 0.187 | 0.090 | 0.913 | 0.616 | 0.171 | 0.590 | 0.199 |
|       | 0.333 | 0.324 | 0.267 |       | 0.114 |       |       | 0.398 |       |       | 0.040 | 0.977 | 0.592 |
| 0.708 |       |       |       | 0.046 |       | 0.155 |       |       | 0.804 | 0.417 |       |       |       |
| 0.793 | 0.970 | 0.850 | 0.511 | 0.673 | 0.462 | 0.472 | 0.131 | 0.163 | 0.835 | 0.410 | 0.428 | 0.599 | 0.872 |
| 0.985 | 0.617 | 0.799 | 0.778 | 0.364 | 0.049 | 0.553 | 0.711 | 0.322 | 0.512 | 0.837 | 0.657 | 0.578 | 0.759 |
| 0.615 | 0.808 | 0.482 |       | 0.065 | 0.205 | 0.481 | 0.149 | 0.331 | 0.553 | 0.294 | 0.761 | 0.255 | 0.384 |
| 0.015 | 0.808 | 0.462 | 0.454 | 0.005 | 0.205 | 0.401 | 0.149 | 0.551 | 0.555 | 0.294 | 0.701 | 0.255 | 0.364 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.659 | 0.818 | 0.270 | 0.126 | 0.329 | 0.257 | 0.846 | 0.590 | 0.565 | 0.435 | 0.465 | 0.291 | 0.084 | 0.809 |
| 0.435 | 0.622 | 0.043 | 0.392 | 0.252 | 0.329 | 0.267 | 0.530 | 0.892 | 0.769 | 0.752 | 0.315 | 0.613 | 0.306 |
|       |       |       | 0.748 |       |       |       |       |       | 0.072 |       |       |       |       |
| 0.819 | 0.609 | 0.278 |       | 0.506 | 0.158 | 0.828 | 0.169 | 0.152 |       | 0.059 | 0.302 | 0.391 | 0.710 |
| 0.136 | 0.343 | 0.893 | 0.060 | 0.332 | 0.553 | 0.784 | 0.781 | 0.331 | 0.543 | 0.584 | 0.072 | 0.064 | 0.956 |
| 0.027 | 0.456 | 0.306 | 0.350 | 0.019 | 0.696 | 0.386 | 0.139 | 0.922 | 0.908 | 0.635 | 0.504 | 0.529 | 0.837 |
| 0.692 | 0.631 |       | 0.514 | 0.315 | 0.133 | 0.504 | 0.061 | 0.336 | 0.266 | 0.877 | 0.777 | 0.140 | 0.199 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.287 | 0.159 | 0.688 | 0.007 | 0.499 | 0.406 | 0.164 | 0.122 | 0.813 | 0.667 | 0.856 | 0.469 | 0.536 | 0.842 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.230 | 0.594 | 0.960 | 0.886 | 0.142 | 0.393 | 0.099 | 0.708 | 0.945 | 0.200 | 0.244 | 0.140 | 0.835 | 0.247 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.415 | 0.813 | 0.271 | 0.072 | 0.929 | 0.531 | 0.856 |       | 0.768 |       | 0.261 | 0.296 | 0.687 | 0.627 |
| 0.914 | 0.694 | 0.928 | 0.224 | 0.891 | 0.329 | 0.906 | 0.535 | 0.227 | 0.317 | 0.405 | 0.035 | 0.991 | 0.721 |
| 0.405 | 0.031 | 0.116 | 0.175 | 0.093 | 0.100 | 0.010 | 0.054 | 0.584 | 0.530 | 0.874 | 0.802 | 0.766 | 0.351 |
| 0.314 | 0.037 | 0.803 | 0.267 | 0.021 | 0.194 | 0.845 | 0.306 | 0.306 | 0.760 | 0.251 | 0.259 | 0.157 | 0.020 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.680 | 0.869 |       | 0.829 | 0.140 | 0.253 | 0.768 | 0.706 | 0.331 |       | 0.862 | 0.856 | 0.734 | 0.346 |
| 0.183 | 0.035 | 0.345 | 0.067 | 0.145 | 0.698 | 0.457 | 0.460 | 0.088 | 0.569 | 0.351 | 0.162 | 0.674 | 0.180 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.164 | 0.791 | 0.861 | 0.728 | 0.949 | 0.834 | 0.800 | 0.194 | 0.399 | 0.706 | 0.478 | 0.139 | 0.896 | 0.937 |
| 0.164 |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.173 | 0.708 | 0.000 | 0.679 | 0.984 | 0.845 | 0.286 | 0.232 | 0.312 | 0.163 | 0.215 | 0.743 | 0.625 | 0.413 |
| 0.441 | 0.302 | 0.697 | 0.261 | 0.909 | 0.903 | 0.434 | 0.631 | 0.260 | 0.176 | 0.328 | 0.639 | 0.875 | 0.740 |
| 0.197 | 0.675 | 0.720 | 0.655 | 0.558 | 0.100 | 0.332 | 0.875 | 0.661 | 0.223 | 0.134 | 0.553 | 0.016 | 0.599 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.060 | 0.427 | 0.454 | 0.355 | 0.126 | 0.324 | 0.748 | 0.755 | 0.179 |       | 0.639 | 0.736 | 0.302 | 0.582 |
| 0.365 | 0.975 | 0.196 | 0.066 | 0.939 | 0.932 | 0.775 | 0.705 | 0.509 | 0.460 | 0.589 | 0.463 | 0.733 | 0.081 |
| 0.299 | 0.020 | 0.703 | 0.650 | 0.071 | 0.549 | 0.489 | 0.259 | 0.141 | 0.686 | 0.101 | 0.560 | 0.461 | 1.000 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.041 | 0.070 | 0.00  | 0.056 | 0.526 | 0.256 | 0.022 | 0 ((1 | 0.500 | 0 705 | 0.000 | 1 000 | 0.042 | 0.017 |
| 0.241 | 0.270 | 0.662 | 0.956 | 0.536 | 0.356 | 0.933 | 0.661 | 0.568 |       | 0.232 | 1.000 | 0.043 | 0.017 |
| 0.628 | 0.201 | 0.546 | 0.759 | 0.141 | 0.226 | 0.813 | 0.231 | 0.323 | 0.206 | 0.322 | 0.680 | 0.872 | 0.444 |
| 0.271 | 0.417 | 0 381 | 0 788 | 0.418 | 0.043 | 0.651 | 0.365 | 0.623 | 0 330 | 0.207 | 0.018 | 0.646 | 0.676 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|       | 0.463 |       |       |       |       |       |       |       |       |       | 0.958 |       |       |
| 0.135 | 0.961 | 0.336 | 0.262 | 0.570 | 0.009 | 0.020 | 0.992 | 0.082 | 0.649 | 0.961 | 0.379 | 0.563 | 0.115 |
| 0.870 | 0.391 | 0.570 | 0.870 | 0.045 | 0.492 | 0.716 | 0.671 | 0.249 | 0.243 | 0.591 | 0.389 | 0.155 | 0.346 |
| 0.341 |       | 0.954 |       |       | 0.667 | 0.870 |       | 0.230 |       |       |       | 0.781 | 0.945 |
| 0.541 | 0.050 | 0.754 | 0.570 | 0.050 | 0.007 | 0.070 | 0.770 | 0.250 | 0.200 | 0.025 | 0.705 | 0.701 | 0.745 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.695 | 0.923 | 0.256 | 0.405 | 0.935 | 0.037 | 0.383 | 0.261 | 0.866 | 0.096 | 0.887 | 0.648 | 0.712 | 0.503 |
| 0.550 | 0.307 | 0.483 | 0.374 | 0.513 | 0.131 | 0.852 | 0.733 | 0.582 | 0.151 | 0.376 | 0.142 | 0.259 | 0.893 |
| 0.754 |       | 0.589 |       | 0.405 | 0.164 | 0.193 | 0.191 | 0.928 | 0.404 |       | 0.646 |       | 0.488 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|       |       | 0.976 |       |       | 0.598 | 0.199 |       | 0.417 |       |       | 0.381 | 0.082 | 0.144 |
| 0.372 | 0.746 | 0.640 | 0.619 | 0.839 | 0.413 | 0.927 | 0.778 | 0.098 | 0.867 | 0.483 | 0.716 | 0.651 | 0.626 |
| 0.661 |       | 0.544 |       |       | 0.532 | 0.977 |       | 0.346 |       |       | 0.811 |       | 0.593 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 0.728 | 0.1// | 0.993 | 0.304 | 0.715 | 0.305 | 0.500 | 0.975 | 0.393 | 0.055 | 0.303 | 0.113 | 0.324 | 0.035 |
|       |       |       |       |       |       |       |       |       |       |       |       |       |       |

WYDOT 800.0 (Rev. 09-16)



## Wyoming Department of Transportation Materials Testing Laboratory Density Random Number Selection Worksheet

**T-312** (Rev. 09-16)

Project: ERP Project Number

Date: M/D/YR

Town: Engineers town

Tested By : Tester name

| (A)  | (B)                            | (C)                            | (D)                             | · · · · · · · · · · · · · · · · · · ·     | (E)                       |
|--|--------------------------------|--------------------------------|---------------------------------|---|---------------------------|
| Total production<br>to be tested                   | Beginning<br>Station           | Ending<br>Station              | Total Feet Payed<br>(C - B = D) | Width<br>Paved<br>(Feet)                  | Width Paved<br>- 2 (Feet) |
| 1500   | 120+00                         | 132+00                         | 1200                            | 12  | 10                        |
| (F)<br>Number of Lots<br>Represented<br>(A / 1500) | (G)<br>Tons per Lot<br>(A / F) | (H)<br>Feet per Lot<br>(D / F) | Feet Rej                        | (I)<br>Feet Represented per test<br>(H/7) |                           |
| 1  | 1500                           | 1200                           |                                 | 171                                       |                           |

| Sample<br>Number | (J)              |                          | Section Rep           | Section Represented |                                  | (M)<br>Random<br>Number | Dist. From<br>Edge<br>Horizontal<br>Distance<br>(Feet)<br>(EXM)+1.0 | Lane<br>1. Right<br>2. Center<br>3. Left | Lift |
|------------------|------------------|--------------------------|-----------------------|---------------------|----------------------------------|-------------------------|---|--|------|
|                  | Random<br>Number | Beginning Station<br>(K) | Ending Station<br>(L) | Test Station        | 1. Upper<br>2. Lower<br>3. Total |                         |   |  |      |
| 1                | 0.106            | 120+00                   | 121+71                | 121+53              | 0.615                            | 7.1                     |   | · · · · · ·                              |      |
| 2                | 0.754            | 121+71                   | 123+43                | 122+14              | 0.675                            | 7.7                     |   | 1  |      |
| 3                | 0.953            | 123+43                   | 125+14                | 123+51              | 0.455                            | 5.5                     |   | 1  |      |
| 4                | 0.621            | 125+14                   | 126+86                | 125+79              | 0.850                            | 9.5                     | S   | 1  |      |
| 5                | 0.369            | 126+86                   | 128+57                | 127+94              | 0.664                            | 7.6                     | · · · · · · · · · · · · · · · · · · ·                               | 1  |      |
| 6                | 0.487            | 128+57                   | 130+29                | 129+45              | 0.758                            | 8.6                     | -   | 1  |      |
| 7                | 0.059            | 130+29                   | 132+00                | 131+90              | 0.630                            | 7.3                     |   | 1  |      |
|                  |                  |                          |                       |                     |                                  |                         |   |  |      |
|                  |                  |                          |                       |                     |                                  | 2                       |   |  |      |
|                  |                  |                          |                       |                     |                                  |                         |   |  |      |

Comments

## VERIFICATION OF ACCURACY OF ELECTRONIC GENERAL PURPOSE BALANCE

- Scope: This method describes the verification procedure for balances used for WYDOT projects. Perform this procedure in accordance with the quality plans at a minimum of once each month, each time the scale is moved inside the lab or the lab trailer is moved in accordance with ASTM E617.
- Apparatus: A balance that has the capacity and readability for the test being performed per WYDOT 814.0 *Sieve Analysis of Combined Aggregate*.

Class 4 (AASHTO M231-95) or (ASTM E 617) weights

#### Reference

| Documents: | AASHTO M231-95 | Standard Specification for Weighing Devices Used in the |  |  |  |  |  |
|------------|----------------|---|--|--|--|--|--|
|            |                | Testing of Materials                                    |  |  |  |  |  |
|            | ASTM E617      | Standard Specification for Laboratory Weights and       |  |  |  |  |  |
| Precision  |                | Mass Standards  |  |  |  |  |  |
|            | WYDOT 814.0    | Sieve Analysis of Combined Aggregate                    |  |  |  |  |  |
|            | WYDOT T-313    | Balance Verification Worksheet                          |  |  |  |  |  |

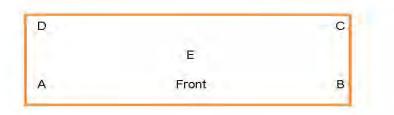
# Procedure: 1. Setup the balance in a location away from drafts or excessive air that might affect the read-out.

- 2. Level the balance and if weighing in water, observe that the suspension apparatus is free of any obstructions that might affect its movement.
- 3. For balances with anticipated usage up to and including 10,000 grams, the verification weights will be 100 grams, 1,000 grams, 5,000 grams, and 10,000 grams.
- 4. Balances with anticipated usage over 10,000 grams, the verification weights will be 5,000 grams, 10,000, and 15,000 grams.
- 5. If one balance is to be used for both of the listed ranges, verify using all weights.
- 6. Place the weight per verification in five locations of the balance (the center and four corners) using the full range and record the actual weight obtained.
- 7. The allowable tolerance per verification is  $\pm 0.1\%$  of the weight used.

- 8. If any recorded weight exceeds the allowable range, discontinue use of the balance until the balance is calibrated or repaired and a complete new verification is performed.
- 9. Copies of all worksheets will be signed by the individual performing the verification and will be kept with the balance.

## WYOMING DEPARTMENT OF TRANSPORTATION T-313 BALANCE VERIFICATION WORKSHEET (Rev. 09-16)

| Project No.(s): ERP Project     | Date: MM/DD /YR  |
|---------------------------------|------------------|
| Sumbitted By: Resident Engineer | At: Town         |
| Manufacturer: Name              | At: Town         |
| Model: Name/Number              | Serial #: Number |
|                                 |                  |



| Verification<br>Weight (grams) | 100          | 1,000           | 5,000             | 10,000             | 15,000              |
|--------------------------------|--------------|-----------------|-------------------|--------------------|---------------------|
| Tolerance<br>(grams)           | 0.1          | 1.0             | 5.0               | 10.0               | 15.0                |
| Allowable<br>Range (grams)     | 99.9 - 100.1 | 999.0 - 1,001.0 | 4,995.0 - 5,005.0 | 9,990.0 - 10,010.0 | 14,985.0 - 15.015.0 |
| Reading A                      | 100.1        | 1,000.2         | 5,000.6           | 10,000.8           | 15,006.1            |
| Reading B                      | 100.0        | 1,000.8         | 5,000.9           | 10,000.4           | 15,007.0            |
| Reading C                      | 100.1        | 1,000.7         | 5,001.0           | 10,001.8           | 15,007.9            |
| Reading D                      | 100.0        | 1,000.2         | 5,001.6           | 10,003.0           | 15,008.4            |
| Reading E                      | 99.9         | 999.2           | 4,998.2           | 9,996.4            | 14,992.2            |

Meets allowable range requirements for all Verification Weights:

**C**NO

Signature: Name

C YES

Certification # Number

WYDOT 801.0 (Rev. 09-16)

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## PREPARATION OF SAMPLES FOR PHYSICAL TESTS

| Scope:     | includ   | nethod describes the preparation of samples for physical tests which usually<br>le liquid limit (WYDOT 812.0) and plastic limit (WYDOT 813.0) tests.<br>procedure is technically equivalent, but not identical, to AASHTO T 87. |  |  |  |  |  |
|------------|--|---|--|--|--|--|--|
| Apparatus: | 1.<br>2.<br>3.<br>4.<br>5.<br>6.   | Mortar and per<br>Sample splitte<br>Drying stove  |  |  |  |  |  |
| Reference  |  |   |  |  |  |  |  |
| Documents: | AASHTO R 58  |   | Standard Method of Test for Dry Preparation of Disturbed<br>Soil and Soil-Aggregate Samples for Test   |  |  |  |  |
|            | WYD  | OT 812.0  | Liquid Limit Test  |  |  |  |  |
|            | WYD  | OT 813.0  | Plastic Limit Test & Plasticity Index  |  |  |  |  |
| Procedure: | 1.   | an oven or ot<br>are considere  | ample thoroughly. Samples dried to a workable condition in ther drying apparatus at a temperature not exceeding $140^{\circ}$ F d to be air dried. This can be accomplished by using a low instant stirring with the trowel.     |  |  |  |  |
|            |  | Note:   | For soils, the sample needs to be workable; not dried to a constant mass.  |  |  |  |  |
|            | <ol> <li>Reduce the sample to a convenient size by use of the sample splitte</li> <li>0.5 lb is sufficient.</li> </ol> |   |  |  |  |  |  |
|            | 3.   | on the No. 10<br>particles are 1  | soil and rock on the No. 10 sieve. Grind material remaining<br>) sieve in a mortar with a rubber covered pestle until the soil<br>proken into separate grains. Discard the fraction retained on<br>eve after the second sieving. |  |  |  |  |
|            | 4.   |   | g portion passing the No. 10 sieve will be separated into two<br>ns of the No. 40 sieve grinding lightly break up between  |  |  |  |  |

4. The remaining portion passing the No. 10 sieve will be separated into two parts by means of the No. 40 sieve, grinding lightly, break up between each of the screenings with the rubber covered pestle. Care must be taken not to pulverize aggregate, only a rubbing action is needed to free clay particles from the coarser aggregate. Discard the material remaining on the No. 40 sieve when repeated grinding produces only small quantities passing the No. 40 sieve.

- 5. Thoroughly mix the remaining material that passes the No. 40 sieve and set aside for testing.
- 6. Remove the sample for testing with a scoop or spoon. Do not pour as pouring will cause segregation.

## AGGREGATE SAMPLING AND QUANTITY

- Scope: This procedure is used when samples of aggregate are taken either for mix design or for maximum density/optimum moisture as used in density testing.
- Apparatus: 1. Shovel
  - 2. Canvas sample sacks
  - 3. Sample splitter

#### Reference

| nerenee    |  |  |  |  |  |  |
|------------|--|--|--|--|--|--|
| Documents: | AASHTO T 180   | Standard Method of Test for Moisture-Density Relations of<br>Soils Using a 4.54-kg (10-lb) Rammer and a 457-mm (18-<br>in.) Drop |  |  |  |  |
|            | WYDOT 414.0  | Marshall and Superpave Mix Design and Mix Volumetric<br>Verification Procedure   |  |  |  |  |
|            | WYDOT 804.0  | Aggregate Sampling   |  |  |  |  |
|            | WYDOT T-120  | Sample Transmittal   |  |  |  |  |
|            | WYDOT T-166  | Aggregate Analysis   |  |  |  |  |
| Sampling:  | See Aggregate Sampling procedures in WYDOT 804.0.<br>A completed Form T-120, <i>Sample Transmittal</i> , Complete and submit Form T-166, <i>Aggregate Analysis</i> . |  |  |  |  |  |
|            | Note: The WYDOT Materials Program will furnish optimum moisture and maximum dry density when requested.  |  |  |  |  |  |

Use sample sacks made of canvas. The sample weight per canvas sack will be 30 lb to 50 lb. Do not exceed 50 lb per sample.

Procedure: Examples of Form T-166 describing the information needed by the WYDOT Materials Program to complete mix design or maximum density follow.

Provide, at a minimum, the quantity of material according to the following:

| Subbase or Blended Subbase                     | 150 lb each stockpile  |  |  |  |
|--|--|--|--|--|
| Crushed Base<br>Blended Crushed Base           | 150 lb (AASHTO T 180)<br>each stockpile                                    |  |  |  |
| Hot Plant Mix Aggregate                        | 100 lb each stockpile – Non-Superpave<br>150 lb each stockpile – Superpave |  |  |  |
| Reclaimed Asphalt Pavement (RAP)               | 120 lb each stockpile*   |  |  |  |
| * refer to WYDOT 414.0 for sampling guidelines |  |  |  |  |

|              | Microsurfacing                             | 100 lb each stockpile   |
|--------------|--|---|
|              | Plant Mix Wearing Course                   | 100 lb when one stockpile is used<br>70 lb each additional stockpile  |
|              | Maintenance Stockpiles                     | 180 lb each stockpile   |
| Concrete Mix | Design                                     |   |
|              | - Silica Fume                              | <ul> <li>100 lb cement</li> <li>300 lb fines</li> <li>400 lb coarse</li> <li>25 lb silica fume</li> <li>1 lb fiber</li> <li>1 quart each admixture</li> </ul> |
|              | - Structural Concrete<br>(A / B / S Class) | 50 lb fly ash<br>140 lb cement<br>400 lb fines<br>600 lb coarse<br>1 quart each admixture   |
|              | - PCCP                                     | 50 lb fly ash<br>140 lb cement<br>600 lb fines<br>775 lb coarse<br>1 quart each admixture   |

## AGGREGATE SAMPLING

- Scope: This procedure covers the methods of obtaining representative aggregate samples of a finished gradation product taken at the end of the production line. Care must be taken to get samples that will provide test data that is truly representative of either the preliminary crushed or final accepted aggregate product. This procedure is similar but not technically equivalent to AASHTO T 2:
  - 1. AASHTO T 2 requires a minimum three belt samples be collected and combined to obtain a representative sample. This procedure requires only one sample be collected at approximately the middle one-third of the conveyor belt.
  - 2. AASHTO T 2 requires the minimum weight of sample be determined based on the nominal maximum size. This procedure requires a minimum 30 lb in every case.
  - 3. AASHTO T 2 does not include a procedure on how to sample from a windrow.

#### Apparatus: 1. Flat square-nose shovel

- 2. Flat square-nose scoop or dust pan and brush
- 3. Conveyor belt template (furnished by the contractor to fit the shape of the conveyor belt)
- 4. Canvas sample sack or container able to hold 30 lb to 50 lb of aggregate at one time
  - Note: Samples submitted to WYDOT must be in a canvas sample sack. If sample is furnished in other type of container, it must be transferred to a canvas sample sack prior to submittal to WYDOT. Care must be taken not to segregate or lose any of the sample during the transfer.

| Reference  |               |  |
|------------|---------------|--|
| Documents: | AASHTO T 2    | Standard Method of Test for Sampling of Aggregates |
|            | WYDOT 800.2   | WYDOT Standard Specifications                      |
|            | WYDOT 804.0   | Correlation of Aggregate Gradation Test Results    |
|            | WYDOT T-165AG | Correlation of Aggregate Gradations                |

## Procedure:

## **Conveyor Belt**

- 1. Obtain conveyor belt samples of the finished product before the addition of any additives (cement, fly-ash, lime, asphalt, and etc.).
- 2. Stop the conveyor belt while sampling. To prevent accidental startups, the conveyor belt will be equipped with a keylock on/off switch or a switch in a lockout box which can either be key-locked or padlocked in the "off" position. The person doing the sampling will keep the key with them and return it after the conveyor belt is clear of any sampling equipment and/or personnel.
- 3. Scaffolding will be attached to the conveyor belt framework having a nonslip walking surface, toe plate and safety hand rail.
- 4. Sample the conveyor belt approximately in the middle one-third. Take the sample when the belt is filled to approximately 80 percent or more of the normal production capacity. Sampling will not be taken over the rollers of the conveyor belt to avoid segregation.

Note: In the presence of WYDOT personnel sampling of the conveyor belt should be performed by the contractor's representative.

- 5. Using the template furnished by the contractor, saw back and forth until the template is all the way through the aggregate stream and onto the conveyor belt. The material between the template will yield a minimum of 30 lb and be placed into a container which is of sufficient capacity that none of the material is lost during sampling or hauling. Any fines left on the belt must be cleaned off with a brush and flat square nose scoop or dust pan and added to the sample.
  - Note: The template shape conforms to the shape of the conveyor belt in the aggregate stream on the conveyor belt.
- 6. When more than one sample is being taken, another cut into the stream of aggregate should be taken as close as possible to the first cut making sure that the stream was not disturbed by the first cut. This procedure may be repeated as many times as needed to obtain the necessary number of samples.

## Windrow

1. Sampling of a windrow for final acceptance of gradation material is allowable when there is no conveyor belt available.

- 2. The windrow sampling location will be randomly selected by WYDOT personnel with notification given to the contractor's representative so that arrangements can be made for the proper equipment (blade, loader bucket, or jersey spreader).
- 3. Flatten the windrow to approximately an 8 inch depth for at least 6 feet in length.
- 4. Divide the spread-out windrow into four quarters. Sample each quarter getting enough material from each quarter so that when combined, the sample will weigh at least 30 lb. Use a flat square nose shovel to dig into each quarter at a 45 degree angle, sampling the entire 8 inch depth while being careful not to contaminate any of the samples with material from beneath the flattened windrow.

## Stockpile

- 1. It is recommended that every effort be made to get conveyor belt samples during preliminary production and stockpiling. In sampling material from stockpiles, it is difficult to ensure unbiased samples.
- 2. Stockpile samples which can be taken of a finished product for project acceptance is limited as described per *WYDOT Standard Specifications* Section 800.2 (Point of Sampling).

Note: All other aggregates will be sampled from either the conveyor belt or a windrow.

- 3. A representative sample of the aggregate is difficult to obtain when sampling a stockpile due to segregation of the material. A visual examination of stockpiles will show segregation along the outside slope and base of the pile, with the coarser material usually rolling along the outside slope. Shoveling to get a representative samples from the base or slope is not practical. Therefore, it will be necessary to use a loader to dig into the stockpile and transfer the material to a flat level surface. In some unusual cases depending on the variability of the material, it may be necessary to sample the pile at more than one location.
- 4. Spread the material and flatten to approximately an 8 inch depth.
- 5. Divide the flattened material into four quarters. Sample each quarter to get enough material from each quarter so when combined the sample will weigh at least 30 lb. Use a flat square nose shovel to dig into at a 45 degree angle; sample the entire 8 inch depth being careful not to contaminate the samples with underlying material.

## **Check Samples**

- 1. When check samples are taken, approximately 30 lb of additional material will be needed. Combine both samples. Split out approximately a 30 lb field sample and send the remaining sample to the Materials Program in a canvas sack.
  - Note: Preliminary crushing tests are for informational purposes only and are not to be used for final acceptance. During preliminary crushing, tests for correlation of testers can be performed and reported on Form T-165AG. Refer to WYDOT 126.0 for correlation procedure.

#### SAMPLE SPLITTING BY MECHANICAL SPLITTER

Scope: This method covers the procedure for reducing a representative sample of aggregate to the appropriate size for testing. This technique is intended to minimize variation of sample characteristics between representative field sample and test samples. This method is intended to be conducted such that the smaller test sample portion is representative of the larger sample and thus, of the total supply.

This procedure is technically equivalent but not identical to AASHTO T 248 Standard Method of Test for Reducing Samples of Aggregate to Testing Size.

- Apparatus: Sample Splitter having
  - 1. An even number of equal width chutes, but not less than a total of eight for coarse aggregate or twelve for fine aggregate which discharge alternately to each side of the splitter.
  - 2. A minimum width of the individual chutes that are approximately 50 percent larger than the largest particle in the sample to be split for coarse aggregate and mixed aggregate. For dry fine aggregate, this minimum width must be at least 50 percent larger than the largest particle in the sample and the maximum width will be <sup>3</sup>/<sub>4</sub> inch.
  - 3. Two receptacles, metal pans of any type, to hold the split halves of the sample following the splitting process.
  - 4. A hopper or straight-edged pan with a width equal to or slightly less than the overall width of the assembly chutes to feed a sample at a controlled rate to the chutes.
  - 5. All splitter and accessory equipment should be designed so that the sample will flow smoothly without restriction or loss of material.

| Reference  |              |           |             |       |      |     |          |         |    |
|------------|--------------|-----------|-------------|-------|------|-----|----------|---------|----|
| Documents: | AASHTO T 248 | Standard  | Method      | of    | Test | for | Reducing | Samples | of |
|            |              | Aggregate | e to Testin | g Siz | z,e  |     |          |         |    |

Selection of Method: Fine Aggregate

> Reduce samples of the fine aggregate that are drier than the saturatedsurface-dry condition in size by use of a mechanical splitter. Samples having free moisture on the particle surfaces may be reduced in size by use of a mechanical splitter after drying to saturated-surface-dry conditions. To dry samples to saturated-surface-dry, use temperatures that do not exceed those specified for any tests contemplated. Alternatively, if the moist sample is very large, a preliminary split may be made using a

mechanical splitter having wide chute openings of 1<sup>1</sup>/<sub>2</sub> inch or more to reduce the sample to not less than 11 lb. As a quick approximation, if the fine aggregate will retain its shape when molded in the hand, it is considered wetter than saturated-surface-dry.

Coarse Aggregate and Mixtures of Coarse and Fine Aggregate

Reduce the sample in accordance with this procedure.

Avoid splitting samples when reducing the sample size will result in nonrepresentative split samples. Aggregate samples having relatively few large-sized particles in the sample dictates by the laws of chance that these few particles would not be equally distributed.

Procedure: Ensure that the splitter is placed on a level surface and is secure to the floor; the splitter should not rock or wobble. Uniformly place the sample to be split in the hopper so that when it is introduced into the chutes, approximately equal amounts will flow through each chute. **Do not** use your hands to redistribute the material.

Introduce the sample at a rate that allows free flow through the chutes and into the receptacles below.

Reintroduce the portion of the sample in one of the receptacles into the splitter as many times as necessary to reduce the sample to the size specified for the intended test. The portion of the material collected in the other receptacle may be reserved for reduction in size for other tests.

## SOUNDNESS OF AGGREGATE BY USE OF SODIUM SULFATE OR MAGNESIUM SULFATE

- Scope: This test method describes the procedure to determine the resistance of aggregates to break down or disintegrate.
- Use: This testing requires repeated immersions of the aggregate in saturated solutions of sodium or magnesium sulfate. The procedure simulates weathering conditions.

#### Reference

| AASHTO T 104  | Standard Method of Test for Soundness of Aggregate by |
|---------------|---|
|               | Use of Sodium Sulfate or Magnesium Sulfate            |
| WYDOT E-46    | Job Mix Formula                                       |
| WYDOT T-100PE | Portland Cement Concrete Mix Design: Pavement         |
| WYDOT T-100SE | Portland Cement Concrete Mix Design: Structural       |
|               | WYDOT E-46<br>WYDOT T-100PE                           |

# Procedure: Perform according to AASHTO T 104 Standard Method of Test for Soundness of Aggregate by Use of Sodium Sulfate or Magnesium Sulfate.

Test results using the two salts (MgSO4 or NaSO4) differ considerably and care must be taken in using the appropriate salt solution. Use the salt solution specified; typically sodium sulfate is used on concrete aggregate and magnesium sulfate used on base and hot plant mix aggregate.

The required number of cycles is five, and the test will be performed on both Coarse (plus No. 4) and Fine (minus No. 4) material for concrete aggregate and the coarse aggregate for other surfacing aggregates.

Report test results on the appropriate Form:

E-46, Job Mix Formula (Contractor Furnished Sources) T-100PE, Portland Cement Concrete Pavement Mix Design T-100SE, Structural Concrete Mix Design (This page intentionally left blank.)

## LIQUID LIMIT TEST

Definition: The liquid limit of a soil is the moisture content at which the soil passes from a plastic to a liquid state. This procedure is technically equivalent to AASHTO T 89, except the number of blows for groove closure may be between 16 to 36 inclusive and the number is not checked according to AASHTO T 89.

Reference

| AASHTO T 89  | Standard Method of Test for Determining the Liquid Limit |
|--------------|--|
|              | of Soils   |
| WYDOT 802.0  | Preparation of Samples for Physical Tests                |
| WYDOT 813.0  | Plastic Limit Test & Plasticity Index                    |
| WYDOT 814.0  | Sieve Analysis of Combined Aggregate                     |
| *WYDOT T-102 | Report of Field Tests on Surfacing Materials             |
| WYDOT T-166  | Aggregate Analysis                                       |
|              | WYDOT 813.0<br>WYDOT 814.0<br>*WYDOT T-102               |

\* Note: Use of weekly reports is optional

- Apparatus: 1. Liquid limit device
  - 2. Grooving tool
  - 3. Porcelain dish
  - 4. Spatula
  - 5. Gram balance (sensitive to 0.1 g)
  - 6. Graduated cylinder (recommend 100 ml)
  - 7. Moisture tins (recommend 3 oz)
  - 8. Drying stove
- Sample: A representative 100 g sample will be taken from material passing the No. 40 sieve which has been prepared in accordance with WYDOT 802.0 *Preparation of Samples for Physical Tests*.

Adjustment of Liquid Limit Device:

- 1. Inspect the following:
  - a. Liquid limit device to determine that the device is in good working order
  - b. The pin connecting the cup is not worn excessively to allow side play
  - c. The screws connecting the cup to the hanger arm are tight
  - d. The points of contact on the cup and base are not excessively worn
  - e. The lip of the cup is not excessively worn
  - f. A groove has not been worn in the cup through long usage

The grooving tool will be inspected for excessive wear. Wear is considered excessive when:

- a. The point of contact on the cup or base exceeds approximately 13 mm in diameter, or
- b. When any point on the rim of the cup is worn to approximately  $\frac{1}{2}$  the original thickness.

Although a slight groove in the center of the cup is noticeable, it is not objectionable. If the groove becomes pronounced before other signs of wear appear, the cup should be considered excessively worn. Excessively worn cups will be replaced.

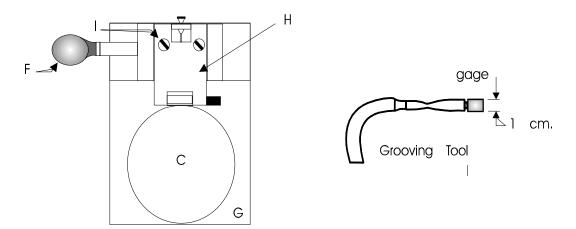


Figure 1 - Liquid Limit Device and Grooving Tool

- 2. By means of the gage on the handle of the grooving tool and the adjustment plate H, Figure 1, the height to which the cup C is lifted must be adjusted so that the point on the cup which comes in contact with the base G, is exactly 10 mm above the base. The adjustment plate H will then be secured by tightening the screws, I. With the gage still in place, check the adjustment by revolving the crank several times. If the adjustment is correct, a slight ringing sound (shock) will be heard when the cam strikes the cam follower. If the cup is raised off the gauge or no sound is heard, further adjustment should be made.
- Procedure: 1. Place the soil sample in the porcelain dish and thoroughly mix with 15 to 20 mL of water, by alternately and repeatedly stirring, kneading, and chopping with a spatula. Further additions of water will be made in increments of 1 to 3 mL and mixed thoroughly.
  - Note: If the Plastic Limit Test is to be run on this material, follow Section WYDOT 813.0.
  - 2. When sufficient water has been thoroughly mixed with the sample for a trial, place a sufficient quantity of material in the cup above the spot where

the cup rests on the base and squeeze and spread into position as shown in Figure 2a; take care to prevent the entrapment of air bubbles within the mass. With the spatula, level the soil and trim to a depth of 10 mm at the point of maximum thickness. Divide the soil in the cup by use of the grooving tool (Figure 2b). To avoid tearing of the sides of the groove, or having the soil slip to the back of the cup, up to six strokes with the grooving tool permitted, with one stroke counting as the tool moves from front to back or from back-to-front along centerline of the soil. Increase the depth of the groove with each pass of the grooving tool. The last pass of the grooving tool should scrape the bottom of the cup. The groove separation should be approximately 1/16 inch, the width of the grooving tool cutting edge.

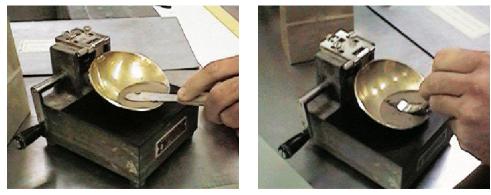
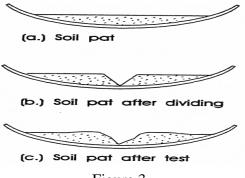


Figure 2a

Figure 2b

3. Turn the crank, F, at the rate of two revolutions per second until the two sides of the sample come in contact at the bottom of the groove for a distance of 0.5 inch, Figure 3 (c.), using from 16 to 36 shocks. Do not hold the base of the machine with the free hand while the crank is turned.



- Figure 3
- 4. If the soil pat does not close the required distance, incorporate additional water at a rate of 1 to 2 ml, thoroughly mix, and repeat test. If the soil pat closes over the required distance before achieving 16 blows, obtain a new 100 g sample and repeat with less water. Once testing has begun, no additional dry soil should be added to the moistened soil.

- 5. When the soil pat closes the required distance within the 16 to 36 shocks, take a moisture sample as follows: Slice the soil, about 0.75 inch in width, extending from edge to edge of the soil pat at right angles to the groove and including that portion of the groove in which the soil flowed together.
- 6. Place the moisture sample in a moisture tin, weigh, dry over a stove, and weigh again. Take care to avoid burning the moisture sample.

Calculation of Moisture:

| (Wet soil and tin, g) - (Dry soil and tin, g) | = Weight of water, g    |
|---|-------------------------|
| (Dry soil and tin, g) - (Tare of tin, g)      | = Weight of Dry soil, g |

% of Moisture =  $\frac{\text{Weight of Water, g}}{\text{Weight of Dry Soil, g}} \times 100$ 

% moisture in sample x correction factor = Liquid Limit

Note: Liquid Limit is rounded to the whole number.

7. On some sandy materials, the liquid limit cannot be determined. The material in the cup will slide or bounce together, rather than flow together. In this case, mark the liquid limit as no value (NV) and the plastic index as non-plastic (NP).

| CORRECTION CHART |                   |                  |                   |  |
|------------------|-------------------|------------------|-------------------|--|
| Number of Shocks | Correction Factor | Number of Shocks | Correction Factor |  |
| 16               | 0.947             | 27               | 1.009             |  |
| 17               | 0.954             | 28               | 1.014             |  |
| 18               | 0.961             | 29               | 1.018             |  |
| 19               | 0.967             | 30               | 1.022             |  |
| 20               | 0.973             | 31               | 1.026             |  |
| 21               | 0.979             | 32               | 1.030             |  |
| 22               | 0.985             | 33               | 1.034             |  |
| 23               | 0.985             | 34               | 1.038             |  |
| 24               | 0.995             | 35               | 1.042             |  |
| 25               | 1.000             | 36               | 1.045             |  |
| 26               | 1.005             |                  |                   |  |

8. Record daily test results on Form T-166, *Aggregate Analysis* and weekly test results on optional Form T-102, *Report of Field Test on Surfacing Materials*. For examples, see section WYDOT 814.0.

## PLASTIC LIMIT TEST AND PLASTICITY INDEX

- Definition: The plastic limit of a soil is the lowest moisture content determined in accordance with the following procedure at which the soil remains plastic. This procedure is technically equivalent, but not identical to AASHTO T 90.
- Apparatus: 1. Porcelain dish
  - 2. Spatula
  - 3. Ground glass plate
  - 4. Graduated cylinder (recommend 100 ml)
  - 5. Gram balance sensitive to 0.1 g
  - 6. Moisture tin (recommend 3 oz)
  - 7. Drying stove

#### Reference

| Documents: | AASHTO T 90  | Standard Method of Test for Determining the Plastic Limit and Plasticity Index of Soils |
|------------|--------------|---|
|            | WYDOT 812.0  | Liquid Limit Test   |
|            | WYDOT 814.0  | Sieve Analysis of Combined Aggregate  |
|            | *WYDOT T-102 | Report of Field Tests on Surfacing Materials  |
|            | WYDOT T-166  | Aggregate Analysis  |

\* Note: Use of weekly reports is optional

- Sample: The material to be used for the plastic limit test can be taken from any stage of the mixing operation of the liquid limit test, or at a stage when the material becomes plastic enough to be easily shaped into a ball without sticking to the fingers excessively when squeezed, check WYDOT 812.0. If the sample for plastic limit is taken during mixing operation of the Liquid Limit test, set it aside and allow to season in air until completion of the Liquid Limit test. If the sample is too dry to permit rolling to a <sup>1</sup>/<sub>8</sub> inch thread, add more water and re-mix.
- Procedure: 1. Form a portion of the soil to be tested that is enough to produce a thread <sup>1</sup>/<sub>8</sub> inch in diameter and 6 inches long into an ellipsoidal ball. Roll between the fingers and the ground glass plate with just-sufficient pressure to produce a thread of uniform diameter (Figure 1). The rate of rolling will be between 80 and 90 strokes per minute. A stroke is counting one complete motion of the hand forward and back to the starting position again. Continue rolling, causing the thread to slowly elongate and decrease in diameter.

Figure 1

1



- 2. When the diameter of the thread becomes  $\frac{1}{8}$  inch, break and re-roll the thread: Continue this alternate rolling to a  $\frac{1}{8}$  inch diameter thread, gathering together, kneading and rolling, until the thread crumbles under the slight pressure required for rolling and the soil can no longer be rolled into a  $\frac{1}{8}$  inch thread. Crumbling may occur when the thread has a diameter greater than  $\frac{1}{8}$  inch. Consider this a satisfactory end point, provided the soil has previously rolled into a thread  $\frac{1}{8}$  inch in diameter.
- 3. As the soil crumbles, place the soil in a tared moisture tin with an air-tight lid until you have approximately 15 to 20 g of material. To avoid moisture loss, keep tin covered until wet weight has been recorded. Thoroughly dry the sample, using extreme care not to burn the sample. Record the dry weight of the material and container.

| Calculation of Moisture: | (Wet soil and tin, g) - (Dry soil and tin, g) | = Weight of water, g    |
|--------------------------|---|-------------------------|
|                          | (Dry soil and tin, g) - (Tare of tin, g)      | = Weight of Dry soil, g |

% of Moisture =  $\frac{\text{Weight of Water,g}}{\text{Weight of Dry Soil,g}} \times 100$ 

The percent of moisture is the plastic limit.

Note: Plastic limit and plastic index is rounded to the whole number.

## PLASTICITY INDEX

Definition: The plasticity index (PI) of a soil is the numerical difference between liquid limit and the plastic limit. It is the range in water content within which the material is in a plastic state.

Calculation to determine Plastic Index:

(Liquid Limit) - (Plastic Limit) = Plasticity Index Non-Plastic Soils (NP)

- 1. When the plastic limit is equal to or greater than the liquid limit, mark the plasticity index as non-plastic (NP).
- 2. When soil cannot be rolled to a tread of  $\frac{1}{8}$  inch diameter in the first try when the moisture is equal to or slightly greater than the liquid limit, the soil is non-plastic (NP).
- 3. Record daily test results on Form T-166, *Aggregate Analysis* and weekly test results on optional Form T-102, *Report of Field Test on Surfacing Materials*. For example, see section WYDOT 814.0. Refer to routing on form.

## SIEVE ANALYSIS OF COMBINED AGGREGATE

Scope: This procedure is technically equivalent, but not identical to AASHTO T 27 and AASHTO T 11. This test method describes the procedure for determining particle size distribution of a combined aggregate using a large mechanical sieve shaker. A combined aggregate is defined as an aggregate containing both coarse and fine fractions. The results will primarily be used to determine compliance with specifications of product control of the following:

| Hot Plant Mix                   | Base                |
|---------------------------------|---------------------|
| Plant Mix Wearing Course        | Subbase             |
| Chip Seal                       | Concrete            |
| Micro surfacing                 | Blotter             |
| Maintenance Stockpile Aggregate | Bed Course Material |
| Gravel for Drains               | Class B Bedding     |
| Pervious Backfill               | Riprap Filter       |
| Gravel for Bedding              | Etc.                |

- Apparatus: 1. Large mechanical shaker with appropriate sized testing screens. For example: (Gilson model TS-1 or TS-2)
  - Note: A large mechanical shaker must be able to handle a 30 lb sample without overloading the screens. The stack of 8 inch or 12 inch sieves is not equivalent to a large mechanical shaker.
  - 2. Washpan with sufficient capacity to allow enough water to completely cover wash sample
  - 3. Balance(s)

| Scale Sensitivity | * Sample Weight |
|-------------------|-----------------|
| 0.1 g             | 4 lb or less    |
| 1.0 g             | 4 lb to 11 lb   |
| 5.0 g             | 11 lb to 44 lb  |
| 20.0 g            | 44 lb plus      |
|                   |                 |

\* Based off of nominal maximum size

- 4. Drying stove
- 5. Splitting device
- 6. 8 inch U.S. standard sieves with a snug-fitting nested cover
- 7. 8 inch sieve shaker with a minimum <sup>1</sup>/<sub>4</sub> hp motor, combined back and forth lateral motion and up-and-down tilting motion, and 15 minute electric reset timer switch with a hold feature for continuous operation

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| Reference  |              |  |
|------------|--------------|--|
| Documents: | AASHTO T 11  | Standard Method of Test for Material Finer Than 75-µm  |
|            |              | (No. 200) Sieve in Mineral Aggregates by Washing       |
|            | AASHTO T 27  | Standard Method of Test for Sieve Analysis of Fine and |
|            |              | Coarse Aggregates                                      |
|            | WYDOT 803    | WYDOT Standard Specifications                          |
|            | WYDOT 802.0  | Preparation of Samples for Physical Tests              |
|            | WYDOT 804.0  | Aggregate Sampling                                     |
|            | WYDOT 805.0  | Sample Splitting by Mechanical Splitter                |
|            | WYDOT 812.0  | Liquid Limit Test                                      |
|            | WYDOT 813.0  | Plastic Limit Test and Plasticity Index                |
|            | *WYDOT T-102 | Report of Field Tests on Surfacing Materials           |
|            | WYDOT T-120  | Pay Adjustment for Aggregate Gradation                 |
|            | WYDOT T-166  | Aggregate Analysis                                     |
|            |              |  |

\* Note: Use of weekly reports is optional

- Sampling: The sampling location and procedure is outlined in section WYDOT 804.0. Aggregate to be tested for gradation acceptance should be free of any additives.
  - Note: Before proceeding, check the equipment; (scale, sieves, etc.). Check for condition, calibration, level and cleanliness. Nest the required sieves in the proper order.
- Procedure: 1. Weigh the entire sample. Record the wet weight (mass) in the "% Moisture" section on Form T-166, *Aggregate Analysis*.
  - Note: Weigh material to the nearest 0.1 percent of the total original dry sample mass. Requirement for 30 lb to 50 lb sample weight is to the nearest hundredth (0.01).
  - 2. Dry the sample. Control the temperature so the heat used will allow steam to escape without generating enough pressure to fracture any of the particles of the sample.
  - 3. Allow the test sample to cool to room temperature, weigh the dried and cooled test sample.

Record this weight (mass) as the Dry weight in the % Moisture Section.

The Dry weight (mass) is subtracted from the Wet weight (mass) to determine the amount of moisture. The amount of moisture is divided by the Dry weight times 100 to determine the percent of moisture in the sample.

$$Wet - Dry = Moisture$$

% Moisture = 
$$\frac{\text{Moisture}}{\text{Dry}} x \ 100$$

Constant mass is when the weight does not change by more than 0.1 percent of the original dry sample mass.

 $\frac{\text{Original Dry Weight}}{\text{Dry Weight}} x \ 100 = \text{within } 0.1\%$ 

Note: Original Dry weight (mass) may change as sample becomes drier.

4. Determine test sample size.

Generally it is not necessary to reduce the sample weight by splitting to less than 30 lb when using the large mechanical sieve shaker. Take care not to overload an individual sieve when working with aggregates, which typically collect on the No. 4 sieve. If it is necessary to reduce the sample size, follow procedure WYDOT 805.0 *Sample Splitting by Mechanical Splitter*. A larger test sample should increase the accuracy of the results. In no case should the size of the test sample be less than:

| Nominal Maximum Size  | Minimum Weight<br>of Test Sample        |
|---|---|
| Aggregate<br><sup>3</sup> / <sub>8</sub> inch<br><sup>1</sup> / <sub>2</sub> inch<br><sup>3</sup> / <sub>4</sub> inch<br>1 inch<br>1 <sup>1</sup> / <sub>2</sub> inch | 2 lb<br>4 lb<br>11 lb<br>22 lb<br>30 lb |

- Note: Nominal maximum size aggregate is one size larger than the first specification sieve to retain more than 10 percent.
- 5. Clamp down the sieve trays, start shaker, then slowly add sample. Follow the instructions outlined in the mechanical sieve shaker "Operating and Service Manual" for tightening the sieve trays. Shake until no material can be observed falling free from one sieve to another.
  - Note: Excessive time (more than approximately ten minutes) to achieve adequate sieving may result in damage to the sample.
- 6. Continue sieving for a sufficient time period and in such manner that, after completion, not more than 0.5 percent by mass of the total sample passes any sieve during one minute of continuous hand sieving performed as follows:

Selecting the sieve with the most retained material, hold the individual sieve, with a snug fitting pan and cover attached, in a slightly inclined position in one hand. Strike the side of the sieve sharply and with an upward motion against the heel of the other hand at the rate of about 150 times per minute, turn the sieve about

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one-sixth of a revolution at intervals of about 25 strokes. In determining sufficiency of sieving for sizes larger than the No. 4 sieve, limit the material on the sieve to a single layer of particles. If the size of the mounted testing sieves makes the described sieving motion impractical, use 8 inch diameter sieves to verify the sufficiency of sieving.

Note: The hand sieve check will be necessary when establishing the shake time for each type of material being tested. Hand sieving will not be required during subsequent tests for the same material. Altering the testing method will require another check (i.e. switching material types or sources, changing tester, or changing equipment used).

```
\frac{\text{Weight Passing after hand sieving}}{\text{Individual Sieve Weight Retained}} \times 100 = \text{not more than } 0.5\%
```

| Table 1. – Maximum Allowable Weight |       |  |  |
|-------------------------------------|-------|--|--|
| Sieve Size lb                       |       |  |  |
| 1 inch                              | 30.60 |  |  |
| <sup>3</sup> / <sub>4</sub> inch    | 23.26 |  |  |
| <sup>1</sup> / <sub>2</sub> inch    | 15.31 |  |  |
| <sup>3</sup> / <sub>8</sub> inch    | 11.63 |  |  |
| No. 4                               | 5.82  |  |  |

- Note: If the sieve with the most retained material meets the criteria, the other sieves do not need to be checked. Check overloads using Table 1 Maximum Allowable Weight.
- 7. Weigh the material retained on each sieve and pan.
  - a. Following adequate sieving time, each sieve is removed from the sieve shaker and the material retained is weighed and recorded on Form T-166, *Aggregate Analysis* in the "Coarse Aggregate" section, column "Wt. Ret.", "K", next to the appropriate sieve size.
    - Note: Weigh material to the nearest tenth percentage (0.1%) of the original dry sample mass. Requirement for 30 lb to 50 lb sample weight is to the nearest hundredth (0.01).
  - b. Determine item "A" (sum of the weight retained on the plus No. 4 material):

 $A = \Sigma$  Weight retained on No. 4 and larger sieves, lb

c. The pan or minus No. 4 material weight should be recorded in column "K" as Pan just above the TOTAL (Pass No. 200), Pan and also as Item "B."

d. The total of column "K", the material mass on sieves and in the pan will be within 0.3 percent, based on the original dry sample mass recorded as Dry Weight in the % Moisture Section in Step 4.

$$\frac{E-D}{E} \times 100 = \text{percent change}$$

- Note: If the percent change differs by more than 0.3 percent, based on the original dry sample mass, the results should not be used for acceptance evaluation and another sample should be obtained.
- e. Determine item "H" (percent retained plus No. 4 material):

$$H = \frac{A}{D} \times 100$$

f. Determine item "I" (percent passing the No. 4 sieve):

$$I = \frac{B}{D} \times 100$$

Note: On Form T-166, Aggregate Analysis items

Combined Aggregate items:

- A = Sum of weight retained No. 4 material and above, lb
- B = Weight passing No. 4 sieve, lb
- D = Total dry sample weight measured after sieving, lb
- E = Total dry sample weight, lb
- H = Percent retained plus No. 4 material
- I = Percent passing minus No. 4 material
- K = Weight retained per sieve and Pan, lb
- 8. Split the fines (minus No. 4 material) to a minimum of 300 g.

Follow the procedure outlined in WYDOT 805.0 Sample Splitting by Mechanical Splitter.

9. After splitting, weigh the reduced fines (minus No. 4) sample.

Record the weight in "Fine Aggregate" section as "Sample Wt." item "F".

Note: Record fines (minus No. 4) to the nearest 0.10 of a g.

10. Wash the fines (minus No. 4 material).

Add enough water to the sample container to cover the sample. Agitate with sufficient vigor to separate and suspend the minus No. 200 material. Pour off the dirty water into a nested No. 8 and No. 200 sieve (8 inch or 12 inch diameter). The No. 200 sieve should be placed in the sink with one side propped up about ½ inch so that the water will flow freely. Add more water, agitate, and pour off the dirty water. Repeat this operation until the wash water is clear. Fines retained on the No. 200 sieve after washing will need to be cleaned of any trapped minus No. 200 material.

Use tool or spoon to agitate the material in the wash pan; do not use hand or any tool on the material within the No. 200 sieve or on the screen itself. Do not hit the screen. Wash the retained material into a pile on one side of the screen.

With the sieve held over the sink, use the heel of free hand to tap the outside edge to help dry and loosen the retained material. When the material starts moving around, empty the material into the washpan by tapping on the outside edge of the sieve. Any material still retained should be washed into the washpan using as little water as possible.

11. Dry the washed sample.

If direct heat is used, popping or sputtering can be controlled by covering the sample container. After enough steam has escaped, the sample can be uncovered. Make sure any material retained on the cover is returned to the sample.

If oven drying is used, "dry" is when the fines are a constant mass at a temperature of  $230 \pm 9$  °F.

12. Weigh the dried wash sample.

Record the weight (mass) in the "Fine Aggregate" section as the "After Wash" weight just below item "F".

- Note: The sample should be allowed to cool to room temperature before recording the final "After Wash" weight (mass) and before placing into 8 inch sieves.
- 13. Sieve the sample through 8 inch U.S. Standard sieves.

Pour the washed, dried and weighed fine aggregate into a nest of U.S. Standard sieves from the No. 4 down to the No. 200 including the pan. The amount of material on any 8 inch sieve should not exceed 200 g. The amount of material on a screen may be reduced by sieving the sample in small portions or by the addition of a sieve above the screen which may be overloaded. See Step 6 for a discussion of shaking time.

- Note: Sieves required for specified testing are listed in the WYDOT Standard Specifications Section 803 or provided by WYDOT Material Program Mix Design Letters.
- 14. Weigh the material retained on each sieve.

Record the weight of the retained material from each sieve in the "Fine Aggregate" section, column "Wt. Ret." Item "P."

The material in the pan should be weighed and recorded at the top in the "Fine Aggregate" section as weight passing No. 200 Pan.

Determine "Total Pass No. 200" by subtracting the "After Wash" weight from the "Sample Weight" and adding the "Weight Pass No. 200 Pan".

Total Pass No. 200 = (Sample Weight) – (After Wash Weight) + (Pan Weight)

Note: Calculate the "Pass No. 200" as material washed out of the sample. The material washed out plus the material in the pan is the "Total Pass No. 200".

The "Total Pass No. 200" in the "Coarse Aggregate" section, is the weight entered in "Coarse Aggregate" section, column "Wt. Ret., item "K" Pass No. 200, Pan.

The Total for "Coarse Aggregate" section, Weight Retained column, item "K" should equal item "E"

- Note: Record "Fine Aggregate" weight to the nearest tenth (0.1) of a g and the "Total Pass No. 200" weight to the nearest tenth (0.1).
- 15. Determine the percent retained for each sieve for both Coarse and Fine Aggregates sections, column % Ret. item "L" and item "R."

Note: Record calculated percent retained results to the nearest tenth (0.1).

Coarse Aggregate: "Percent Retained" column, item "L" is found by dividing the weight retained on each sieve in item "K" by the total sample weight item "E" and multiplying by 100.

$$L = \frac{K}{E} \ge 100$$

Note: Report the weight for "Pass No. 200, Pan" before splitting in item "K".

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The total for "Coarse Aggregate" column, % Retained column item "L", should equal 100 percent.

Fine Aggregate: "Percent Retained" column item "R", is calculated by dividing the weight retained on each sieve in item "P" by the "Fine Aggregate" sample weight item "F" (before wash).

 $R = \frac{P}{F} \times 100$ 

The total for "Fine Aggregate" column, % Retained column item "R", should equal 100 percent.

16. Determine item "S":

"Fine Aggregate", Percent Retained (% Ret) item "S", is found by multiplying item "R" by item "I" (Total Sample Wt. Washed) and dividing by 100.

$$S = \frac{R \times I}{100}$$

The total for "Fine Aggregate" column, % Retained item "S", should equal item "I".

Coarse Aggregate items:

K = Weight retained per sieve, lb

L = Percent retained per sieve based on total sample weight item "E", %

Fine Aggregate items:

- F = Fine Aggregate total dry sample weight, lb
- P = Weight retained per sieve, lb
- R = Percent retained per sieve based on total sample weight item "F", washed, %
- S = Percent retained per sieve based on total sample, %
- 17. Determine the percent retained for the Combined Sample for each sieve size and record in the "Combined Aggregate" section, Percent Retained column item "Z."

$$Z = L + S$$

18. Find the "Combined Aggregate" column, % Passing column, "to 0.1%". Begin subtracting from 100 at the Maximum Aggregate size, 100 minus the sum of item "Z".

% passing = 
$$100.0 - \Sigma Z$$

The percent passing the No. 200 should equal "Fine Aggregate", Percent Retained (% Ret) column item "S", Pass No. 200.

- Note: In the "to 1%" column, round each result to the nearest whole number and record the result in the "Combined Aggregate" section, % Passing column item 1%. For the No. 200 sieve, round the result to the nearest tenth percent (0.1%) except when over 10 percent. These are the results that should be used for analysis.
- Note: For evaluating gradation for acceptance in the CMS, enter the gradation test result to the nearest tenth (0.1). This will allow the acceptance to be calculated with the correct significance level (whole number) and also allow verification comparisons. Results produced from CMS on E-120 (Pay Adjustment for Aggregate Gradation).

If calculating the acceptance outside of the CMS, round the gradation test result to the nearest whole number except for the No. 200 sieve which is rounded to the nearest tenth (0.1). If determining verification comparisons outside of the CMS, round the gradation test result to the nearest tenth (0.1).

- 19. Atterberg limits should be determined in accordance with procedures outlined in WYDOT 802.0, WYDOT 812.0, and WYDOT 813.0.
- 20. Record the weekly results on optional Form T-102, *Report of Field Tests* on *Surfacing Materials*. Refer to routing on the forms. For Example of Form T-102 see pages following in this section.

#### WYOMING DEPARTMENT OF TRANSPORTATION **T-166** MATERIALS TESTING LABORATORY

(Rev. 10-18)

AGGREGATE ANALYSIS

| PROJECT NO(S).: ERP Project Number   |  |                                |  |                        |             |  |
|--|--|--------------------------------|--|------------------------|-------------|--|
| ENGINEER: Resident Engineer<br>SAMPLE I.D.:<br>PIT OR QUARRY: As Listed on Plans |  |                                |  |                        |             |  |
|  |  |                                |  | QUANTITY: As Per Plans |             |  |
|  |  |                                |  | ED: mm/dd/yr.          | »: mm/dd/yr |  |
| WEIGH  | AACIZIIC                                 | % Retained =                   |  |                        |             |  |
| COARSE AGO   | Retained                                 | A or B<br>D x 10               |  |                        |             |  |
| 13.94 =  | (lbs or kg)                              |                                |  |                        |             |  |
| sh   | 4 [4.75 mm] = (A) $7.00$                 | 50.3 = (                       |  |                        |             |  |
| 75µm]  | 4 [4.75 mm]= (B) 6.91                    | 49.7 =                         |  |                        |             |  |
| µm], Pan   | $^{C}AL$ , A + B = (D) 13.91             |                                |  |                        |             |  |
| 0 [75µm]   |  |                                |  |                        |             |  |
| % RE   | COMBINED AGGREGAT                        | E                              |  |                        |             |  |
| WT RET KX1   | % PASSING<br>100 - S ( Z )               | SPEC                           |  |                        |             |  |
| =K =L  | to 0.1% to 1%                            | % PASSING                      |  |                        |             |  |
| nm]  | 100.0 100                                |                                |  |                        |             |  |
| 1  | 100.0 100                                | 100                            |  |                        |             |  |
| m] 0.40 <mark>2.9</mark>   | 97.1 97                                  | 90-100                         |  |                        |             |  |
| um] 2.20 15.8  | 81.3 81                                  | 76-86                          |  |                        |             |  |
| m] 2.50 17.9   | 63.4 63                                  | 58-68                          |  |                        |             |  |
| nm] 1.90 <mark>13.0</mark>   | 49.8 50                                  | 47-57                          |  |                        |             |  |
| nm]  | 38.3 38                                  | 37-45                          |  |                        |             |  |
| mm]  | 27.1 27                                  | 1.                             |  |                        |             |  |
| um]  | 18.3 18                                  | 18-24                          |  |                        |             |  |
| um]  |  |                                |  |                        |             |  |
| μm]  | 11.2 11                                  |                                |  |                        |             |  |
| μm]  | 6.9 7                                    |                                |  |                        |             |  |
| um]  | 4.1 4.1                                  | 2.6-6.6                        |  |                        |             |  |
| um], Pan 6.91 49.0   | 1  |                                |  |                        |             |  |
| SSING 13.91 99.  |  |                                |  |                        |             |  |
| OSS % 0.3%   | WET WT (lb or kg)                        | 14.4                           |  |                        |             |  |
| ACES % One of more   | DRY WT (b or kg)<br>WET - DRY = MOISTURE | 14.1<br>0.3                    |  |                        |             |  |
| S MODULUS: see M.T.M., S   | DIST.=(MOIST./ DRY WT)x100               | 2,1                            |  |                        |             |  |
| Tin         Wet+Tare=         Dry + Tr           No.         AA         BB       | COLUMN                                   | PLASTIC INDEX<br>(PD) =LL - PL |  |                        |             |  |
| (LL) 96.2 83.0   | 1.014 24.0                               | 10 T                           |  |                        |             |  |
|  | 1.V.1 CT.V                               | 3.0                            |  |                        |             |  |
| (LL) 96.2 83.<br>(PL) 91.8 80.5  | 1.014 24.0                               |                                |  |                        |             |  |

REMARKS

If value greater than 10, round to whole number. TESTED BY Field Tester

CERTIFICATION NO. ####



#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY REPORT OF FIELD TESTS ON SURFACING MATERIALS

Form T-102 (Rev. 09-16)

|                           |                            |                  | Report      | / Lot No(s).: | ###                       |  |  |
|---------------------------|----------------------------|------------------|-------------|---------------|---------------------------|--|--|
| Project No(s).: #######   |                            |                  |             | Location:     | On plans                  |  |  |
| Submitted By: Re          | y: Resident Engineer       |                  |             | At:           | Town                      |  |  |
| ID Marks: ସ୍ନ             | s: QA ####                 |                  | Quantity R  | epresented:   | I: Total Planned Quantity |  |  |
| Source: Pit               | Source: Pit or Quarry Name |                  | _           | For Use As:   | Grading Spec.             |  |  |
| Date Received: XX/XX/XXXX |                            | _ c              | ate Tested: | XX/XX/XXXX    |                           |  |  |
| Sampled (Check            | k One):                    | C Mechanical ID# | C Belt      | C Windrow     | C Stockpile               |  |  |

#### TEST RESULTS

| Test Number          | Test #         | Test #     | Test #     | Test #     | Test #     | Test #     | Test #     |
|----------------------|----------------|------------|------------|------------|------------|------------|------------|
| Date Tested          | XX/XX/XXXX     | XX/XX/XXXX | XX/XX/XXXX | XX/XX/XXXX | XX/XX/XXXX | XX/XX/XXXX | XX/XX/XXXX |
| Station Sampled      | ## + ##        | ## + ##    | ## + ##    | ## + ##    | ## + ##    | ## + ##    | ## + ##    |
| Tons Represented - T | Specifications |            |            |            |            |            |            |
| Asphalt Content      | %              | %          | %          | %          | %          | %          | %          |
| % Past 4"            |                |            |            |            |            |            |            |
| % Past 3"            |                | 5          |            |            |            |            |            |
| % Past 2"            |                |            |            |            |            |            |            |
| % Past 11⁄2"         | 100            | 100        | 100        | 100        | 100        | 100        | 100        |
| % Past 1"            | 95-100         | 100        | 100        | 100        | 100        | 100        | 100        |
| % Past ¾"            |                | 95         | 95         | 94         | 96         | 94         | 95         |
| % Past 1⁄2"          |                | 76         | 76         | 77         | 75         | 78         | 76         |
| % Past ¾"            |                | 64         | 65         | 64         | 63         | 65         | 64         |
| % Past No. 4         | 40-65          | 41         | 43         | 43         | 43         | 44         | 44         |
| % Past No. 8         | 30-55          | 33         | 31         | 34         | 34         | 35         | 36         |
| % Past No. 16        |                | 26         | 22         | 27         | 25         | 28         | 29         |
| % Past No. 30        |                | 20         | 18         | 21         | 19         | 22         | 23         |
| % Past No. 50        |                | 16         | 15         | 17         | 15         | 18         | 19         |
| % Past No. 100       |                | 13         | 12         | 14         | 12         | 15         | 16         |
| % Past No. 200       | 3-15           | 10.6       | 10.8       | 11.6       | 10.6       | 12.6       | 13.6       |
| Liquid Limit (LL)    |                |            |            |            |            |            |            |
| Plastic Index (PI)   |                |            |            |            |            |            |            |

\* Note: One Quality test not to represent more than 1000 T

| Quantity Placed:  | To Last Report Current To | ons   | Since Last Report Form Tons | Total To Date <u>Total Tons</u> |
|-------------------|---------------------------|-------|-----------------------------|---------------------------------|
| Does Material Mee | et Specifications?        | C YES |                             |                                 |
| Corrective Mea    | sures Taken               |       |                             |                                 |
|                   | <u>6</u> 2                |       |                             |                                 |

Remarks

Tested By\_\_\_\_\_ Certification No. WYDOT 814.0 (Rev. 10-18)

# Wyoming Department of Transportation

Pay Adjustment For Aggregate Gradation Lot Number: 6 Pay Factor To Be Assessed: 1.02 August 22, 2018

 Project Number: 1804281
 Prime Contractor: Croell, Inc.

 Road: Elk Mountain - Laramie (Cooper Cove Section)
 Crushing Company: Croell, Inc.

 County: Albany & Carbon Counties
 Testing Company: Croell, Inc.

 Material Type: HOT PLANT MIX (RECYCLE)
 Grading: 1/2<sup>min</sup>

 Units in Lot: 5,000.00
 Percent Rap: 15.00

 QC/QA Job: Yes
 Pit County: Carbon

 Resident Engineer: Steve Cook, P.E., Laramie (307)745-2115
 Pit: Brokow

 Notes:
 Notes:

| SIEVE SIZE: |          | 1/2"<br>(12.5 mm) | 3/8"<br>(9.50 mm) | No. 4<br>(4.75 mm) | (2.36 mm)       | No. 30<br>(600 µm) | No. 200<br>(75 μm) |              |
|-------------|----------|-------------------|-------------------|--------------------|-----------------|--------------------|--------------------|--------------|
|             | SPECS:   | 90.0 100.0        | 71.0 81.0         | 41.0 51.0          | 25.0 33.0       | 11.0 17.0          | 3.0 7.0            |              |
| TE          | ST NO .: | -=Indicated       | a percent pass    | ing value Out      | Of Specificatio | n on test num      | ber and sieve size | e annotated. |
|             | 51       | 96                | 77                | 50                 | 33              | 16                 | 5.5                |              |
| V           | 5-2      | 95                | 76                | 49                 | 32              | 16                 | 5.7                |              |
|             | 5-3      | 95                | 78                | 51                 | 33              | 17                 | 5.7                |              |
|             | 5-4      | 96                | 79                | 49                 | 31              | 16                 | 5.3                |              |
|             | 5-5      | 96                | 78                | 50                 | 31              | 16                 | 5.6                |              |
| ٧           | V-5      | 94                | 76                | 50                 | 34~             | 17                 | 5.2                |              |
| AV          | ERAGE:   | 95.6              | 77.6              | 49.8               | 32.0            | 16.2               | 5.6                |              |
| 24          | RANGE:   | 1.0               | 3.0               | 2.0                | 2.0             | 1.0                | 0.4                |              |
|             | STD:     | 0.548             | 1.140             | 0.837              | 1.000           | 0.447              | 0.167              |              |
| PAY F       | ACTOR:   | 1,05              | 1.05              | 1.04               | 1.02            | 1.05               | 1.05               |              |

| PAY ADJUST: | ITEM<br>NUMBER | PROJECT       | BID PRICE<br>PER UNIT | QUANTITY | PAY FACTOR<br>MINUS 1.00 | 0.67 X BID PRICE X (PAY FACTOR - 1) X LOT<br>SIZE |
|-------------|----------------|---------------|-----------------------|----------|--------------------------|---|
|             | 401.03310      | NHPPI-1804261 | \$31.75               | 5,000,00 | 0.02                     | \$2,127.25  |

Total Quantity: 5,000.00

Total Pay Adjust: \$2,127.25

# SIEVE ANALYSIS OF CONCRETE AGGREGATE

- Scope: This method is used for determining the distribution of particle sizes in fine and coarse aggregate including concrete or mortar. The determination of percent moisture and of the fineness modulus of concrete aggregate are also included.
- Use: This method is used to determine the particle size distribution (gradation) for both fine and coarse aggregate and the fineness modulus of fine aggregate in concrete aggregate for the purpose of determining specification compliance.
- Apparatus: (For Fine Aggregate Sieve Analysis)
  - 1. Standard 8 inch sieves
  - 2. Wash pan
  - 3. Sample splitter
  - 4. Gram scale, sensitive to 0.1 g
  - 5. 35 lb [15 kg] scale, sensitive to 0.01 lb [5 g]
  - 6. Drying stove

(For Coarse Aggregate Sieve Analysis)

- 1. Large mechanical sieve shaker (Gilson model TS-1, TS-2, or equivalent)
- 2. Drying stove
- 3. Splitting device
- 4. Balance(s)

| Scale Sensitivity | Sample Weight  |
|-------------------|----------------|
| 0.1 g             | 4 lb or less   |
| 1.0 g             | 4 lb to11 lb   |
| 5.0 g             | 11 lb to 44 lb |
| 20.0 g            | 44 lb plus     |
|                   |                |

Reference

| Documents: | AASHTO M 45<br>AASHTO T 11 | Standard Specification for Aggregate for Masonry Mortar<br>Standard Method of Test for Materials Finer Than 75-µm (No. |
|------------|----------------------------|--|
|            |                            | 200) Sieve in Mineral Aggregates by Washing  |
|            | AASHTO T 27                | Standard Method of Test for Sieve Analysis of Fine and Coarse Aggregates   |
|            | WYDOT 414                  | WYDOT Standard Specifications  |
|            | WYDOT 471.0                | WYDOT Concrete Mix Design Procedure  |
|            | WYDOT 472.0                | Contractor Concrete Mix Design Procedure   |
|            | WYDOT 803                  | WYDOT Standard Specifications  |
|            | WYDOT SS-500G              | WYDOT Supplementary Specification - Structural Concrete with   |
|            |                            | Quality Control and Quality Acceptance   |
|            | WYDOT 804.0                | Aggregate Sampling   |
|            | WYDOT 805.0                | Sample Splitting by Mechanical Splitter  |
|            | WYDOT 814.0                | Sieve Analysis of Combined Aggregate   |

WYDOT 816.0 (Rev. 10-18)

| *WYDOT T-101 | Report of Field Tests on Concrete Aggregate |
|--------------|---|
| *WYDOT T-102 | Report of Field Test of Surfacing Materials |
| WYDOT T-166  | Aggregate Analysis                          |

\* Note: Use of weekly reports is optional

Sampling: The sampling procedure is outlined in section WYDOT 804.0.

Sample frequency as per *WYDOT Standard Specifications* Subsection 414.4.2 and Table 414.4.2-1.

- Note: Before Procedure 1. Below, check the equipment; (scale, sieves, etc.). Check for condition, calibration, level and cleanliness. Nest the required sieves in the proper order.
- Procedure: Moisture Determination for Fine and Coarse Concrete Aggregate

Moisture determination for fine and coarse concrete aggregate should be performed for each sample taken or as specified in *WYDOT Standard Specifications* Table 414.4.2-1. See Example Form T-166 in this section.

- 1. Weigh the entire sample. Record the wet weight (mass), % Moisture Area on Form T-166.
  - Note: Weigh material to the nearest 0.1 percent of the total original sample mass. Requirement for 30 lb to 50 lb sample weight is to the nearest 0.01.
- 2. Dry the sample. Control the temperature so that the heat used will allow steam to escape without generating enough pressure to fracture any of the particles of the sample.
  - Note: A sample is considered dry when it is a constant mass at a temperature of  $230 \pm 9$  °F.

Original Dry weight (mass) may change as the sample becomes drier.

3. Allow the test sample to cool to room temperature, weigh the dried sample, and cool test sample.

Record this weight (mass) as the Dry weight in the % Moisture Section on Form T-166.

The Dry weight (mass) is subtracted from the Wet weight (mass) to determine the amount of moisture. The amount of moisture is divided by the Dry weight times 100 to determine the percent of moisture in the sample. Wet - Dry = Moisture

% Moisture 
$$=\frac{\text{Moisture}}{\text{Dry}} \times 100$$

Note: A sample is considered dry when it is a constant mass at a temperature of  $230 \pm 9^{\circ}$  F.

Constant mass is when the weight does not change by more than 0.1 percent of the original dry sample mass.

 $\frac{\text{Original Dry Weight}}{\text{Dry Weight}} \times 100 = \text{within } 0.1\%$ 

Procedure: Sieve Analysis for Fine Concrete Aggregate

1. Representative samples of fine aggregate are thoroughly dried to a constant mass and reduced to test size by splitting (WYDOT 805.0).

After splitting, weigh the reduced test size. For fine aggregate, the test size is a minimum of 500 grams. (No less than 300 grams after drying).

On Form T-166, record the weight in the "Fine Aggregate" section as "Sample Wt." Item "F".

Record the test sample weight to the nearest tenth (0.10) of a gram.

- 2. Wash the sample according to WYDOT 814.0, Steps 8 through 12.
- 3. Fine material which is washed into the No. 200 sieve from the aggregate should be cleaned. With the sieve held over the sink, use the heel of your free hand to tap the outside edge to help dry and loosen the retained material. When the material starts moving around, empty the material back into the washpan by tapping on the outside edge of the sieve. Any material still retained should be washed into the washpan using as little water as possible.
- 4. Dry the washed sample.

Place the pan and sample either on a stove or in an oven for drying.

If direct heat is used, popping and sputtering can be controlled by covering the sample container. After enough steam has escaped, the sample can be uncovered. Make sure any material retained on the cover is returned to the sample.

Dry is when the fines are a constant mass at a temperature of  $230 \pm 9$  °F.

Constant mass is when the weight does not change by more than 0.1 percent of the original dry sample mass.

 $\frac{\text{Original Dry Weight +Pan}}{\text{Dry Weight +Pan}} \times 100 = \text{within } 0.1\%$ 

- Note: The sample should be allowed to cool to approximately room temperature before recording the final "After Wash" weight (mass) and before putting into the 8 inch sieves.
- 5. Weigh the dried wash sample.

After the sample is thoroughly dry and cooled, weigh the sample. On Form T-166, record the weight (mass) in the "Fine Aggregate" section as the "After Wash Weight", just below Item "F".

6. Sieve the sample through 8 inch U.S. Standard sieves.

After the sample has been weighed, pour the material into the required nest of U.S. Standard sieves from the  $\frac{3}{8}$  inch on down to the No. 200 including the pan. Use a brush or a scraper to be sure you get all the sample fines out of the drying pan.

The amount of material retained on any one sieve must not weigh more than about 200 grams for the usual 8 inch diameter sieve.

Note: The amount of material on a sieve screen may be reduced by sieving the sample in smaller portions and mathematically recombining or by the addition of a sieve above the sieve which maybe overloaded.

In no case will fragments in the sample be turned or manipulated through the sieves by hand.

Continue sieving for a sufficient period and in such manner that, after completion, not more than 0.5 percent by mass of the total sample passes any sieve during one minute of continuous hand sieving performed as follows:

Selecting the sieve with the most retained material, hold the individual sieve, with a snug fitting pan and cover attached, in a slightly inclined position in one hand. Strike the side of the sieve sharply and with an upward motion against the heel of the other hand at the rate of about one-hundred-fifty times per minute, turn the sieve about one-sixth of a revolution at intervals of about twenty-five strokes.

Note: The hand sieve check will be necessary when establishing the

shake time for each type of material being tested. Hand sieving will not be required during subsequent tests for the same material. Altering the testing method will require another check (i.e. switching material types or sources, changing tester, or changing equipment used)."

 $\frac{\text{Weight Passing after hand seiving}}{\text{Individual Seive Weight Retained}} \times 100 = \text{not more than } 0.5\%$ 

- Note: If the sieve with the most retained material meets the criteria, the other sieves do not need to be checked.
- 7. Weigh the material retained on each sieve and record the weight.
  - Note: Sieves required for specified testing are listed in the WYDOT Standard Specifications Section 803 or provided by WYDOT Material Program mix design letters.

Record the weight of the retained material from each sieve in the "Fine Aggregate" section, column "Wt. Ret." Item "P" on Form T-166.

The material in the pan should be weighed and recorded at the top of Form T-166 in the "Fine Aggregate" section as weight passing No. 200 Pan.

Determine "Total Pass No. 200 by subtracting the "After Wash" weight from the "Sample Weight" and adding the "Weight Pass No. 200 Pan".

Total Pass No. 200 = (Sample WT.) - (After Wash WT.) + (Pan WT.)

Note: The Pass No. 200 is calculated material washed out of the sample. The material washed out plus the material in the pan is the Total Pass No. 200.

Record the weight (mass) of the minus No. 4 to the nearest tenth (0.10) of a gram.

- 8. Determine the percent retained for the "Fine Aggregates" section, column "% Ret." Item "R" on Form T-166.
  - Note: All calculated results should be recorded to the nearest 0.10 (tenth).

"Fine Aggregate" section, "Percent Retained" column, Item "R" is found by dividing the weight retained on each sieve in "Fine Aggregate" section, "Percent Retained" column, Item "P" by the before wash weight "Fine Aggregate" section, Item "F."

$$R = \frac{P}{F} \times 100$$

The "Total" for "Fine Aggregate" section, "% Retained" column, Item "R"

should equal 100 percent.

Fine Aggregate items:

- F = Reduced dry sample weight;
- P = Wt. retained per sieve;
- R = Percent retained per sieve based on the before wash sample weight item "F".
- 9. After determining the "Percent Retained" column, Item "R" for "Fine Aggregate", record the results in the "Combined Aggregate" section, "Percent Retained" column, Item "Z" on Form T-166 also.
- 10. On Form T-166, find the "Combined Aggregate" section, "% Passing" column, Item "0.1%". Begin subtracting from 100 at the Maximum Aggregate size; 100 minus the sum of Item "Z".

% passing =  $100.0 - \Sigma Z$ 

The percent passing the No. 200 should equal "Fine Aggregate" section, "Percent Retained" column, Item "R".

Round each result to the nearest whole number, except for the No. 200 sieve.

Record the result in the "Combined Aggregate" section, "% Passing" column, Item "1%".

For the No. 200 sieve, round the result to the nearest tenth (0.10) percent except when over 10 percent.

These are the results that should be used for acceptance.

Report: Daily results must be filled out on Form T-166, while weekly results are recorded on optional Form T-101.

As per *WYDOT Standard Specifications* 414.4.7, the fine aggregate may be adjusted up to two percent by weight, based on the total weight of aggregate without requiring a new mix design. Ensure the fine aggregate fraction does not exceed 44 percent of the total aggregate mass.

### Procedure: Fineness Modulus of Concrete Aggregate;

1. Determine the fineness modulus of the fine aggregate after the completion of all functions in section "Sieve Analysis for Fine Concrete Aggregate" (Calculating the percent retained and passing for each sieve).

To determine the fineness modulus, use the percent retained for each sieve from the  $\frac{3}{8}$  inch through the No. 100. On Form T-166, calculate the fineness modulus in the "Fine Aggregates" section, column "% Ret." Item "S" (see Example Form T-166 in this section).

Example:

| Retained on the: | 3/8 | inch | = | 0    | % |       |   |                              |
|------------------|-----|------|---|------|---|-------|---|------------------------------|
| Retained on the: | No. | 4    | = | 2.9  | % | 2.9   | = | 0+2.9                        |
| Retained on the: | No. | 8    | = | 21.0 | % | 23.9  | = | 0+2.9+21.0                   |
| Retained on the: | No. | 16   | = | 16.3 | % | 40.2  | = | 0+2.9+21.0+16.3              |
| Retained on the: | No. | 30   | = | 26.7 | % | 66.9  | = | 0+2.9+21.0+16.3+26.7         |
| Retained on the: | No. | 50   | = | 23.2 | % | 90.1  | = | 0+2.9+21.0+16.3+26.7+23.2    |
| Retained on the: | No. | 100  | = | 6.7  | % | 96.8  | = | 02.9+21.0+16.3+26.7+23.2+6.7 |
|                  |     |      |   |      |   | 320.8 |   |                              |

320.8 = Cumulative Total Fineness Modulus: 320.8 / 100 = 3.21

If the fineness modulus varies by more than  $\pm 0.20$  from the fineness modulus used for the mix design, it will be necessary to contact the WYDOT Materials Program for a review of the mix design being used.

Note: *WYDOT Supplementary Specification* SS-500G Section 513.4.10.2.6 part;

A new mix design is required when:

A change in the fine aggregate fineness modulus of more than 0.3 from the initial mix.

Report: Record the fineness modulus result for each fine aggregate test on Form T-166 in the fineness modulus section located below the data entry area (See Example Form T-166 in this section).

Report the fineness modulus for each test result under remarks on Form T-101 (Weekly Report).

Procedure: Sieve Analysis Coarse Concrete Aggregate

The sampling location and procedure is outlined in section WYDOT 804.0. Aggregate to be tested for gradation acceptance should be free of any additives.

Note: Before Procedure 1 below, check the equipment (scale, sieves, etc.). Check for condition, calibration, level and cleanliness. Nest the required sieves in the proper order.

See the procedure for "Moisture Determination for Fine and Coarse Concrete Aggregate" in this section.

1. Determine test sample size.

Generally it is not necessary to reduce the sample weight by splitting to less than 30 lb when using the large mechanical sieve shaker. Care should be taken not to overload an individual sieve when working with aggregates which could collect primarily on the No. 4 sieve. If it is necessary to reduce the sample size, follow procedure WYDOT 805.0, *Splitting by Mechanical Splitter*. A larger test sample should increase the accuracy of the results. In no case should the size of the test sample be less than:

| Nominal Maximum<br>Size Aggregate | Minimum Weight<br>of Test Sample |
|-----------------------------------|----------------------------------|
| <sup>3</sup> / <sub>8</sub> inch  | 2 lb                             |
| <sup>1</sup> / <sub>2</sub> inch  | 4 lb                             |
| <sup>3</sup> / <sub>4</sub> inch  | 11 lb                            |
| 1 inch                            | 22 lb                            |
| $1\frac{1}{2}$ inch               | 30 lb                            |

Should the sample require splitting to reduce the sample size, the weight (mass) after splitting is entered in the "Coarse Aggregate" section, "Sample" Item "E" on Form T-166.

- 2. Clamp down the sieve trays, start shaker and add sample. Follow the instructions outlined in the mechanical sieve shaker "Operating and Service Manual" for tightening sieve trays.
  - Note: Shake until no material can be observed falling from one sieve to another. Excessive time (more than approximately 10 minutes) to achieve adequate sieving may result in damage to the sample.
- 3. Continue sieving for a sufficient period and such manner that, after completion, not more than 0.5 percent by mass of the total sample passes any sieve during one minute of continuous hand sieving performed as follows.

Selecting the sieve with the most retained material, hold the individual

sieve, with a snug fitting pan and cover attached, in a slightly inclined position in one hand. Strike the side of the sieve sharply and with an upward motion against the heel of the other hand at the rate of about one-hundred-fifty times per minute, turn the sieve about one-sixth of a revolution at intervals of about twenty-five strokes. In determining sufficiency of sieving for sizes larger than the No. 4 sieve, limit the material on the sieve to a single layer of particles.

If the size of the mounted testing sieves makes the described sieving motion impractical, use 8 inch diameter sieves to verify the sufficiency of sieving.

 $\frac{\text{Weight Passing after hand sieving}}{\text{Individual Sieve Weight Retained}} \times 100 = \text{not more than } 0.5\%$ 

If the sieve with the most retained material meets the criteria, the other sieves do not need to be checked.

4. Weigh the material retained on each sieve tray and pan.

Following adequate sieving time, each sieve tray is removed from the sieve shaker and the material retained is weighed and recorded on Form T-166 in the "Coarse Aggregate" section, column "Wt. Ret." Item "K", next to the appropriate sieve size.

Weigh material to the nearest 0.1% of the original dry sample mass. Requirement for 30 lb to 50 lb sample weight is to the nearest hundredth (0.01).

The "Total" of the sieve and pan weights (Item "K") should be within 0.3 percent of the original total dry sample weight which was recorded as item "E" if the sample was split, or the % Moisture Dry Weight when not split.

 $\frac{\text{Weight of Material on Sieves +Pan}}{\text{Original Dry Weight}} = 100 = \text{within } 0.3\%$ 

If the amounts differ by more than 0.3 percent, based on the original dry sample mass, the results should not be used for acceptance or rejection purposes and another sample should be obtained.

When amounts differ by less than 0.3 percent, based on the original dry sample mass, the "Total" determined material and pan sample weight should be used for calculations. Enter the Sample weight (mass) in the "Coarse Aggregate" section, Item "E".

5. Determine the percent retained for each screen for the "Coarse Aggregate" section, column "% Retained", Item "L" on Form T-166.

"Coarse Aggregate" section, "Percent Retained" column, Item "L" is found by dividing the weight retained on each sieve tray in column "K" by the sample weight Item "E" and multiplying by 100.

$$L = \frac{K}{E} x (100)$$

The "Total" for the "Coarse Aggregate" section, column "Percent Retained", Item "L" should equal 100 percent.

- 6. After determining the percent retained for each sieve size, enter the results recorded in the "Combined Aggregate" section, column "% Retained", Item "Z" on Form T-166.
- 7. Find the percent passing for the coarse aggregate.

Find the "Combined Aggregate" section, "% Passing" column, Item "0.1%" on Form T-166. Begin subtracting from 100 at the Maximum Aggregate size; 100 minus the sum of Item "Z".

% passing = 
$$100.0 - \Sigma Z$$

8. On Form T-166, except for the No. 200 sieve, round each result to the nearest whole number. Record the result in the "Combined Aggregate" section, "% Passing" column, Item "1%".

For the No. 200 sieve, round the result to the nearest 0.1 percent (tenth). These are the results that should be used for acceptance.

<u>A washed sieve analysis must be performed on all material passing the #4</u> <u>screen</u>, following the procedure previously described for fine concrete aggregate when:

- 1. There is a significant amount of material coating the aggregate OR
- 2. There is more than 5% passing the No. 4 sieve.
- Report: Daily testing results are recorded on Form T-166, while weekly test results are recorded on optional Form T-101.

The results of surfacing material gradation tests for the week are recorded on optional Form T-102. When several different surfacing materials are being tested at the same time, each will need a completely different report for the week.

See Example of Forms T-101, T-102, T-166 for fine aggregate, and T-166 for coarse aggregate in this section.

# WYOMING DEPARTMENT OF TRANSPORTATION T-166 MATERIALS TESTING LABORATORY (Rev. 10-18)

AGGREGATE ANALYSIS

| ENGINEER: Resid               | lent Enginee                        | r                   |                | TOWN<br>SAMPLED BY            | vn                       |  |  |                                       |                                |
|-------------------------------|-------------------------------------|---------------------|----------------|-------------------------------|--------------------------|--|--|---------------------------------------|--------------------------------|
| PIT OR QUARRY: Pit or         | Quarry Na                           | me                  |                |                               | : Project Cou            | ntv  |  |                                       |                                |
| QUANTITY: Tota                | Plan Quant                          | ity                 |                |                               |                          |  | : Grading Spe  |                                       |                                |
| DATE RECEIVED: XX/X           |                                     | 1                   |                |                               | ,                        | DATE TESTEI  | : XX/XX/XX   |                                       |                                |
|                               | W E                                 | IGHT                | (lbs or k      | g)                            |                          |  |  | Weight                                | % Retained =                   |
|                               | COARSI                              | E AGG.              |                | FINE AG                       | G.                       |  |  | Retained                              |                                |
| Sample                        | RAICE RICE RICE RICE RICE RICE RICE | = (E)               | 56             | 2.8                           | = (F)                    |  |  | (lbs or kg)                           | ( <sup>D</sup> J ···           |
| After Wash                    |                                     |                     |                | 560.1                         |                          | RETAINED No.   | 4 [4.75 mm] = (A)  | 1                                     | -                              |
| Pass No. 200 [75µm]           |                                     |                     |                | 2.7                           |                          | PASS No.   | 4 [4.75 mm]= (B)   |                                       |                                |
| Pass No. 200 [75 µm], Pan     |                                     |                     |                | 1.8                           |                          | TOT  | $\mathbf{AL}$ , $\mathbf{A} + \mathbf{B} = (\mathbf{D})$ |                                       |                                |
| Total Pass No. 200 [75µm]     |                                     |                     |                | 4.5                           | FINE                     |  |  |                                       |                                |
|                               |                                     | % RET =             | WT             | % RET =                       | FINE.<br>MOD.            | <b>F</b> actoria a secondaria a secondaria de la second | COMBINI  | ED AGGREC                             | ATE                            |
| SIEVE<br>SIZE                 | WT RET                              | <u>K X 100</u><br>E | RET            | <u>P x 100</u><br>F           | CALC.                    |  | % PAS<br>100 - \$  |                                       | SPEC<br>% PASSING              |
|                               | =K                                  | =L,                 | = <b>P</b>     | =R                            | = <b>S</b>               | =Z   | to 0.1 %   | to 1 %                                | % PASSING                      |
| 1 1/2" [37.5 mm]              | 1                                   |                     | 1              | L                             |                          |  |  | · · · · · · · · · · · · · · · · · · · |                                |
| 1" [25mm]                     |                                     |                     |                | 1.00                          |                          |  |  |                                       |                                |
| 3/4" [19 mm]                  | 1                                   |                     |                |                               |                          |  |  |                                       |                                |
| 1/2" [12.5 mm]                | 1                                   | 1                   | 1              |                               |                          |  |  |                                       |                                |
| 3/8" [9.5 mm]                 | 1                                   |                     |                | T                             |                          |  | 100.0  | 100                                   | 100                            |
| No. 4 [4.75 mm]               | 2                                   |                     | 16.3           | 2.9                           | 2.9                      | 2.9  | 97.1   | 97                                    | 95 - 100                       |
| No. 8 [2.36 mm]               | 11                                  |                     | 118.2          | 21.0                          | 23.9                     | 21.0   | 76.1   | 76                                    |                                |
| No. 16 [1.18 mm]              |                                     |                     | 91.7           | 16.3                          | 40.2                     | 16.3   | 59.8   | 60                                    | 45 - 80                        |
| No. 30 [600 µm]               |                                     |                     | 150.3          | 26.7                          | 66.9                     | 26.7   | 33.1   | 33                                    |                                |
| No. 40 425 [µm]               |                                     |                     |                |                               |                          |  |  |                                       |                                |
| No. 50 [300 µm]               |                                     |                     | 130.6          | 23.2                          | 90.1                     | 23.2   | 9.9  | 10                                    | 10 - 30                        |
| No. 100 [150 μm]              |                                     |                     | 37.7           | 6.7                           | 96.8                     | 6.7  | 3.2  | 3                                     | 2 - 10                         |
| No. 200 [75 µm]               |                                     |                     | 13.5           | 2.4                           | 99.2                     | 2.4  | 0.8  | 0.8                                   | 0 - 4                          |
| Pass No. 200 [75 µm], Pan     | 1                                   |                     | 4.5            | 0.8                           | 100.0                    |  |  |                                       |                                |
| TOTAL PASSING                 | 22.23                               |                     | 562.8          | 100.0                         |                          |  |  |                                       |                                |
| SHAKER LOSS %                 |                                     |                     | 1              | - 11                          |                          |  | WET WT   | (lborkg)                              | 30.0                           |
| FRACTURED FACES % One or more |                                     | SHAKE               | R LOSS F       | ORMULA                        |                          | DRY WT   | (lb or kg)   | 29.9                                  |                                |
| FLAT & ELONGATED %            | 1:5 Ratio                           |                     | ([E or F] - TC | DTAL PASSING                  | 6) / [E or F] * 100      |  | WET - DI   | RY = MOISTURE                         | 0.10                           |
| ✓ FINENESS MODU               | LUS: see M.T                        | .M., Sect           | . 816.0:       |                               | 3,21                     | % MC   | DIST.=(MOIST./ DRY                                       | WT)x100                               | 0.33                           |
| BLOWS = Tin<br>No.            | Wet+Tare=<br>AA                     | Dry + Tare=<br>BB   | Tare =<br>CC   | Moisture =<br>AA - BB =<br>DD | Dry Wt =<br>BB - CC = EE | (DD/EE)x 100   | IOISTURE<br>x Corr. Factor =                             |                                       | PLASTIC INDEX<br>(PI) =LL - PL |
| LIQUID LIMIT (LL)             | -                                   |                     | 1 = = 1        |                               |                          | ALCON PACING   |  |                                       |                                |

REMARKS

TESTED BY

CERTIFICATION NO.

#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY T-166 (Rev. 10-18)

AGGREGATE ANALYSIS

| DEPARTMENT                |                 |                    |              |                               |                          | TEST NU  | MBER                     | : ###                       |                   |                                |
|---------------------------|-----------------|--------------------|--------------|-------------------------------|--------------------------|----------|--------------------------|-----------------------------|-------------------|--------------------------------|
| PROJECT NO(S).: ERP       |                 |                    |              |                               |                          |          |                          | : Project De:               |                   |                                |
| ENGINEER: Resid           | lent Enginee    | r                  |              |                               |                          |          |                          |                             | ngineer's Tov     | vn                             |
| SAMPLE I.D.:              |                 | 5                  |              |                               |                          |          |                          | : Tester                    |                   |                                |
| PIT OR QUARRY: Pit of     | r Quarry Na     | me                 |              |                               |                          | CO       | UNTY                     | : Project Cou               | inty              |                                |
| QUANTITY: Tota            |                 | ity                |              |                               |                          |          |                          | Grading Sp                  |                   |                                |
| DATE RECEIVED: XX/X       | (X/XX           |                    |              |                               |                          | DATE TI  | ESTED                    | : XX/XX/XX                  |                   |                                |
|                           | WE              | IGHT               | (lbs or l    | kg)                           |                          |          |                          |                             | Weight            | % Retained =                   |
|                           | COARSI          | E AGG.             |              | FINE AG                       | łG.                      |          |                          |                             | Retained          | A or B<br>D x 10               |
| Sample                    | 31.37           | = (E)              |              |                               | = (F)                    |          |                          |                             | (lbs or kg)       | ( D J **                       |
| After Wash                | 31.             | 36                 |              |                               |                          | RETAIN   | ED No. 4                 | [4.75 mm] = (A)             | 10.000            | 9                              |
| Pass No. 200 [75µm]       | 0.(             | 01                 |              |                               |                          | PA       | ASS No.                  | 4 [4.75 mm]= (B)            |                   |                                |
| Pass No. 200 [75 µm], Pan | 0.0             | 01                 |              |                               |                          |          | TOT                      | AL, $A + B = (D)$           |                   |                                |
| Total Pass No. 200 [75µm] | 0.0             | 02                 |              |                               |                          |          |                          |                             |                   |                                |
|                           |                 | % RET =            | WT           | % RET =                       | % RET                    |          |                          | COMBIN                      | ED AGGREC         | GATE                           |
| SIEVE<br>SIZE             | WT RET          | <u>КХ 100</u><br>Е | WT<br>RET    | <u>P x 100</u><br>F           | <u>R x I</u><br>100      |          | $1 L_{75}$ $100 - S(7.)$ |                             | SPEC<br>% PASSING |                                |
|                           | =K              | =L.                | =P           | =R                            | = <b>S</b>               |          | =Z                       | to 0.1 %                    | to 1 %            | % PASSING                      |
| 1 1/2" [37.5 mm]          |                 |                    |              | 1                             |                          |          |                          | 100.0                       | 100               | 100                            |
| 1" [25mm]                 |                 |                    |              | 1                             |                          |          |                          | 100.0                       | 100               | 95 - 100                       |
| 3/4" [19 mm]              | 5.32            | 17.0               |              |                               |                          |          | 17.0                     | 83.0                        | 83                |                                |
| 1/2" [12.5 mm]            | 16.60           | 52.9               |              | 1                             |                          | E        | 52.9                     | 30.1                        | 30                | 25 - 60                        |
| 3/8" [9.5 mm]             | 6.27            | 20,0               |              |                               |                          | 2        | 20.0                     | 10,1                        | 10                |                                |
| No. 4 [4.75 mm]           | 3.11            | 9.9                |              | 1000                          |                          |          | 9.9                      | 0.2                         |                   | 0 - 10                         |
| No. 8 [2.36 mm]           | 0.07            | 0.2                |              | 1                             |                          |          | 0.2                      | 0.0                         | 0                 | 0 - 5                          |
| No. 16 [1.18 mm]          |                 |                    |              | 1.1                           |                          |          |                          |                             |                   |                                |
| No. 30 [600 µm]           |                 |                    | - <u>-</u>   | 1                             |                          |          | _                        |                             |                   |                                |
| No. 40 425 [µm]           |                 |                    |              |                               |                          |          |                          |                             |                   |                                |
| No. 50 [300 µm]           |                 |                    | 100          | 1                             |                          |          |                          | 1                           |                   |                                |
| No. 100 [150 μm]          |                 | · ;                |              |                               |                          |          |                          |                             |                   |                                |
| No. 200 [75 µm]           |                 |                    |              |                               |                          |          |                          |                             |                   |                                |
| Pass No. 200 [75 µm], Pan |                 |                    |              | 1                             |                          |          |                          |                             |                   |                                |
| TOTAL PASSING             | 31.4            | 100.0              |              |                               |                          |          |                          | r                           |                   |                                |
| SHAKER LOSS %             | One or more     |                    |              |                               |                          |          |                          | -                           | (lb or kg)        | 31.8                           |
| FRACTURED FACES %         | 1:5 Ratio       | _                  |              | ER LOSS F                     |                          |          |                          | 1                           | (Ib or kg)        | 31.4                           |
| FLAT & ELONGATED %        | 1               |                    |              | OTAL PASSING                  | G) / [E or F] * 100      |          |                          |                             | RY = MOISTURE     | 0.40                           |
| ✓ FINENESS MODU           | -               | I.M., Sect         |              | I news                        |                          | L        |                          | IST.=(MOIST./ DRY           | WT)x100           | 1.27                           |
| BLOWS = Tin<br>No.        | Wet+Tare=<br>AA | Dry + Tare=<br>BB  | Tare =<br>CC | Moisture =<br>AA - BB =<br>DD | Dry Wt =<br>BB - CC = EE | (DD/EE)x |                          | OISTURE<br>x Corr. Factor = |                   | PLASTIC INDEX<br>(PI) =LL - PL |
| LIQUID LIMIT (LL)         |                 |                    |              |                               |                          |          |                          |                             |                   |                                |
| PLASTIC LIMIT (PL)        |                 |                    |              | L                             |                          |          |                          |                             |                   |                                |

REMARKS

TESTED BY

CERTIFICATION NO.



# WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY REPORT OF FIELD TESTS ON CONCRETE AGGREGATE

Form T-101 (Rev. 09-16)

|                       |                    | Report No(s).: | _###                |  |
|-----------------------|--------------------|----------------|---------------------|--|
| Project No(s).:       | #####              | Location:      | On Plans            |  |
| Submitted By:         | Resident Engineer  | At:            | Town                |  |
| Identification Marks: | QC ###             | Quantity Rep.: | total plan quantity |  |
| Source:               | Pit or Quarry name | For Use As:    | Grading spec.       |  |
| Date Received:        | 09/18/16           | Date Tested:   | 09/18/16            |  |

#### TEST RESULTS COARSE or MEDIUM AGGREGATE

|              |               |           |           | ~         | ~ .       |           | CS #1     |
|--------------|---------------|-----------|-----------|-----------|-----------|-----------|-----------|
| Test Num     | ıber          | 1         | 2         | 3         | 4         | 5         | 6         |
| Date Tes     | sted          | Current   | Current   | Current   | Current   | Current   | Current   |
| yd³ (m³) Rep | resented      | 80        | 90        | 70        | 80        | 90        | 90        |
| Sieve Size   | Specification | % Passing |
| 2 1/2"       |               |           |           |           |           |           |           |
| 2"           |               |           |           |           |           |           |           |
| 1 1/2"       | 100           | 100       | 100       | 100       | 100       | 100       | 100       |
| 1"           | 95-100        | 100       | 100       | 99        | 100       | 100       | 100       |
| 3/4"         |               | 80        | 90        | 79        | 84        | 71        | 83        |
| 1/2"         | 45-80         | 41        | 58        | 39        | 51        | 27        | 30        |
| 3/8"         |               | 18        | 32        | 15        | 29        | 11        | 10        |
| No. 4        | 10-30         | 1         | 3         | 1         | 6         | 1         | 1         |
| No. 8        | 2-10          | 0.4       | 0.4       | 1         | 2         | 0.4       | 1         |
| No. 200      | 0-4           | 0.3       | 0.1       | 0.5       | 0.9       | 0.3       | 0.1       |

#### FINE AGGREGATE

| Test Num         | ber           | 1         | 2         | 3         | 4         | 5         | 6         |
|------------------|---------------|-----------|-----------|-----------|-----------|-----------|-----------|
| Date Tes         | ted           | Current   | Current   | Current   | Current   | Current   | Current   |
| yd³ (m³) Repr    | resented      | 80        | 90        | 70        | 80        | 90        | 90        |
| Sieve Size       | Specification | % Passing |
| 3/8"             | 100           | 100       | 100       | 100       | 100       | 100       | 100       |
| No. 4            | 95-100        | 96        | 97        | 97        | 96        | 96        | 97        |
| No. 8            |               | 75        | 74        | 74        | 74        | 70        | 76        |
| No. 16           | 45-80         | 53        | 60        | 59        | 58        | 52        | 60        |
| No. 30           |               | 34        | 32        | 35        | 32        | 32        | 33        |
| No. 50           | 10-30         | 17        | 15        | 16        | 16        | 17        | 10        |
| No. 100          | 2-10          | 5         | 4         | 4         | 6         | 5         | 3         |
| No. 200          | 0-4           | 2.7       | 1.6       | 1.8       | 2.7       | 2.0       | 0.8       |
| Fineness Modulus | 3.20          | 3.20      | 3.18      | 3.15      | 3.17      | 3.28      | 3.21      |

**Does Material Meet Specifications?** 

If Not What Corrective Measures Taken

Remarks: W-FA #6 IS SPLIT WITH CS-FA #

Resident Engineer's Name Engineer Tested By: Technician's Name Certification Number: XXX WYDOT 816.0 (Rev. 10-18)



#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY REPORT OF FIELD TESTS ON SURFACING MATERIALS

Form T-102 (Rev. 09-16)

|                                |                         |                  | Repo                                   | rt / Lot No(s).: | Report Number            |  |
|--------------------------------|-------------------------|------------------|--|------------------|--------------------------|--|
| Project No(s).: Project Number |                         | nber             | Location:                              |                  |                          |  |
| Submitted By: R                | Resident Er             | igineer's Name   | 75                                     | At:              | Resident Engineer's Town |  |
| ID Marks: 1                    | Fotal Plan G            | Quantity         | Quantity                               | Represented:     | Grading Specification    |  |
| Source: P                      | it or Quar              | ry Name          | For Use As: Project or Pit or Quarry l |                  |                          |  |
| Date Received:                 | Date Received: XX/XX/XX |                  |  | Date Tested:     | XX/XX/XX                 |  |
| Sampled (Che                   | ck One):                | C Mechanical ID# | 💽 Belt                                 | C Windrow        | C Stockpile              |  |

TEST RESULTS

| Test Number          |                | Test #        | Text #        |
|----------------------|----------------|---------------|---------------|---------------|---------------|---------------|---------------|
| Date Tested          |                | XX/XX/XX      | XX/XX/XX      | XX/XX/XX      | XX/XX/XX      | XX/XX/XX      | XX/XX/XX      |
| Station Sampled      |                |               |               |               |               |               |               |
| Tons Represented - T | Specifications | Test Quantity |
| Asphalt Content      | %              | %             | %             | %             | %             | %             | 9             |
| % Past 4"            |                |               |               |               |               |               |               |
| % Past 3"            |                | 25-<br>27-    |               |               |               |               |               |
| % Past 2"            |                |               |               |               |               |               |               |
| % Past 11⁄2"         | 100            | 100           | 100           | 100           | 100           | 100           | 100           |
| % Past 1"            | 95 - 100       | 100           | 100           | 100           | 100           | 100           | 100           |
| % Past ¾"            |                | 92            | 89            | 91            | 91            | 86            | 91            |
| % Past 1⁄2"          |                | 78            | 75            | 78            | 78            | 70            | 76            |
| % Past ¾"            |                | 66            | 63            | 66            | 67            | 62            | 65            |
| % Past No. 4         | 40 - 65        | 63            | 55            | 59            | 60            | 53            | 57            |
| % Past No. 8         | 30 - 55        | 47            | 40            | 43            | 45            | 39            | 41            |
| % Past No. 16        |                | 25            |               |               |               |               |               |
| % Past No. 30        |                | 28            | 26            | 28            | 29            | 25            | 29            |
| % Past No. 50        |                |               |               |               |               |               |               |
| % Past No. 100       |                |               |               |               |               |               |               |
| % Past No. 200       | 3 - 15         | 11.6          | 10.7          | 12.1          | 11.5          | 9.7           | 11.1          |
| Liquid Limit (LL)    |                | 22.1          |               | 23.7          |               | 22.9          |               |
| Plastic Index (PI)   |                | NP            |               | 3.0           |               | NP            |               |

\* Note: One Quality test not to represent more than 1000 T

| Quantity Placed:  | To Last Report Current Ton | <u>s</u> | Since Last | Report Form Tons | Total To Date Total Tons | _ |
|-------------------|----------------------------|----------|------------|------------------|--------------------------|---|
| Does Material Mee |                            | C YES    | C NO       | ]                |                          |   |
| Corrective Meas   | sures Taken                |          |            |                  |                          |   |
| Remarks           | Q-CB #3 SPLIT WITH CS-CB # | ≠1       |            |                  |                          |   |

Tested By Tester's Name Certification No. XXX

# DETERMINING THE PERCENTAGE OF FRACTURED FACES IN COARSE AGGREGATE

- Scope: This test method describes the procedure to determine the percentage of aggregate having one or more fractured faces. Procedure adopted from AASHTO T 335.
- Use: The purpose of ensuring fractured face requirements is to provide aggregate that has adequate shear strength from inter-particle friction to improve stability and texture.

A fractured face is an angular, rough, or broken surface of an aggregate particle created by crushing or other means.

A face will be considered a "fractured face" whenever one-quarter or more of the maximum cross-section area, when viewed normal to that face, is fractured with sharp and well-defined edges (this excludes small nicks).

- Apparatus: 1. Drying Stove
  - 2. Splitting device or quartering canvas
  - 3. 8 inch U.S. standard sieves
  - 4. 8 inch sieve shaker with a minimum <sup>1</sup>/<sub>4</sub> hp motor, combined back and forth lateral motion and up-and-down tilting motion, and 15 minute electric reset timer switch with a hold feature for continuous operation
  - 5. Balance(s)

| Scale Sensitivity | Sample Weight  |
|-------------------|----------------|
| 0.1 g             | 4 lb or less   |
| 1.0 g             | 4 lb to 11 lb  |
| 5.0 g             | 11 lb to 44 lb |
| 20.0 g            | 44 lb plus     |

#### Reference

| Documents: | AASHTO T 335     | Standard Method of Test for Determining the          |
|------------|------------------|--|
|            |                  | Percentage of Fracture in Coarse Aggregate, Method 1 |
|            | WYDOT 803        | WYDOT Standard Specifications                        |
|            | WYDOT 803.2.2(1) | WYDOT Standard Specifications: Concrete              |
|            | WYDOT 803.4.3    | WYDOT Standard Specifications: Crushed Base          |
|            | WYDOT 803.5.5-2  | WYDOT Standard Specifications: Hot Plant Mix         |
|            | WYDOT 803.6.1    | WYDOT Standard Specifications                        |
|            | WYDOT 804.0      | Aggregate Sampling                                   |
|            | WYDOT 805.0      | Sample Splitting by Mechanical Splitter              |
|            | WYDOT E-46       | Job Mix Formula                                      |
|            | WYDOT T-159      | Flat & Elongated and Fractured Faces                 |
|            |                  |  |

Sampling: The sampling location and procedure is outlined in section WYDOT 804.0 *Aggregate Sampling*. Aggregate to be tested for gradation acceptance should be free of any additives.

Test Sample: Dry the sample sufficiently to obtain clean separation of fine and coarse material. Control the temperature so the heat used will allow steam to escape without generating enough pressure to fracture any of the particles of the sample.

Allow the test sample to cool.

Procedure: 1. Determine the mass (weight) of the test sample size. Follow procedure WYDOT 805.0 *Sample Splitting by Mechanical Splitter*.

| Nominal Maximum<br>Size Aggregate | Minimum Sample Mass (Weight)<br>Retained 4.75-mm (No. 4) Sieve |
|-----------------------------------|--|
| 1 inch                            | 3.5 lb   |
| <sup>3</sup> / <sub>4</sub> inch  | 2.2 lb   |
| <sup>1</sup> / <sub>2</sub> inch  | 1.5 lb   |
| <sup>3</sup> / <sub>8</sub> inch  | 0.9 lb   |
| No. 4                             | 0.5 lb   |

- 2. Using an 8 inch sieve, screen the material over the No. 4 sieve and discard the minus No. 4 fraction. Following are the requirements for specific uses;
  - Note: For Plant Mix Wearing Course, the portion passing the <sup>3</sup>/<sub>8</sub> inch sieve may be further reduced to a minimum of 0.5 lb as required in *WYDOT Standard Specifications* 803.6.1. This will reduce the number of particles to be separated during the procedure. In this case, percent fractured particles is determined on each portion and a weighted average percentage of fractured particles is calculated based on the mass of each of the portions to reflect the total percentage of fractured particles in the entire sample.
- 3. Determine whether each particle has no fractured faces, one fractured face, two or more fractured faces, and place each into separate piles. A fractured face is whenever one-quarter or more of the maximum cross-section area, when viewed normal to that face, is fractured with sharp and well-defined edges (excluding small nicks).
- 4. Determine the mass of particles in each pile by weighing to the nearest 0.1 percent.

5. Calculate the mass percentage of each particle category (one fractured face and two or more fractured faces) to the nearest 1 percent in accordance with the following;

Calculating for one or more fractured faces;

$$\% 1 \text{ FF} = \frac{1 \text{ FF} + 2 \text{ FF}}{\text{mass}} \times 100$$

Where:

% 1 FF is the percent of particles with one or more fractured faces
1 FF is the mass (weight) of particles with one fractured face
2 FF is the mass (weight) of particles with two or more fractured faces
mass is the total test sample mass (weight)

Calculating for two or more fractured faces;

$$\% 2 \text{ FF} = \frac{2 \text{ FFmass}}{\text{mass}} \times 100$$

Where: <u>% 2 FF</u> is the percent of particles with two or more fractured faces

Using the equations in the worksheet T-159, correct the value so it is representative of the sample.

Report the results on Form E-46.

| State Project Number         C: Fit the Guarry Nume         C: C  | MATERIALS TESTING LABORATORY<br>FLAT & ELONGATED AND FRACTURED FACES<br>TEST NUMBER: ## |                         |                             |             |
|---|---|-------------------------|-----------------------------|-------------|
| N: Fit or Cuarry Name         C: Fit or Cuarry Name         S: Fer Plans       C: Fit of %       Sieve Size       Sample Elong Elongated Sample (1:5 Ratio)         A       A       B       C: D       E       F       F         A       A       B       Sieve Size       Sample Elong Elongated Sample (1:5 Ratio)       Centreded         1       B00       38.200       34.12"       501 330       D       E       F       F         A       A       B       C: D       D       E       F       F       C         1       20.900       77.400       34" & +10"       M: of Elongated Sample (1:5 Ratio)       M: of Elong % CG)=         A       A       B       C       D       C       D       C       C       D         20.900       1.1800       36'11       M: of Elongated Sample (1:5 Ratio)       M: of Elongated Sample (1:5 Ratio) <t< th=""><th>LOCATION: per plans</th><th></th><th></th><th></th></t<>  | LOCATION: per plans   |                         |                             |             |
| Fit or Quarry Name       Fit or Quarry Name       Ren Plans       Certained       Ren Plans       Certained       Passing       Wr. of       Fiet Plans       Certained       Ret Plans       Certained       Retained       Retained     Passing     Wr. of     Flat &     % Retained       %     %     %     % Retained     %       %     %     %     %     %     Retained       %     %     %     %     %     %       %     %     %     %     %     %       %     %     %     %     %     %       %     %     %     %     %     %       1     %     %     %     %     %       16     500     60.300     3%     %     %       0     %     %     %     %     %       16     500     60.300     %     %     %       0     %     %     %     %     %       0     %     %     %     % </th <th>AT: Engineer's town</th> <th></th> <th></th> <th></th>   | AT: Engineer's town   |                         |                             |             |
| If for Quarry Name       DATE         C: Rith CD/YR       DATE         C: Rith CD/YR       DATE         S: Fer Plus:       C: Rith Corrected       MM. cf       FIER RETAINS         S: Fer Plus:       C: Rith Rith Rith Rith Rith Rith Rith Rith  | SAMPLED BY: Tester or Inspector   |                         |                             |             |
| Di MM/DD/NR       CERTING       S: Per Plurs       S: Per Plurs       CERTING       A W- B       A     W     Dir Rat & Sieve Size     Sample (1:5 Ratio)       A     W- B     C     D     E     F       A     W- B     C     D     E     F       1     20     98,200     112" & 34" & 41/2"     5601 300     Elong ated     Weight     W       1     18.00     98,200     17.400     34" & 41/2"     5601 300     E     F     E       1     20.900     17.400     34" & 41/2"     5601 300     E     COrrected     W     35.911       16.500     60.900     100     34" & 41/2"     5501 70     28.359     35.911       1     20.900     17.400     34" & 41/2"     5501 70     28.351       1     20.900     17.400     36" 41     35.911       1     20.900     17.400     38" 8 + 1/2"     35.911       1     20.900     17.400     38" 8 + 1/2"     35.911       1     20.900     10     17.400     35.911       1     20.900     10     17.40     0.010       1 <td>COUNTY: Project county</td> <td></td> <td></td> <td></td>  | COUNTY: Project county  |                         |                             |             |
| : Fer Plurs       CERTING         S. Fer Plurs       CERTING         S. Fer plurs       CERTING         A $\%$ B $Wt.$ of $S.9911$ $2.50.070$ $2.35.911$ $2.50.070$ $2.35.911$ $2.76.911$ $2.76.911$ $2.76.911$ $2.76.911$ $2.76.911$ $2.76.911$ $2.96.911$ <t< td=""><td>DATE TESTED: MM/DD/YR</td><td></td><td></td><td></td></t<>   | DATE TESTED: MM/DD/YR   |                         |                             |             |
| S: Fer plans         Original Gradation       Tat & Elongated Sample (1:5 Ratio)         Original Cradation       A       B       Wrt. of       Flat & %       %       Retained         %       %       %       Sieve Size       Sample       Elong       Elongated       Wreigh         %       %       %       Sieve Size       Sample       Elong       Elongated       Wreigh         1       300       77.400       -34" & +1/2"       501 390       = (Dx100)/C       = A/K         1       300       77.400       -34" & +1/2"       501 390       = (Dx100)/C       = A/K         1       20.900       *       40.000       -34" & +1/2"       501 390       = (Dx100)/C       = A/K         1       20.900       *       40.000       -34" & +1/2"       501 390       = (Dx100)/C       = A/K         1       20.900       **       40.000       -38" & *       >       -       28         1       20.900       **       40.000       -38" & *       >       -       -       -       -       28         1       20.900       **       40.000       -38" & *       -       -       -   | TESTED BY: Tester Nome  |                         |                             |             |
| Original Gradation         Flat & Elongated Sample (1:5 Ratio)           Retrained $\%$ <  | CERTIFICATION NO.: ####   |                         |                             |             |
| Retained<br>%         Mt. of<br>%         Flat &<br>%         % Flat &<br>%         % Retained<br>%           %         %         %         %         %         %         %           A         %         B         C         D         Elong Elong Elong Elong Hed<br>Weight         %         %           1         300         38.200 $34'' \& +1/2''         501 330         = (Dx100)/C         =AxK           1         300         38.200         10'' \& +38'''         250 070         = (Dx100)/C         =AxK           16:500         60.900         12'' \& +10.330'' \& +10.4         60 160         Md.Total % (2.G)=           16:500         8         40.000         38'' \& +10.4         60 160         Md.Total % (2.G)=           16:500         60.900         1/2'' \& 250 070         26100         35.911           20:500         m' = 40.000 36'' \& m' = 410 36'' \& m' = 410           20:500         m' = 40.000 36'' \& m' = 410 35.91           10:00         11/2'' \& 20.00 10'' \& 0.000 36'' \& m' = 410           20:500         m' = 410'' \& 0.000 36'' \& m' = 410'' \& 0.000 36'' \& m' = 410'' \& 0.000           10:00         0.00 M = 410'' $ | One or More Fractured Faces   |                         | Two or More Fractured Faces | Faces       |
| A $^{\text{M}}$ B         C         D         E         F           1.800         98.200         34" & +1/2"         501 330         = (Dx100)/C         = Ax/K           20.900         77.400         34" & +1/2"         501 330         = (0x100)/C         = Ax/K           16.500         60.900         -1/2" & +3/8"         250 070         35.911         35.911           1         20.900         ** 40.000         -36" & + No.4         60.160         28.35.91           1         20.900         ** 40.000         -36" & + No.4         60.160         35.911           AA-BB         1.7182         Carry out decima to four places on the factor         35.911           AA-BB         1.7182         Carry out decima to four places on the factor           Retained         Passing         Wf. of         Wf. of           Retained         %         Sieve Size         Sample           %         %         Sieve Size         Sample         Elongated           %         %         Sieve Size         Sample         Elongated         Weight           %          3         1         0         W         M           %         %         Sieve               | or N.   | Wf.                     | % Two or<br>More We         | Weighted %  |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$   | л н   | -                       |                             | a           |
| 20 800         77.400         34'' & +1/2''         501 330         35.911           16 500         60.900         -1/2'' & +3/8''         250 070         28.351           12 20 900 <sup>80</sup> 40.000         36'' & + No.4         60.160         35.911           AA-BB         1.1782         Carry out decimal to four places on the factor.         35.911           Original Gradation         1.1782         Carry out decimal to four places on the factor.           AA-BB         0.1378         K. Flat & K. Flat & K. Retained           %         %         %         %           %         %         %         %           %         %         %         %           %         %         %         %   | F)/100 =(Hx100)/C =(JxF)/100  |                         | =(Mx100)/C =(Nx             | =(NxF)/100  |
| 16 500         60 900         1/2" & +3/8"         250 070         28.351         28.351           1         20 900         ** 40 000         -3/8" & + No.4         60.160         35.911           Mrd.T otal % (2 G)=           (100         1.7182         Carry out decimal to four places on the factor.           Original Gradation         5.817           Retained         Passing         Wt. of         % Retained           %         % Sieve Size         Sample         Elong Elong         Corrected           %         %         Sieve Size         Sample         Elong Elong         Corrected           %         %         Sieve Size         Sample         Elong Elong Elong Signed         Weight           %         %         Sieve Size         Sample         Elong Elong Elong Signed         Veight  | 366.000 72.997  | 26.214 291.89           | 58.216                      | 20.906      |
| 20.900 <sup>100</sup> 38" & 8 + No.4     60.160     35.911       Wtd.Total % (% G)=       (100     1.7182     Carry out decimal to four places on the factor.       (AA-BB)     1.7182     Carry out decimal to four places on the factor.       (100     1.7182     Carry out decimal to four places on the factor.       (100     1.7182     Carry out decimal to four places on the factor.       (100     Flat & Elongated Sample (1:5 Ratio).       (100     R       (100     R       (100     R       (100     R       (100     R       (100     Sieve Size       (100     R       (100     R       (100     R       (100     R   | 174.050 69.601  | 19.732 159.47           | 63.770                      | 18.079      |
| =     100     1.7182     Carry out decimal to four places on the factor.       AA-BB     1.7182     Carry out decimal to four places on the factor.       Original Gradation     Flat & Elongated Sample (1:5 Ratio)       Retained     %     Sleve Size       %     Sleve Size     Wt. of       %     %     Sleve Size       %     Sleve Size     Sample Elong Elong ed       %     %     Sleve Size       0     R     0       %     Sleve Size     Sample Elong Elong ed       %     Sleve Size     Sample Elong Elong sted       %     Sleve Size     Sample Elong Elong sted  | 46.360 77.061   | 27.673 40.99            | 68.135                      | 24 468      |
| Original Gradation     Flat & Elongated Sample (1:5 Ratio)       Retained     Passing       %     %       %     Sieve Size   | Wtd. Total % (2 L)=   | 73.619 Wtd. T           | Witd. Total % (2 P)=        | 63,453      |
| Original Gradation         Flat & Elongated Sample (1:5 Ratio)           Retained         Wt. of         Wt. of         Corrected           %         %         Sieve Size         Sample         Elong Elong         Weight           %         %         Sieve Size         Sample         Elong Elongated         Weight           %         %         Sieve Size         Sample         Elongated         Weight           %         %         Sample         Sample         Sample         Elongated         Weight  |   |                         |                             |             |
| Retained         Passing         Wt. of<br>Wt. of         Flat &<br>Flat &<br>Flat &<br>Sieve Size         Corrected           %         %         Sieve Size         Sample         Flong         Elong         Weight           Q         R         Sieve Size         Sample         Flong         Elong         Weight           Mi         0         R         S         T         U         Wi           Mi         -344* & +1/2*         -344* & +1/2*         -344* & +1/2*         -344* & -1/2*         -344* & -1/2*   | One or More Fractured Faces   |                         | Two or More Fractured Faces | Faces       |
| Q         R         S         T         U         W           ∞         ∞         = (Tx100)/S         =QxV           ni         -344*&+1/2*         =         -344*   | Wt. One % One or % Weighted %   | M. Two<br>ted % or More | % Two or<br>More VVei       | Weighted %  |
| ®         = (Tx100)S         = CxV           -34" & + 1/2"         -34" & 54" & 54"         -34" & 54" & 54"  | Y Z EE FI   | F GG                    | HH                          | ٦J          |
| -3/4"   | WJ/100 =(Zx100)/S =(EExW)/100   |                         | =(GGx100)/S =(HF            | =(HHxW//100 |
|   |   |                         |                             | 1           |
| 3/6" [19.5 mm] -1/2" & +3/8"  |   |                         |                             | 1           |
| No. 4 [4.75 mm] 2c -3/8" & + No. 4  |   | 2.44                    |                             |             |
| VMd. Total % $(\Sigma Y)$ =   | Wtd. Total % (2 FF)=  | VMd. To                 | Vutd. Total % (2 JJ)=       |             |

i

4

WYDOT 817.0 (Rev. 10-17)

### LA ABRASION RESISTANCE (LAR)

- Scope: This test method, commonly referred to as the Los Angeles Rattler (LAR), is a measure of the degradation of aggregates resulting from a combination of actions including impact and grinding.
- Use: LAR is an aggregate source criteria for approval of Contractor Furnished Sources in the appropriate *WYDOT Standard Specifications* book. A standard gradation of material is placed inside a rotating steel drum along with a specified number of steel spheres. The steel drum contains a steel shelf inside the drum to pick the material up and carry it to a point within the drum where the material and steel spheres drop to the opposite side of the drum, creating an impact crushing effect. This cycle is repeated for 500 revolutions. When the drum stops and the contents are removed, the aggregate portion is sieved to determine the percent degradation. A specification for LAR is typical for most surfacing aggregates.

| Apparatus: | 1. | Los Angeles machine, according to AASHTO T 96 |
|------------|----|---|
|            |    |   |

- 2. Sieves; No. 4 and No. 12
- 3. Balance (sensitive to 0.1 g)
- 4. Charge (steel spheres)

#### Reference

| Documents: | AASHTO T 96               | Standard Test Method for Resistance to Degradation of<br>Small-Size Coarse Aggregate by Abrasion and Impact in<br>the Los Angeles Machine |
|------------|---------------------------|---|
|            | WYDOT 414.0               | Marshall and Superpave Mix Design and Mix Volumetric Verification Procedure   |
|            | WYDOT 804.0<br>WYDOT E-46 | Aggregate Sampling<br>Job Mix Formula   |

- Sampling: Obtain and reduce field samples according to WYDOT 804.0.
- Procedure: Perform according to AASHTO T 96. Perform test procedure using charge requirements on aggregate with at least one fractured face for grading "B".
- Report: Report the results on Form E-46. See example in WYDOT 414.0.

WYDOT 818.0 (Rev. 01-15)

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# FINE AGGREGATE ANGULARITY

- Scope: This test method covers the procedure to determine the fine aggregate angularity of an aggregate, also referred to as the uncompacted void content of a standard graded fine aggregate sample.
- Use: This test method determines the void content under standardized conditions which depends on the fine aggregate particle shape and texture. A higher void content indicates greater angularity, less sphericity, a rougher surface texture, or a combination of these. A lower void content indicates more spherical particles, smoother particles, or a combination of these. Fine Aggregate Angularity is typically a tool for aggregate classification of fines for use with mix designs for Hot Plant Mix. A specification for Fine Aggregate Angularity is typical for aggregate properties for Hot Plant Mix.

#### Apparatus: As defined in AASHTO T 304

- 1. Cylindrical measure (approximately 100 ml)
- 2. Jar and funnel with bottom opening of  $12.7 \pm 0.6$  mm diameter
- 3. Funnel stand capable of holding funnel  $115 \pm 2$  mm above the top of cylinder
- 4. Glass plate approximately 2 inch x 2 inch minimum x  $\frac{1}{8}$  inch thick
- 5. Pan of sufficient size to contain the funnel stand and prevent loss of material
- 6. Metal spatula with blade approximately 4 inch long x 1 inch wide, with straight edge
- 7. Balance accurate and readable to  $\pm 0.1$  g, capable of weighing the cylindrical measure and its contents

As defined in WYDOT 814.0

- 1. Wash pan with sufficient capacity to allow enough water to completely cover wash sample
- 2. Drying stove
- 3. Balance(s)

| Scale Sensitivity | Sample Weight |
|-------------------|---------------|
| 0.1 g             | 4 lb or less  |
| 1.0 g             | 4 lb to 11 lb |

- 4. 8 inch or 12 inch diameter No. 100 wash sieve
- 5. 8 inch or 12 inch diameter U.S. standard sieves
- 6. 8 inch or 12 inch sieve shaker

WYDOT 824.0 (Rev. 01-15)

Reference

| Documents: | AASHTO T 84  | Standard Method of Test for Specific Gravity and Absorption of Fine Aggregate |
|------------|--------------|---|
|            | AASHTO T 304 | Standard Method of Test for Uncompacted Void Content of                       |
|            |              | Fine Aggregate, Method A  |
|            | WYDOT 414.0  | Marshall and Superpave Mix Design and Mix Volumetric                          |
|            |              | Verification Procedure  |
|            | WYDOT 804.0  | Aggregate Sampling  |
|            | WYDOT 805.0  | Sample Splitting by Mechanical Splitter                                       |
|            | WYDOT 814.0  | Sieve Analysis of Combined Aggregate  |
|            | WYDOT E-46   | Job Mix Formula   |
|            |              |   |

- Sampling: The sampling location and procedure is outlined in WYDOT 804.0. Aggregate to be tested for acceptance evaluation must be free of any additives.
- Procedure: Calibrate the cylindrical measure to determine volume per AASHTO T 304.

Determine the Specific Gravity of the minus No. 4 material per AASHTO T 84.

Determine the mass (weight) of the test sample size.

- 1. Follow procedure WYDOT 805.0.
- 2. Follow WYDOT 814.0, use minus No. 4 to obtain about 3 lb.
- 3. Wash the minus No. 4 material.
  - Note: A wetting agent may or may not be necessary to add to the test sample. A wetting agent is any dispersing agent, such as Calgon, Joy, or other detergent that will promote separation of the fine materials.

When a wetting agent is used, a sufficient amount should be added to assure a thorough separation of the material finer than the No. 100 sieve from the coarser particles. There should be enough wetting agent to produce a small amount of suds when the sample is agitated. The quantity will depend on the hardness of the water, the quality of the detergent, and the agitation process. Excessive foaming may cause material to overflow the sieves. Add enough water to the sample container to cover the test sample. Agitate with sufficient vigor to separate and suspend the minus No. 100 material. Pour off the dirty water into nested No. 8 and No. 100 sieve (8 inch or 12 inch diameter). The No. 100 sieve should be placed in the sink with one side propped up about <sup>1</sup>/<sub>2</sub> inch so that water will flow freely. Add more water, agitate, and pour off the dirty water. Repeat this operation until the wash water is clear. Fines retained on the No. 100 sieve after washing will need to be cleaned of any trapped minus No. 100 material.

You may use your hand or spoon to agitate the material in the wash pan, but do not use your hand or any tool on the material within the No. 100 sieve or on the screen itself. Do not hit the screen. Wash the retained material into a pile on one side of the screen.

- Note: A spray nozzle or a piece of rubber tubing attached to a water faucet may be used to rinse any of the material that may have fallen onto the sieves. The velocity of water, which may be increased by pinching the tubing or by use of a nozzle, should not be sufficient to cause any splashing of the sample over the sides of the sieve. With the sieve held over the sink use the heel of your free hand to tap the outside edge to help dry and loosen the retained material. When the material starts moving around, empty the material into the washpan by tapping on the outside edge of the sieve. Any material still retained should be washed into the washpan using as little water as possible.
- 4. Dry the washed sample.

If direct heat is used, popping or sputtering can be controlled by covering the sample container. After enough steam has escaped the sample can be uncovered. Make sure any material retained on the cover is returned to the sample.

If oven drying, consider the sample to be "dry" when the fines are at a constant mass at a temperature of  $230 \pm 9^{\circ}$  F.

5. Determine the mass of a standard graded sample:

Pour the washed and dried fine aggregate into a nest of U.S. Standard sieves from the No. 8 down to the No. 100 including the pan. The amount of material on any 8 inch sieve should not exceed 200 g. The amount of material on a screen may be reduced by sieving the sample in small portions.

Continue sieving for a sufficient period and in such a manner that, after completion, not more than 0.5 percent by mass of the total sample passes any sieve during one minute of continuous hand sieving as described in WYDOT 814.0.

Weigh out and combine the following quantities of fine aggregate, which has been dried and sieved.

| Individual Size Fraction | <u>Mass, g</u> |
|--------------------------|----------------|
| No. 8 to No. 16          | 44             |
| No. 16 to No. 30         | 57             |
| No. 30 to No. 50         | 72             |
| No. 50 to No. 100        | _17            |
|                          | 190 g          |

The tolerance on each of these amounts is  $\pm 0.2$  g.

- 6. Mix the combined test sample with the spatula until it appears to be homogeneous. Position the jar and funnel vertical in the stand and center the cylindrical measure beneath them in the level catch pan. Using a finger to block the opening of the funnel, pour the test sample into the funnel. Level the material in the funnel with the spatula. Remove the finger used as a block and allow the test sample to fall freely into the cylindrical measure.
- 7. After the funnel empties, strike-off excess heaped fine aggregate from the cylindrical measure by a quick single pass of the spatula. The width of the blade should be vertical, keeping the straight part of its edge horizontal and in light contact with the top of the measure.

Until this operation is complete, exercise care to avoid vibration or any disturbance that could cause compaction of the fine aggregate in the cylindrical measure. Brush adhering grains from the outside of the container.

Note: After strike-off, the cylindrical measure may be tapped lightly to compact the sample to make it easier to transfer the container of fine aggregate to the scale or balance without spilling any of the test sample.

Determine and record the mass of the cylindrical measure and fine aggregate to the nearest 0.1 g.

Retain all fine aggregate particles for a second test run.

Recombine the sample from the retaining pan and cylindrical measure and repeat the procedure.

Average the results of the two test run.

- a. Record the mass of the empty cylindrical measure.
- b. For each test run, record the mass of the cylindrical measure and fine aggregate.

Calculations: Calculate the uncompacted voids for the each determination as follows;

$$U = \frac{V - (F / G)}{V} \times 100$$

Where:

V = volume of cylindrical measure, mL;
 F = net mass of fine aggregate in cylindrical measure, g (gross mass minus the mass of the empty measure);
 G = bulk dry specific gravity of fine aggregate;
 U = uncompacted voids in the material, percent;

Calculate the average uncompacted voids for the two determinations.

Report:Report the results on Form E-46. See example in WYDOT 414.0Report the uncompacted voids in percent to the nearest 0.1 percent.Report the specific gravity value used in the calculation.

WYDOT 824.0 (Rev. 01-15)

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### DELETERIOUS SUBSTANCES IN PORTLAND CEMENT CONCRETE

- Scope: This test method describes the procedure for an approximate determination of injurious organic impurities in the fine aggregates for concrete.
- Use: This procedure is used to determine if the fine aggregate for concrete contains organic impurities which could potentially be damaging to the concrete.

Reference

Documents: AASHTO T 21 Standard Method of Test for Organic Impurities in Fine Aggregates for Concrete

- Procedure: Same as AASHTO T 21
- Commentary: Section 9. *Determination of Color Value*; of AASHTO T 21, provides a standard color solution procedure and a glass color standard alternate procedure. Either procedure is acceptable.

If 9.2 *Glass Color Standard Procedure* is used, matching organic plates 1, 2, or 3 is considered acceptable when evaluating organic impurities. If the color matches organic plates 4 or 5 or is darker than organic plate 5, then the fine aggregate is considered to possibly contain injurious organic compounds.

WYDOT 832.0 (Rev. 02-12)

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#### **RESISTANCE R - VALUE AND MOISTURE SENSITIVITY**

Scope: This method describes the testing for determination of the R-Value and moisturesensitivity of soils, subbases, and bases.

> The Moisture Sensitivity procedure uses the results of AASHTO T 190, "Resistance R-Value and Expansion Pressure of Compacted Soils", to determine if a soil, sub-base, base or other unbound material is moisture sensitive. Moisture sensitivity is a factor considered in the acceptance of Crushed Base.

Reference

Documents: AASHTO T 190 Standard Method of Test for Resistance R-Value and Expansion Pressure of Compacted Soils

- Procedure: This procedure is identical to AASHTO T 190 except as modified below:
  - **4.4** Occasionally, material from very plastic, clay-test specimens will extrude from under the mold and around the follower ram during the loading operation. If this occurs between 200 and 400 psi and fewer than five lights are lit, the soils will be reported as less than 5 R-Value (-5). Coarse granular materials and clean sands may require the use of paper baskets to permit testing.

#### Moisture Sensitivity of Unbound Materials

A graph of exudation pressure versus R-Value is developed for the material. The R-Value of the material at 300 psi exudation pressure is then compared to the R-Value at 200 psi exudation pressure. If the difference between the 300 psi R-Value and the 200 psi R-Value is less than or equal to 5, the material will be considered non-moisture sensitive.

Report: Report the gradation R-Value and the moisture-sensitivity.

WYDOT 833.0 (Rev. 02-12)

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# PERCENTAGE OF FLAT AND ELONGATED PARTICLES IN COARSE AGGREGATE

- Scope: This test method describes the determination of the percentages of flat and elongated particles in coarse aggregates at a 1:5 ratio. This procedure is adopted from ASTM D4791.
- Use: Individual particles of aggregate of specific fractions sieve sizes are measured to determine the ratios of length to thickness which can affect the workability of materials. Flat and Elongated Particles is an aggregate quality test that can vary based on the type and amount of crushing effort. A specification for Flat and Elongated Particles is typical for flexible pavements.
- Apparatus: 1. Proportional Caliper Device

The proportional caliper device illustrated in Figure 1 of this section is an example of an apparatus suitable for this test method. It consists of a base plate with two fixed posts and a swinging arm mounted between them so that the openings between the arms and the posts maintain a constant ratio. The axis position can be adjusted to provide the desired ratio of opening dimensions. Figure 1 of this section illustrates a device on which ratios of 1:2, 1:3, and 1:5 may be set. For Hot Plant Mix aggregate, a 1:5 ratio is specified.

2. Balance

Reference

The balance or scales used be accurate to 0.5% of the mass of the sample.

| nerenee    |             |  |
|------------|-------------|--|
| Documents: | ASTM D4791  | Standard Test Method for Flat Particles, Elongated   |
|            |             | Particles, or Flat and Elongated Particles in Coarse |
|            |             | Aggregate  |
|            | WYDOT 414.0 | Marshall and Superpave Mix Design and Mix Volumetric |
|            |             | Verification Procedure                               |
|            | WYDOT 804.0 | Aggregate Sampling                                   |
|            | WYDOT 805.0 | Sample Splitting by Mechanical Splitter              |
|            | WYDOT 814.0 | Sieve Analysis of Combined Aggregate                 |
|            | WYDOT E-46  | Job Mix Formula                                      |
|            | WYDOT T-159 | Flat & Elongated and Fractured Faces                 |
|            | WYDOT T-166 | Aggregate Analysis                                   |
|            |             |  |

WYDOT 835.0 (Rev. 09-16)

Sampling: Sample the coarse aggregate in accordance with WYDOT 804.0.

Thoroughly mix the sample and reduce it to an amount suitable for testing using WYDOT 805.0. The sample for testing must be approximately the mass desired when dry.

Procedure: Determination will be by % mass. Oven dry the sample to constant mass at a temperature of 230 °F  $\pm$  9 °F.

Sieve the sample of coarse aggregate to be tested in accordance with WYDOT 814.0.

Reduce each size fraction larger than the No. 4 sieve present in the amount of 10% or more of the original sample in accordance with WYDOT 805.0 until approximately 100 particles are obtained for each sieve.

Use the proportional caliper device as follows:

*Flat and Elongated Test* - Adjust the caliper device to test at 1:5 ratio. Set the larger opening equal to the particle length. The particle is flat and elongated if the thickness of the particle can pass through the smaller opening of the caliper.

After the particles have been classified into the group described above, determine the proportion of the sample in each group by % mass.

Calculation: Calculate the percentage of flat and elongated particles to the nearest 1 percent for each sieve size greater than No. 4.

Assume that the sieve sizes not tested (those representing less than 10 percent of the sample) have the same percentage of flat and elongated particles as the next smaller or the next larger sizes, or use the average for the next smaller and larger sizes, if both are present.

Report: Use the worksheet T-159 to correct the value so it is representative of the sample. See example in WYDOT 414.0.

Report the final values on Form E-46 or Form T-166.



Figure 1 - Proportional Caliper

WYDOT 835.0 (Rev. 09-16)

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#### FINE AGGREGATE SAND EQUIVALENT

- Scope: This test method covers the procedure for determining the sand equivalent (SE) of fine aggregate samples.
- Use: This procedure is used to determine the relative proportion of fine dust or clay-like material in fine aggregate. It uses settling rates in a calcium chloride flocculating solution to establish the relative amounts of slow and rapid settling material in a sample passing the No. 4 sieve. SE is an indicator of the quality of the minus No. 4 pit run filler. A specification for SE is typical for Hot Plant Mix aggregate.

#### Reference

| Documents: | AASHTO T 176 | Standard Method of Test for Plastic Fines in Graded     |
|------------|--------------|---|
|            |              | Aggregates and Soils by Use of the Sand Equivalent Test |
|            | WYDOT 414.0  | Marshall and Superpave Mix Design and Mix Volumetric    |
|            |              | Verification Procedure                                  |
|            | WYDOT E-46   | Job Mix Formula   |
|            |              |   |

Procedure: Perform according to AASHTO T 176.

To be consistent with the procedure used in WYDOT Materials Program, a mechanized shaker is recommended.

Report: Report the results on Form E-46. See example in WYDOT 414.0.

WYDOT 836.0 (Rev. 02-12)

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### INSOLUBLE RESIDUE BY WET METHOD OR BY X - RAY FLUORESCENCE SPECTROMETRY

- Scope: This method describes the quantitative determination of acid soluble and insoluble compounds found in aggregates used for surfacing, typically chip seal or plant mix wearing course. The standard procedure is adopted from ASTM D3042 *Standard Test Method for Insoluble Residue in Carbonate Aggregates*. This method is limited to quantitative determinations of the following analytes: SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, CaCO<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, MgCO<sub>3</sub>, Na<sub>2</sub>O and K<sub>2</sub>O.
- Use: Wyoming requires ASTM D3042 Section 7, "Procedure for Determining Only the Plus 75 µm (No. 200) Size Fraction of Insoluble Residue".

Reference

| Documents: | ASTM D3042   | Standard Test Method for Insoluble Residue in Carbonate |
|------------|--------------|---|
|            |              | Aggregates, Section 7                                   |
|            | WYDOT T-107W | Report of Test on Aggregate                             |

Discussion: Acid solubility may be estimated by the quantities of certain compounds in an aggregate source. Aggregates containing high percentages of  $SiO_2$  and  $Al_2O_3$  will be more acid insoluble as compared to samples containing high percentages of  $CaCO_3$ ,  $Fe_2O_3$ , and  $MgCO_3$  (i.e., acid soluble).<sup>1</sup> Numerous reports indicate a strong correlation between acid insolubility of aggregates and a resistance to polishing.

The X-Ray Fluorescence Spectrometry (XRFS) method has the following limitations:

- 1. Inorganic, element analysis only (i.e., non-carbon);
- 2. Cannot determine molecular structure (conversion from element detection to compounds actually present is problematic); and
- 3. Limited subset of the most common 11 elements typically found in aggregates analyzed.

Because of the above limitations, and primarily because the molecular structure of compounds cannot be definitively determined (for example, is MgO, MgCO<sub>3</sub> or both present), this method can produce erroneous results for acid insolubility of an aggregate source. However, the method can be used for quick, qualitative analysis of aggregates to determine if aluminum and/or silicon are of such high

concentrations that it clearly identifies the aggregate as acid insoluble. For these reasons, the Materials Program does not recommend the XRFS method for aggregate acceptance testing. The XRFS may be utilized for preliminary evaluation of aggregate sources, although further evaluation with ASTM D3042 may be indicated.

Report: See attached example report Form T-107W.

### <sup>1</sup> CRC Handbook of Chemistry and Physics, Section B, The Elements and Inorganic Compounds -

Refer to Table of Physical Constants of Inorganic Compounds (acid solubility characteristics) for the following compounds; Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, CaCO<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, and MgCO<sub>3</sub>.

Refer to Table of Gravimetric Factors and their Logarithms for the following compounds; MgO, Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, P<sub>2</sub>O<sub>5</sub>, CaO, TiO<sub>2</sub>, MnO, Fe<sub>2</sub>O<sub>3</sub>, CaCO<sub>3</sub>, MgCO<sub>3</sub>.

| WYOMING DEPARTMENT OF TRANSPORT | ATION |
|---------------------------------|-------|
| MATERIALS TESTING LABORATORY    |       |
| REPORT OF TEST ON AGGREGATE     |       |

|     | T-107W<br>(Rev.09-16) |
|-----|-----------------------|
| DC; | Soils/Surfacing       |
|     | EAU ENOD              |

| Project No(s).:              | ERP Project Number  |
|------------------------------|---------------------|
| Submitted By:                | Joe Tester          |
| Identification Marks:        |                     |
| Source or Brand:             | Pit Name            |
| <b>Quantity Represented:</b> | Total Plan Quantity |
| Date Received:               | 9/10/2016           |

| Laboratory No.: |                         |  |
|-----------------|-------------------------|--|
| Location:       | Project Location        |  |
| At:             | Resident Engineers Town |  |
| Date Sampled:   | 9/16/2016               |  |
| For Use As:     | On Plans                |  |
| Date Tested:    | 9/10/2016               |  |

TEST RESULTS

INSOLUBLE RESIDUE IN CARBONATE AGGREGATES (ASTM D3042, Section 7)

|                           | 806.258 |
|---------------------------|---------|
| Total Weight #200 sieve = | 327.395 |
| Tare Weight #200 sieve =  | 478.863 |
| Insol Weight =            |         |

SAMPLE Weight = 494.480

TOTAL INSOLUBLE RESIDUE = 96.842 %

Field Remarks:

Lab Remarks;

Greg Milburn P.E. STATE MATERIALS ENGINEER Tested By: Reviewed By:

MATERIALS ENGINEER

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### PERCENT PHOSPHORIC ACID and PHOSPHORUS CONTENT in ASPHALT By X-RAY FLUORESCENCE SPECTROMETRY

- Scope: This procedure describes how to quantitatively determine percent of phosphoric acid (deca-acid oligomer form) and phosphorus content in asphalt binder.
- Use: This method is limited to x-ray fluorescence spectrometer (XRFS) using an energy-dispersive detector measuring low levels (ppm accuracy) of elemental phosphorus under positive helium pressure instead of vacuum. To ensure accuracy of phosphorus measurement, by correcting for various masking and interference effects, detector will also measure energy levels for adjacent elements to phosphorus (including but not limited to silicon, sulfur, arsenic, etc).

### Reference

- Documents: WRI Calculation of Phosphorous Content of Phosphoric Acid Oligomers (Western Research Institute, Laramie, WY; Michael Harnsberger, February 28, 2007)
  - WAL Phosphorus Content (ppm) of Asphalt Binder Samples (Wyoming Analytical Laboratories, Golden, CO; Chuck Wilson, March 28, 2007)
- Apparatus: 1. X-Ray fluorescence spectrometer, including:
  - a. X-ray detector; energy-dispersive (EDXRF), using helium gas background instead of vacuum.
  - b. Liquid sample cups using 6.0 micron poly carbonate or Mylar film for both standard (control) and test samples.
  - 2. Helium gas, reagent grade, 99.5% minimum purity
  - 3. Standard (control) samples of asphalt binder with known concentrations of phosphoric acid and SBS polymer. Standard samples are as follows:
    - a. 0% phosphoric acid (PA), 0% SBS polymer
      b. 0% PA, 2.5% SBS
      c. 0.2% PA, 2.5% SBS
      d. 0.4% PA, 2.5% SBS
      e. 0.8% PA, 2.5% SBS
      f. 1.6% PA, 2.5% SBS
- Procedure: 1. Obtain or prepare standard (control) samples of asphalt binder with known concentrations of phosphoric acid and SBS polymer. If samples are prepared, use low shear mixer to blend phosphoric acid and SBS polymer at a temperature of 295 °F for 1 hour. When blending, measure mass of base asphalt and SBS polymer to 2 decimal places and mass of phosphoric acid to 4 decimal places.

- 2. For each standard (control) sample, pour sample solution into liquid sample cup to a level of <sup>1</sup>/<sub>4</sub> to <sup>3</sup>/<sub>8</sub> inch (approx. 6 to 10 millimeters). Let sample cool to temperature of 72 °F before testing in XRFS. Make sure there are no wrinkles or bulges in the film of the windows.
- 3. Place standard (control) sample into test chamber of XRFS and measure for elemental phosphorus. Repeat for each standard (control) sample.
- 4. Heat and liquefy asphalt binder test samples to pour into liquid sample cup to a level of <sup>1</sup>/<sub>4</sub> to <sup>3</sup>/<sub>8</sub> inch (approx. 6 to 10 millimeters). Let sample cool to temperature of 72 °F before testing in XRFS. Make sure there are no wrinkles or bulges in the film of the windows.
- 5. Place asphalt binder test sample into test chamber of XRFS and measure for elemental phosphorus. Repeat for each test sample.
- 6. Determine percent weight phosphoric acid (%) and phosphorus content (ppm) using either Method A, Bracketing Standards, or Method B, Calibration/Regression Line -

Method A, Bracketing Standards -

Calculate and record percent weight phosphoric acid (% PA), to the nearest 0.01, for each test sample according to the following equation:

$$\left[\left\{\frac{(cps, P \text{ in test sample}) - A}{(B - A)}\right\} x C\right] + D = \% PA$$

cps = counts per second, elemental phosphorus

- A = Low bracketing standard (control) sample, cps
- B = High bracketing standard (control) sample, cps
- C = Difference, in % PA, between bracketing standards
- D = % PA for low bracketing standard (control) sample

Calculate and record phosphorus content (ppm), to the nearest whole number, for each test sample according to the following equation:

3530.652 x (% PA) + 134.674 = ppm, Phosphorus

### Method B, Calibration/Regression Line -

Standard (control) samples can be measured for elemental phosphorus and a calibration/regression line generated based on intensity. Calibration/regression line must not exceed 0.006 standard deviation. Using the calibration/regression line, calculate and record percent weight phosphoric acid (%PA) and phosphorus content (ppm).

- **NOTE**: Difference(s) between Method A and Method B must not exceed 0.01% PA. If difference is greater than 0.01% PA, then Method A must be used (counts per second, cps, methodology).
- 7. Report test sample ID number, manufacturer/supplier, PGAB grade, percent weight phosphoric acid (nearest 0.01, %), phosphorus content (nearest whole number, ppm), and date tested for each asphalt binder test sample.

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### LIQUID ASPHALT SAMPLING

- Scope: Submit sample(s) to Materials Program according to requirements described below for all liquid asphalt (each different type or grade) supplied for road construction or maintenance projects. Examples of referenced Forms T-121, E-221, and E-224 follow in this section.
- Use: Asphalt samples are required for many products for QC and QA testing. While this procedure can be used for both types of samples, it must be followed for QA samples. Refer to applicable specification for additional information not mentioned in this section.
- Apparatus: 1. Waste container (minimum 2 gallon capacity)
  - 2. Sample containers (clean,  $1 \pm$  quart capacity)
    - a. Performance graded binder (PGAB) <u>Use metal screw cap cans</u>, <u>cans</u>, American Can #10201 can / #18914 cap or equivalent (WYDOT #FT1700).
    - b. Emulsified asphalt Use plastic containers as specified in Subsection 407.4.2, Sampling Procedures, Nalgene #2104-003 or equivalent (WYDOT #FT1730).
  - 2. Heat resistant gloves / protective clothing liquid temperatures may exceed 150° F
  - 3. Rags (clean) for cleaning excess material from sample container. Do not use water or solvent (gasoline, diesel fuel, etc.) to clean container.
  - 4. Tape
  - 5. Documentation: Each sample <u>requires</u> the following:
    - a. Form T-121, *Sample Transmittal Asphalt*
    - b. Weight ticket/information (Emulsified Asphalt) or Invoice (PGAB)
    - c. Certificate of Compliance (COC)
    - d. Bill of Lading (BOL) or shipping manifest

Note: BOL may include all appropriate information

### Reference

| WYDOT Constructio | n Manual   |
|-------------------|--|
| WYDOT E-221       | Pay Adjustment for Performance Graded Asphalt Binder |
| WYDOT E-224       | Pay Adjustment for Emulsified Asphalt                |
| WYDOT T-121       | Sample Transmittal Asphalt                           |
| WYDOT T-128       | Construction Test Requirements                       |
|                   | WYDOT E-221<br>WYDOT E-224<br>WYDOT T-121            |

Procedures: Sample liquid asphalt according to the following table:

|   |  |   | id Asphalt Sa   |                               |  |  |
|---|--|---|---|-------------------------------|--|--|
| Т   | <b>D</b> 0                                 | Point of  |   | Docume                        | ntation  | Timeline   |
| 1 9   | pe   | Acceptance  | WYDOT   | Forms                         |  | (submit  |
| Asphalt   | Sample                                     | (remove debris<br>from valve by<br>discarding<br>1 gallon before<br>sampling)   | Numbering<br>of<br>Samples                                  | Record<br>receipt,<br>payment | Other  | sample to<br>arrive at<br>Materials Lab<br>As Soon As<br>Possible) |
|   | Quality,<br>Q <sup>(1)</sup>               | By Supplier;<br>at time of loading;<br>sampling valve at<br>refinery  | Lab Report  | E-224                         | Lab Report   | By Supplier;<br>after sampling                                     |
| Emulsified<br>(Applies to<br>both tack oils<br>and chip seal<br>oils) | QA<br>Verification<br>, FCS <sup>(2)</sup> | By Engineer;<br>at time of<br>unloading;<br>sampling valve on<br>tanker/pup <sup>(4)</sup><br>(see Figure 1)  | T-121; use  | N/A                           | Use Bill-Of-Lading<br>(BOL)<br>or manifest number;<br><i>NOT 'Control</i><br><i>Number'</i> ;<br>must include supplier<br>batch and storage<br>tank numbers  | By Engineer;<br>after sampling                                     |
| Performance<br>Graded<br>Binder<br>(PGAB)                             | Quality,<br>Q <sup>(3)</sup>               | By Contractor;<br>when mix plant<br>operating and<br>engineer present;<br>sampling valve on<br>supply line<br>between<br>storage tank and<br>mixer<br>(see Figures 2 & 3) | designation<br>noted on<br>T-128;<br>number<br>sequentially | E-221                         | Mark sample cans<br>with<br>Lot and Sublot<br>numbers;<br>securely tape<br>together;<br>Submit 'incomplete'<br>lot(s), 'as is', at end<br>of season; 5 sublots<br>per lot usually but<br>can vary 3 to 7 | By Engineer;<br>after each lot is<br>completed                     |

Liquid Asphalt Sampling

<sup>(1)</sup> One quart; each load; not required if 5 tons or less

<sup>(2)</sup> One quart; every 200 tons (must be same batch, same tank from supplier)

<sup>(3)</sup> Two quarts; every 100 tons (1 sublot); not required if project quantity less than 100 tons

<sup>(4)</sup> Ensure the two tests represent the same material. The Materials Program requires the following information to have the system work correctly when field check samples are received:

- a. Refinery sample dates
- b. Field sample dates

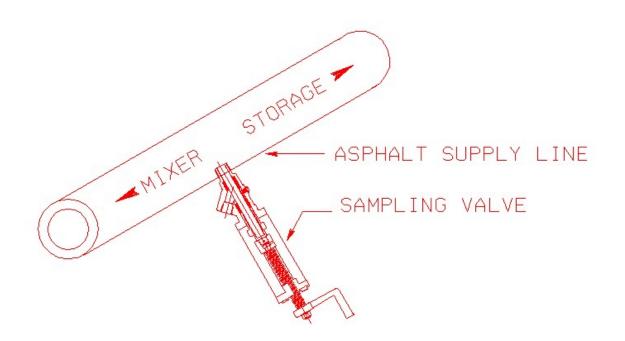
c. BOL numbers must match or the results will be meaningless



**Figure 1 - Typical Sampling Valve for Tanker** 



**Figure 2 - Typical Sampling Valve for Storage Tank** 



## **Figure 3 - Typical Sampling Valve for Asphalt Supply Line**

Typical sampling valve is Rod Seal Valve/Figure 8115 Sampling Valve with a "contoured halfcoupling" (for mounting to asphalt supply line pipeline) manufactured by Fetterolf Corporation, P.O. Box 103, Skippack, PA 19474-0103, (610) 584-1500, or equivalent.



### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SAMPLE TRANSMITTAL ASPHALT

| LAB USE ONLY:   |
|---|
| LAB NO:   |
| DATE RECEIVED:  |
| Project No.(s): ERP Project Number  |
| Engineer: Resident Engineer City: Resident Engineer's Town State: WY                                    |
| Sampled Date: Date Sampled (mm/dd/yy)   |
| Source (Refinery): Refinery Name City: Refinery City State: Refinery State                              |
| Grade: Performance Graded Emulsion:   |
| Type     Grade     Type     Grade       Quantity Represented:     Tons Represented     Tons Represented |
| Invoice, C.O.C. or Bill of Lading #(s): Invoice, C.O.C., or Bill of Lading Number (BOL)                 |
| Quality # or Field Sample #: As Required  |
| PG ONLY Asphalt Binder: Lot #: Sublot #: of   |
| Remarks: Sampling Documentation   |
|   |
|   |
|   |
|   |
|   |
| Submitted By: Technician  |

### WYOMING DEPARTMENT OF TRANSPORTATION PAY ADJUSTMENT FOR PERFORMANCE GRADED ASPHALT BINDER

Form E-221 (Rev. 08-16)

Project Number: N442077

Project Name: Osage - Newcastle (Newcastle Marginal) PGAB Grade: PG 64-28 Resident Engineer: John Leahy, P.E.

Engineer's Town: Newcastle

| PGAB             | Grade: PG 6       | 4-28 |           |                  |                    |                  |           | Approv | ed By: n/a           |            |  | Date:   |
|------------------|-------------------|------|-----------|------------------|--------------------|------------------|-----------|--------|----------------------|------------|--|---------|
|                  | Refinery          |      | Field Acc | eptance Sa       | mple               | (1)              | (2)       | (3)    | (4)                  | (5)        | Pay                                      | 1       |
| Date<br>Received | Invoice<br>Number | Lot  | Sublot    | Sample<br>Number | Lab Test<br>Report | Received<br>Tons | Void Tons | Net    | Contractor's<br>Cost | Pay Factor | Adjustment<br>((3) x (4) x<br>[(5)-1.0)] | Remarks |
| 08/25/2018       | 246861            | 0    | 0         | 0                |                    | 37.97            | 0.00      | 37.97  | \$0.00               | .00        | \$0.00                                   |         |
| 08/25/2018       | 246753            | 0    | 0         | 0                |                    | 38.60            | 0.00      | 38.60  | \$0.00               | .00        | \$0.00                                   |         |
| 08/25/2018       | 103771            | 0    | 0         | 0                |                    | 19.24            | 0.00      | 19.24  | \$0.00               | .00        | \$0.00                                   |         |
| 08/25/2018       | 247193            | 0    | 0         | 0                |                    | 36.93            | 0.00      | 36.93  | \$0.00               | .00        | \$0.00                                   |         |
| 08/25/2018       | 247136            | 0    | 0         | 0                |                    | 38.69            | 0.00      | 38.69  | \$0.00               | .00        | \$0.00                                   |         |
| 08/27/2018       | 247137            | 0    | 0         | 0                |                    | 38.19            | 0.00      | 38.19  | \$0.00               | .00        | \$0.00                                   |         |
| 08/27/2018       | 247283            | 0    | 0         | 0                |                    | 38.57            | 0.00      | 38.57  | \$0.00               | .00        | \$0.00                                   |         |
|                  |                   |      |           |                  |                    |                  | 1.16      | 248.19 |                      |            | \$0.00                                   |         |

8/28/2018 8:02:58 PM

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| 1           | DEPARTNENT                       |  |                       |                        | c                   |   |                        |                       |                           |                          |                                     | Sheet<br>of                                    |
|-------------|----------------------------------|--|-----------------------|------------------------|---------------------|---|------------------------|-----------------------|---------------------------|--------------------------|-------------------------------------|--|
| oje<br>nt E | Number:<br>ct Name:<br>Engineer: | Project Number: ERP Project Number<br>Project Name: <u>Name of Project</u><br>Resident Engineer: Engineer's Name | imber<br>ct<br>1e     |                        | ‴ ទូ ទ              | Signatures<br>Computed By: Technician's Name<br>Checked By: Technician's Name | Technicia<br>Technicia | in's Name<br>n's Name |                           |                          | Date: 2                             | Date: <u>XX/XX/XX</u><br>Date: <u>XX/XX/XX</u> |
| ee          | r's Town:                        | Engineer's Town: Engineer's Town   | u.                    |                        |                     | Engineer: Engineer's Name   | Engineer'              | s Name                |                           |                          | Date:                               | Date: XX/XX/XX                                 |
|             |                                  |  |                       |                        |                     |   |                        |                       |                           |                          | Check if Final Report               | eport 🗆  |
|             |                                  | Refinery Acceptance Sample   | tance Sample          | FIELD                  | FIELD               | (1)   | (2)                    | (6)                   | (4)                       | 3                        | PAY                                 |  |
| A           | ASPHALT                          |  |                       | SCREEN                 | CHECK               |   | Quantity               |                       | CONTRACTOR'S              | PERCENT ADJ.             | ADJUSTMENT                          | REMARKS  |
| IXI         | PE/GRADE                         | RECEIVED TYPE/GRADE BELL-OF-LADING<br>NUMBER   | ** LAB TEST<br>REPORT | Accept<br>or<br>Reject | SAMPLE<br>(FCS-EA#) | TONS<br>RECEIVED  | TONS                   | NET<br>(1) - (2)      | COST<br>(F.O.B. Refinery) | (see Lab<br>Test Report) | (3) x (4) x<br>[-1 x { (5) / 100 }] |  |
|             | CSS-1                            | 5034012  | 16-029                | Accept                 |                     | 8.740   |                        | 6.740                 | \$146.00                  | 000                      | \$0.00                              | Transferred from P141018                       |
|             | CSS-1                            | 5034262  | 16-143                | Accept                 |                     | 21.880  |                        | 21.880                | \$146.00                  | 5.00                     | (\$ 158.72)                         | No refinery sample to Lab                      |
| ľ           | CSS-1H                           | 5034437  | 16-016                | Accept                 |                     | 24,290  |                        | 24.290                | \$146.00                  | 00.0                     | \$0.00                              |  |
|             | CRS-2                            | 5034538  | 18-025                | Accept                 |                     | 34,930  | 10.740                 | 24,190                | \$146,00                  | 0.0                      | \$0.00                              | Void and used for county job                   |
| L           | CRS-2                            | 5034826  | (6-028                | Accept                 |                     | 40.130  |                        | 40.130                | \$146.00                  | 10.00                    | (\$585.90)                          |  |
|             | CRS-2                            | 5034562  |                       | Reject                 |                     |   |                        |                       | \$146.00                  | 0.00                     |                                     |  |
|             | CRS-2                            | 5034775  |                       | Reject                 |                     |   |                        |                       | \$146.00                  | 0.00                     |                                     |  |
|             | CRS-2                            | 5034654  | 16-054                | Accept                 | 1                   | 36.720  |                        | 36.720                | \$146,00                  | 00'0                     | \$0.00                              |  |
|             | CRS-2                            | 5035162  | 16-059                | Accept                 | 2                   | 13,860  |                        | 13.88.0               | \$146.00                  | 0.00                     | \$0.00                              |  |
|             | CRS-2                            | 1.869805   | 16-182                | Accept                 |                     | 34.310  |                        | 34.310                | \$146.00                  | 25.00                    | (\$1,252.32)                        |  |
|             | CRS-2                            | 5036982  |                       | Reject                 |                     |   |                        |                       | \$146,00                  | 0.00                     |                                     |  |
|             | CRS-2                            | 5037100  | 16-242                | Accept                 |                     | 40.530  |                        | 40.530                | \$146.00                  | 5,00                     | (\$ 295,87)                         | No refinery sample to Lab                      |
|             | CRS-2P                           | 5037831  | 16-201                | Accept                 |                     | 24.760  | 1                      | 24.780                | \$190,00                  | 0.00                     | \$0.00                              |  |
|             | CRS-2P                           | 5037928  |                       | Accept                 |                     | 37,720  |                        | 37,720                | \$130.00                  | 00'0                     | \$0.00                              | Waiting for lab report                         |
|             | CRS-2P                           | 5037929  |                       | Reject                 |                     |   |                        |                       | \$190,00                  | 0.00                     |                                     |  |
|             | CRS-2P                           | 5036044  |                       | Accept                 |                     | 35.780  |                        | 35.780                | \$190.00                  | 0.00                     | \$0.00                              | Waiting for lab report                         |
|             | HFRS-2P                          | 5039567  |                       | Reject                 |                     |   |                        |                       | \$225,00                  | 00.0                     |                                     |  |
| 1.          | HFRS-2P                          | 5039972  |                       | Accept                 | 8                   | 23.940  |                        | 23.940                | \$225,00                  | 0.00                     | \$0.00                              | Waiting for lab report                         |
|             |                                  |  |                       |                        |                     | SHEET   | SHEET TOTAL            | 364.850               | -s                        | SHEET TOTAL              | (\$2,293.81)                        |  |

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### ASPHALT VOLUME CORRECTION TABLE

- Scope: The temperature of 60 °F is customarily used as a standard for volume determination of asphalts. A unit volume of asphalt will change with each degree of temperature change (Coefficient of Volumetric Expansion). The correction factor varies with the specific gravity. The table below is applicable for <u>all asphaltic materials</u>, including emulsions (undiluted).
- Use: The table in this section is used for volume correction of asphaltic materials based on specific gravity and temperature. The temperature correction factor is used on WYDOT Form E-56, *Daily Asphalt and Lime Report* and is used in conjunction with WYDOT 421.0 to determine the percent of asphalt in hot plant mix material. Prime Coat used for calculating spread rates for tack, seal, chip and fog seals in conjunction with Form E-58, *Daily Emulsion Application Rate Record* and the WYDOT Construction Manual.

Reference

Documents:WYDOT 421.0Asphalt/Lime Content Report (Invoice and Tank Volume)WYDOT E-56Daily Asphalt and Lime ReportWYDOT Construction ManualWYDOT E-58WYDOT E-58Daily Emulsion Application Rate Record

- Procedure: Upon receiving the product shipment of semi-solid asphalt materials, obtain the Bill of Lading (BOL) or Certificate of Compliance (COC) of the truck manifest and weigh ticket. Note the specific gravity of the product as listed on the manifest. Following the procedure as required in WYDOT 421.0, determine the temperature of the tank being measured. Using the tank stab temperature and the specific gravity of the product, determine the temperature correction factor, interpolating between the two columns in which the manifest specific gravity falls.
- Example: If the specific gravity equals 0.985 at 60 °F and the volume measured equals 9,000 gal at 180 °F, read the table at 180 °F and interpolate between 0.9593 and 0.9633 (from the 0.950 column and the 1.000 column) as follows:

$$0.9593 + \left(\frac{0.9633 - 0.9593}{1.000 - 0.950}\right) \times (0.985 - 0.95) = 0.9593 + 0.0028 = 0.9621$$

Therefore, the corrected volume at 60 equals 9,000 gal x 0.9621 equals 8659 gal.

| WYDOT 841.0  |  |
|--------------|--|
| (Rev. 10-17) |  |

|             | <b>CORRECTION FACTORS</b> (to determine volume at 60 °F) |        |        |        |        |        |  |  |
|-------------|--|--------|--------|--------|--------|--------|--|--|
| Temperature | Specific Gravity at 60 °F                                |        |        |        |        |        |  |  |
| ° <b>F</b>  | 0.800  | 0.850  | 0.900  | 0.950  | 1.000  | 1.050  |  |  |
| 40          | 1.0095   | 1.0085 | 1.0075 | 1.0068 | 1.0061 | 1.0055 |  |  |
| 41          | 1.0091   | 1.0081 | 1.0072 | 1.0065 | 1.0058 | 1.0053 |  |  |
| 42          | 1.0086   | 1.0076 | 1.0068 | 1.0061 | 1.0055 | 1.0050 |  |  |
| 43          | 1.0081   | 1.0072 | 1.0064 | 1.0058 | 1.0052 | 1.0047 |  |  |
| 44          | 1.0076   | 1.0068 | 1.0060 | 1.0054 | 1.0049 | 1.0044 |  |  |
| 45          | 1.0072   | 1.0064 | 1.0057 | 1.0051 | 1.0046 | 1.0042 |  |  |
| 46          | 1.0067   | 1.0059 | 1.0053 | 1.0047 | 1.0043 | 1.0039 |  |  |
| 47          | 1.0062   | 1.0055 | 1.0049 | 1.0044 | 1.0040 | 1.0036 |  |  |
| 48          | 1.0057   | 1.0051 | 1.0045 | 1.0041 | 1.0037 | 1.0033 |  |  |
| 49          | 1.0053   | 1.0047 | 1.0042 | 1.0038 | 1.0034 | 1.0031 |  |  |
| 50          | 1.0048   | 1.0042 | 1.0038 | 1.0034 | 1.0031 | 1.0028 |  |  |
| 51          | 1.0043   | 1.0038 | 1.0034 | 1.0031 | 1.0028 | 1.0025 |  |  |
| 52          | 1.0038   | 1.0034 | 1.0030 | 1.0027 | 1.0024 | 1.0022 |  |  |
| 53          | 1.0034   | 1.0030 | 1.0027 | 1.0024 | 1.0021 | 1.0020 |  |  |
| 54          | 1.0029   | 1.0025 | 1.0023 | 1.0020 | 1.0018 | 1.0017 |  |  |
| 55          | 1.0024   | 1.0021 | 1.0019 | 1.0017 | 1.0015 | 1.0014 |  |  |
| 56          | 1.0019   | 1.0017 | 1.0015 | 1.0014 | 1.0012 | 1.0011 |  |  |
| 57          | 1.0015   | 1.0013 | 1.0012 | 1.0011 | 1.0009 | 1.0009 |  |  |
| 58          | 1.0010   | 1.0008 | 1.0008 | 1.0007 | 1.0006 | 1.0006 |  |  |
| 59          | 1.0005   | 1.0004 | 1.0004 | 1.0004 | 1.0003 | 1.0003 |  |  |
| 60          | 1.0000   | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |  |  |
| 61          | 0.9995   | 0.9996 | 0.9996 | 0.9997 | 0.9997 | 0.9997 |  |  |
| 62          | 0.9990   | 0.9992 | 0.9992 | 0.9993 | 0.9994 | 0.9994 |  |  |
| 63          | 0.9986   | 0.9988 | 0.9989 | 0.9990 | 0.9991 | 0.9992 |  |  |
| 64          | 0.9981   | 0.9983 | 0.9985 | 0.9986 | 0.9988 | 0.9989 |  |  |
| 65          | 0.9976   | 0.9979 | 0.9981 | 0.9983 | 0.9985 | 0.9986 |  |  |
| 66          | 0.9971   | 0.9975 | 0.9977 | 0.9980 | 0.9982 | 0.9983 |  |  |
| 67          | 0.9967   | 0.9969 | 0.9972 | 0.9975 | 0.9978 | 0.9980 |  |  |
| 68          | 0.9962   | 0.9962 | 0.9966 | 0.9970 | 0.9973 | 0.9976 |  |  |
| 69          | 0.9957   | 0.9960 | 0.9964 | 0.9968 | 0.9971 | 0.9974 |  |  |
| 70          | 0.9952   | 0.9958 | 0.9962 | 0.9966 | 0.9969 | 0.9972 |  |  |
| 71          | 0.9948   | 0.9954 | 0.9959 | 0.9963 | 0.9966 | 0.9970 |  |  |
| 72          | 0.9943   | 0.9949 | 0.9955 | 0.9959 | 0.9963 | 0.9967 |  |  |
| 73          | 0.9938   | 0.9945 | 0.9951 | 0.9956 | 0.9960 | 0.9964 |  |  |
| 74          | 0.9933   | 0.9941 | 0.9947 | 0.9953 | 0.9957 | 0.9961 |  |  |
| 75          | 0.9929   | 0.9937 | 0.9944 | 0.9950 | 0.9954 | 0.9959 |  |  |
| 76          | 0.9924   | 0.9932 | 0.9940 | 0.9946 | 0.9951 | 0.9956 |  |  |
| 77          | 0.9919   | 0.9928 | 0.9936 | 0.9943 | 0.9948 | 0.9953 |  |  |
| 78          | 0.9914   | 0.9924 | 0.9932 | 0.9939 | 0.9945 | 0.9950 |  |  |

| Temperature | Specific Gravity at 60 °F |        |        |        |        |        |  |
|-------------|---------------------------|--------|--------|--------|--------|--------|--|
| ° <b>F</b>  | 0.800                     | 0.850  | 0.900  | 0.950  | 1.000  | 1.050  |  |
| 79          | 0.9910                    | 0.9920 | 0.9929 | 0.9936 | 0.9942 | 0.9948 |  |
| 80          | 0.9905                    | 0.9915 | 0.9925 | 0.9932 | 0.9939 | 0.9945 |  |
| 81          | 0.9900                    | 0.9911 | 0.9921 | 0.9929 | 0.9936 | 0.9942 |  |
| 82          | 0.9895                    | 0.9907 | 0.9917 | 0.9926 | 0.9933 | 0.9939 |  |
| 83          | 0.9890                    | 0.9903 | 0.9913 | 0.9923 | 0.9930 | 0.9936 |  |
| 84          | 0.9885                    | 0.9899 | 0.9909 | 0.9919 | 0.9927 | 0.9933 |  |
| 85          | 0.9881                    | 0.9895 | 0.9906 | 0.9916 | 0.9924 | 0.9931 |  |
| 86          | 0.9876                    | 0.9890 | 0.9902 | 0.9912 | 0.9921 | 0.9928 |  |
| 87          | 0.9871                    | 0.9886 | 0.9898 | 0.9909 | 0.9918 | 0.9928 |  |
| 88          | 0.9866                    | 0.9882 | 0.9894 | 0.9905 | 0.9914 | 0.9928 |  |
| 89          | 0.9862                    | 0.9878 | 0.9891 | 0.9902 | 0.9911 | 0.9923 |  |
| 90          | 0.9857                    | 0.9873 | 0.9887 | 0.9898 | 0.9908 | 0.9917 |  |
| 91          | 0.9852                    | 0.9869 | 0.9883 | 0.9895 | 0.9905 | 0.9914 |  |
| 92          | 0.9847                    | 0.9865 | 0.9879 | 0.9892 | 0.9902 | 0.9911 |  |
| 93          | 0.9843                    | 0.9861 | 0.9876 | 0.9889 | 0.9899 | 0.9909 |  |
| 94          | 0.9838                    | 0.9856 | 0.9872 | 0.9885 | 0.9896 | 0.9906 |  |
| 95          | 0.9833                    | 0.9852 | 0.9868 | 0.9882 | 0.9893 | 0.9903 |  |
| 96          | 0.9828                    | 0.9848 | 0.9864 | 0.9878 | 0.9890 | 0.9900 |  |
| 97          | 0.9824                    | 0.9844 | 0.9861 | 0.9875 | 0.9887 | 0.9898 |  |
| 98          | 0.9819                    | 0.9839 | 0.9857 | 0.9871 | 0.9884 | 0.9895 |  |
| 99          | 0.9814                    | 0.9835 | 0.9853 | 0.9868 | 0.9881 | 0.9892 |  |
| 100         | 0.9809                    | 0.9831 | 0.9849 | 0.9865 | 0.9878 | 0.9889 |  |
| 101         | 0.9804                    | 0.9827 | 0.9846 | 0.9862 | 0.9875 | 0.9937 |  |
| 102         | 0.9799                    | 0.9822 | 0.9842 | 0.9858 | 0.9872 | 0.9984 |  |
| 103         | 0.9795                    | 0.9818 | 0.9838 | 0.9855 | 0.9869 | 0.9931 |  |
| 104         | 0.9790                    | 0.9814 | 0.9834 | 0.9851 | 0.9866 | 0.9878 |  |
| 105         | 0.9785                    | 0.9810 | 0.9830 | 0.9848 | 0.9863 | 0.9876 |  |
| 106         | 0.9780                    | 0.9805 | 0.9826 | 0.9844 | 0.9859 | 0.9873 |  |
| 107         | 0.9776                    | 0.9801 | 0.9823 | 0.9841 | 0.9856 | 0.9870 |  |
| 108         | 0.9771                    | 0.9797 | 0.9819 | 0.9837 | 0.9853 | 0.9867 |  |
| 109         | 0.9766                    | 0.9793 | 0.9815 | 0.9834 | 0.9850 | 0.9864 |  |
| 110         | 0.9761                    | 0.9789 | 0.9811 | 0.9831 | 0.9847 | 0.9861 |  |
| 111         | 0.9757                    | 0.9785 | 0.9808 | 0.9828 | 0.9844 | 0.9859 |  |
| 112         | 0.9752                    | 0.9780 | 0.9804 | 0.9824 | 0.9841 | 0.9856 |  |
| 113         | 0.9747                    | 0.9776 | 0.9800 | 0.9821 | 0.9838 | 0.9853 |  |
| 114         | 0.9742                    | 0.9772 | 0.9796 | 0.9817 | 0.9835 | 0.9850 |  |
| 115         | 0.9738                    | 0.9768 | 0.9793 | 0.9814 | 0.9832 | 0.9848 |  |
| 116         | 0.9733                    | 0.9763 | 0.9789 | 0.9810 | 0.9829 | 0.9845 |  |
| 115         | 0.9738                    | 0.9768 | 0.9793 | 0.9814 | 0.9832 |        |  |

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| WYDOT 841.0  |  |  |  |  |
|--------------|--|--|--|--|
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| Femperature   Specific Gravity at 60 °F |        |        |          |        |        |        |
|---|--------|--------|----------|--------|--------|--------|
| <b>Cemperature</b>                      | 0.000  | 0.050  | <u> </u> | ·      | 1 000  | 1.050  |
| ° <b>F</b>                              | 0.800  | 0.850  | 0.900    | 0.950  | 1.000  | 1.050  |
| 118                                     | 0.9723 | 0.9755 | 0.9781   | 0.9804 | 0.9823 | 0.9839 |
| 119                                     | 0.9718 | 0.9751 | 0.9778   | 0.9801 | 0.9820 | 0.9837 |
| 120                                     | 0.9713 | 0.9746 | 0.9774   | 0.9797 | 0.9817 | 0.9834 |
| 121                                     | 0.9709 | 0.9742 | 0.9770   | 0.9794 | 0.9814 | 0.9831 |
| 122                                     | 0.9704 | 0.9738 | 0.9766   | 0.9790 | 0.9811 | 0.9828 |
| 123                                     | 0.9699 | 0.9734 | 0.9763   | 0.9787 | 0.9808 | 0.9826 |
| 124                                     | 0.9694 | 0.9729 | 0.9759   | 0.9783 | 0.9804 | 0.9823 |
| 125                                     | 0.9690 | 0.9725 | 0.9755   | 0.9780 | 0.9801 | 0.9820 |
| 126                                     | 0.9685 | 0.9721 | 0.9751   | 0.9777 | 0.9798 | 0.9817 |
| 127                                     | 0.9680 | 0.9717 | 0.9747   | 0.9774 | 0.9795 | 0.9815 |
| 128                                     | 0.9675 | 0.9712 | 0.9743   | 0.9770 | 0.9792 | 0.9812 |
| 129                                     | 0.9671 | 0.9708 | 0.9740   | 0.9767 | 0.9789 | 0.9809 |
| 130                                     | 0.9666 | 0.9704 | 0.9736   | 0.9763 | 0.9786 | 0.9806 |
| 131                                     | 0.9661 | 0.9700 | 0.9732   | 0.9760 | 0.9783 | 0.9803 |
| 132                                     | 0.9656 | 0.9695 | 0.9728   | 0.9756 | 0.9780 | 0.9800 |
| 133                                     | 0.9652 | 0.9691 | 0.9725   | 0.9753 | 0.9777 | 0.9798 |
| 134                                     | 0.9647 | 0.9687 | 0.9721   | 0.9749 | 0.9774 | 0.9795 |
| 135                                     | 0.9642 | 0.9683 | 0.9717   | 0.9746 | 0.9771 | 0.9792 |
| 136                                     | 0.9637 | 0.9678 | 0.9713   | 0.9743 | 0.9768 | 0.9789 |
| 137                                     | 0.9632 | 0.9674 | 0.9710   | 0.9740 | 0.9765 | 0.9787 |
| 138                                     | 0.9627 | 0.9670 | 0.9706   | 0.9736 | 0.9762 | 0.9784 |
| 139                                     | 0.9623 | 0.9666 | 0.9702   | 0.9733 | 0.9759 | 0.9781 |
| 140                                     | 0.9618 | 0.9662 | 0.9698   | 0.9729 | 0.9756 | 0.9778 |
| 141                                     | 0.9613 | 0.9658 | 0.9695   | 0.9726 | 0.9753 | 0.9776 |
| 142                                     | 0.9608 | 0.9653 | 0.9691   | 0.9722 | 0.9749 | 0.9773 |
| 143                                     | 0.9604 | 0.9649 | 0.9687   | 0.9719 | 0.9746 | 0.9770 |
| 144                                     | 0.9599 | 0.9645 | 0.9683   | 0.9716 | 0.9743 | 0.9767 |
| 145                                     | 0.9594 | 0.9641 | 0.9679   | 0.9713 | 0.9740 | 0.9765 |
| 146                                     | 0.9589 | 0.9636 | 0.9675   | 0.9709 | 0.9737 | 0.9762 |
| 147                                     | 0.9585 | 0.9632 | 0.9672   | 0.9706 | 0.9734 | 0.9759 |
| 148                                     | 0.9580 | 0.9628 | 0.9668   | 0.9702 | 0.9731 | 0.9756 |
| 149                                     | 0.9575 | 0.9624 | 0.9664   | 0.9699 | 0.9728 | 0.9754 |
| 150                                     | 0.9570 | 0.9619 | 0.9660   | 0.9695 | 0.9725 | 0.9751 |
| 151                                     | 0.9565 | 0.9615 | 0.9657   | 0.9692 | 0.9722 | 0.9748 |
| 152                                     | 0.9560 | 0.9611 | 0.9653   | 0.9688 | 0.9719 | 0.9745 |
| 153                                     | 0.9556 | 0.9607 | 0.9649   | 0.9685 | 0.9716 | 0.9742 |
| 154                                     | 0.9551 | 0.9602 | 0.9645   | 0.9682 | 0.9713 | 0.9739 |
| 155                                     | 0.9546 | 0.9598 | 0.9642   | 0.9679 | 0.9710 | 0.9737 |
| 155                                     | 0.9541 | 0.9594 | 0.9638   | 0.9675 | 0.9710 | 0.9734 |

| <b>Femperature</b> | Specific Gravity at 60 °F |        |        |        |        |        |  |  |
|--------------------|---------------------------|--------|--------|--------|--------|--------|--|--|
| ° <b>F</b>         | 0.800                     | 0.850  | 0.900  | 0.950  | 1.000  | 1.050  |  |  |
| 157                | 0.9537                    | 0.9590 | 0.9634 | 0.9672 | 0.9704 | 0.9731 |  |  |
| 158                | 0.9532                    | 0.9585 | 0.9630 | 0.9668 | 0.9700 | 0.9728 |  |  |
| 159                | 0.9527                    | 0.9581 | 0.9627 | 0.9665 | 0.9697 | 0.9726 |  |  |
| 160                | 0.9522                    | 0.9577 | 0.9623 | 0.9661 | 0.9694 | 0.9723 |  |  |
| 161                | 0.9518                    | 0.9573 | 0.9619 | 0.9658 | 0.9691 | 0.9720 |  |  |
| 162                | 0.9513                    | 0.9568 | 0.9615 | 0.9655 | 0.9688 | 0.9717 |  |  |
| 163                | 0.9508                    | 0.9564 | 0.9611 | 0.9652 | 0.9685 | 0.9715 |  |  |
| 164                | 0.9503                    | 0.9560 | 0.9607 | 0.9648 | 0.9682 | 0.9712 |  |  |
| 165                | 0.9498                    | 0.9556 | 0.9604 | 0.9645 | 0.9679 | 0.9709 |  |  |
| 166                | 0.9493                    | 0.9551 | 0.9600 | 0.9641 | 0.9676 | 0.9706 |  |  |
| 167                | 0.9489                    | 0.9547 | 0.9596 | 0.9638 | 0.9673 | 0.9704 |  |  |
| 168                | 0.9484                    | 0.9543 | 0.9592 | 0.9634 | 0.9670 | 0.9701 |  |  |
| 169                | 0.9479                    | 0.9539 | 0.9589 | 0.9631 | 0.9667 | 0.9698 |  |  |
| 170                | 0.9474                    | 0.9534 | 0.9585 | 0.9627 | 0.9664 | 0.9695 |  |  |
| 171                | 0.9470                    | 0.9530 | 0.9581 | 0.9624 | 0.9661 | 0.9692 |  |  |
| 172                | 0.9465                    | 0.9526 | 0.9577 | 0.9621 | 0.9658 | 0.9689 |  |  |
| 173                | 0.9460                    | 0.9522 | 0.9574 | 0.9618 | 0.9655 | 0.9687 |  |  |
| 174                | 0.9455                    | 0.9517 | 0.9570 | 0.9614 | 0.9652 | 0.9684 |  |  |
| 175                | 0.9450                    | 0.9513 | 0.9566 | 0.9611 | 0.9649 | 0.9681 |  |  |
| 176                | 0.9445                    | 0.9509 | 0.9562 | 0.9607 | 0.9645 | 0.9678 |  |  |
| 177                | 0.9441                    | 0.9505 | 0.9558 | 0.9604 | 0.9642 | 0.9676 |  |  |
| 178                | 0.9436                    | 0.9500 | 0.9554 | 0.9600 | 0.9639 | 0.9673 |  |  |
| 179                | 0.9431                    | 0.9496 | 0.9551 | 0.9597 | 0.9636 | 0.9670 |  |  |
| 180                | 0.9426                    | 0.9492 | 0.9547 | 0.9593 | 0.9633 | 0.9667 |  |  |
| 181                | 0.9422                    | 0.9488 | 0.9543 | 0.9590 | 0.9630 | 0.9665 |  |  |
| 182                | 0.9417                    | 0.9483 | 0.9539 | 0.9587 | 0.9627 | 0.9662 |  |  |
| 183                | 0.9412                    | 0.9479 | 0.9536 | 0.9584 | 0.9624 | 0.9659 |  |  |
| 184                | 0.9407                    | 0.9475 | 0.9532 | 0.9580 | 0.9621 | 0.9656 |  |  |
| 185                | 0.9402                    | 0.9471 | 0.9528 | 0.9577 | 0.9618 | 0.9654 |  |  |
| 186                | 0.9397                    | 0.9466 | 0.9524 | 0.9573 | 0.9615 | 0.9651 |  |  |
| 187                | 0.9393                    | 0.9462 | 0.9521 | 0.9570 | 0.9612 | 0.9648 |  |  |
| 188                | 0.9388                    | 0.9458 | 0.9517 | 0.9566 | 0.9609 | 0.9645 |  |  |
| 189                | 0.9383                    | 0.9454 | 0.9513 | 0.9563 | 0.9606 | 0.9643 |  |  |
| 190                | 0.9378                    | 0.9449 | 0.9509 | 0.9559 | 0.9603 | 0.9640 |  |  |
| 191                | 0.9374                    | 0.9445 | 0.9505 | 0.9556 | 0.9600 | 0.9637 |  |  |
| 192                | 0.9369                    | 0.9441 | 0.9501 | 0.9553 | 0.9596 | 0.9634 |  |  |
| 193                | 0.9364                    | 0.9437 | 0.9498 | 0.9550 | 0.9593 | 0.9631 |  |  |
| 194                | 0.9359                    | 0.9432 | 0.9494 | 0.9546 | 0.9590 | 0.9628 |  |  |

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|-------------|--------|--|--|--|
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| <b>CORRECTION FACTORS (to determine volume at 60 °F)</b> |                           |        |        |        |        |        |  |  |
|--|---------------------------|--------|--------|--------|--------|--------|--|--|
| Temperature  | Specific Gravity at 60 °F |        |        |        |        |        |  |  |
| ° <b>F</b>   | 0.800                     | 0.850  | 0.900  | 0.950  | 1.000  | 1.050  |  |  |
| 196  | 0.9349                    | 0.9424 | 0.9486 | 0.9539 | 0.9584 | 0.9623 |  |  |
| 197  | 0.9345                    | 0.9420 | 0.9483 | 0.9536 | 0.9431 | 0.9620 |  |  |
| 198  | 0.9340                    | 0.9415 | 0.9479 | 0.9532 | 0.9278 | 0.9617 |  |  |
| 199  | 0.9335                    | 0.9411 | 0.9475 | 0.9529 | 0.9425 | 0.9615 |  |  |
| 200  | 0.9330                    | 0.9407 | 0.9471 | 0.9526 | 0.9572 | 0.9612 |  |  |
| 201  | 0.9325                    | 0.9403 | 0.9468 | 0.9523 | 0.9569 | 0.9609 |  |  |
| 202  | 0.9320                    | 0.9398 | 0.9464 | 0.9519 | 0.9566 | 0.9606 |  |  |
| 203  | 0.9316                    | 0.9394 | 0.9460 | 0.9516 | 0.9563 | 0.9604 |  |  |
| 204  | 0.9311                    | 0.9390 | 0.9456 | 0.9512 | 0.9560 | 0.9601 |  |  |
| 205  | 0.9306                    | 0.9386 | 0.9452 | 0.9509 | 0.9557 | 0.9598 |  |  |
| 206  | 0.9301                    | 0.9381 | 0.9448 | 0.9505 | 0.9554 | 0.9595 |  |  |
| 207  | 0.9297                    | 0.9377 | 0.9445 | 0.9502 | 0.9551 | 0.9593 |  |  |
| 208  | 0.9292                    | 0.9373 | 0.9441 | 0.9498 | 0.9547 | 0.9590 |  |  |
| 209  | 0.9287                    | 0.9369 | 0.9437 | 0.9495 | 0.9544 | 0.9586 |  |  |
| 210  | 0.9282                    | 0.9364 | 0.9433 | 0.9492 | 0.9541 | 0.9581 |  |  |
| 211  | 0.9277                    | 0.9360 | 0.9430 | 0.9489 | 0.9538 | 0.9580 |  |  |
| 212  | 0.9272                    | 0.9356 | 0.9426 | 0.9485 | 0.9535 | 0.9578 |  |  |
| 213  | 0.9268                    | 0.9352 | 0.9422 | 0.9482 | 0.9532 | 0.9576 |  |  |
| 214  | 0.9263                    | 0.9347 | 0.9418 | 0.9478 | 0.9529 | 0.9573 |  |  |
| 215  | 0.9258                    | 0.9343 | 0.9415 | 0.9475 | 0.9526 | 0.9570 |  |  |
| 216  | 0.9253                    | 0.9339 | 0.9411 | 0.9471 | 0.9523 | 0.9567 |  |  |
| 217  | 0.9248                    | 0.9335 | 0.9407 | 0.9468 | 0.9520 | 0.9565 |  |  |
| 218  | 0.9243                    | 0.9330 | 0.9403 | 0.9464 | 0.9517 | 0.9562 |  |  |
| 219  | 0.9239                    | 0.9326 | 0.9399 | 0.9461 | 0.9514 | 0.9559 |  |  |
| 220  | 0.9234                    | 0.9322 | 0.9395 | 0.9458 | 0.9511 | 0.9556 |  |  |
| 221  | 0.9229                    | 0.9318 | 0.9392 | 0.9455 | 0.9508 | 0.9554 |  |  |
| 222  | 0.9224                    | 0.9313 | 0.9388 | 0.9451 | 0.9504 | 0.9551 |  |  |
| 223  | 0.9220                    | 0.9309 | 0.9384 | 0.9448 | 0.9501 | 0.9548 |  |  |
| 224  | 0.9215                    | 0.9305 | 0.9380 | 0.9444 | 0.9498 | 0.9545 |  |  |
| 225  | 0.9210                    | 0.9301 | 0.9377 | 0.9441 | 0.9495 | 0.9543 |  |  |
| 226  | 0.9205                    | 0.9296 | 0.9373 | 0.9437 | 0.9492 | 0.9540 |  |  |
| 227  | 0.9200                    | 0.9292 | 0.9369 | 0.9434 | 0.9489 | 0.9537 |  |  |
| 228  | 0.9195                    | 0.9288 | 0.9365 | 0.9430 | 0.9486 | 0.9534 |  |  |
| 229  | 0.9191                    | 0.9284 | 0.9361 | 0.9427 | 0.9483 | 0.9531 |  |  |
| 230  | 0.9186                    | 0.9279 | 0.9357 | 0.9424 | 0.9480 | 0.9528 |  |  |
| 231  | 0.9181                    | 0.9275 | 0.9354 | 0.9421 | 0.9477 | 0.9526 |  |  |
| 232  | 0.9176                    | 0.9271 | 0.9350 | 0.9417 | 0.9474 | 0.9523 |  |  |
| 233  | 0.9171                    | 0.9267 | 0.9346 | 0.9414 | 0.9471 | 0.9520 |  |  |
| 234  | 0.9166                    | 0.9262 | 0.9342 | 0.9410 | 0.9468 | 0.9517 |  |  |

| Temperature | Specific Gravity at 60 °F |        |        |        |        |        |  |  |
|-------------|---------------------------|--------|--------|--------|--------|--------|--|--|
| °F          | 0.800                     | 0.850  | 0.900  | 0.950  | 1.000  | 1.050  |  |  |
| 235         | 0.9162                    | 0.9258 | 0.9339 | 0.9407 | 0.9465 | 0.9515 |  |  |
| 236         | 0.9157                    | 0.9254 | 0.9335 | 0.9403 | 0.9461 | 0.9512 |  |  |
| 237         | 0.9152                    | 0.9250 | 0.9331 | 0.9400 | 0.9458 | 0.9509 |  |  |
| 238         | 0.9147                    | 0.9245 | 0.9327 | 0.9396 | 0.9455 | 0.9506 |  |  |
| 239         | 0.9142                    | 0.9241 | 0.9323 | 0.9393 | 0.9452 | 0.9504 |  |  |
| 240         | 0.9137                    | 0.9236 | 0.9319 | 0.9389 | 0.9449 | 0.9501 |  |  |
| 241         | 0.9133                    | 0.9232 | 0.9316 | 0.9386 | 0.9446 | 0.9498 |  |  |
| 242         | 0.9128                    | 0.9228 | 0.9312 | 0.9383 | 0.9443 | 0.9495 |  |  |
| 243         | 0.9123                    | 0.9224 | 0.9308 | 0.9380 | 0.9440 | 0.9492 |  |  |
| 244         | 0.9118                    | 0.9219 | 0.9304 | 0.9376 | 0.9437 | 0.9489 |  |  |
| 245         | 0.9113                    | 0.9215 | 0.9301 | 0.9373 | 0.9434 | 0.9487 |  |  |
| 246         | 0.9108                    | 0.9211 | 0.9297 | 0.9369 | 0.9431 | 0.9484 |  |  |
| 247         | 0.9104                    | 0.9207 | 0.9293 | 0.9366 | 0.9428 | 0.948  |  |  |
| 248         | 0.9099                    | 0.9202 | 0.9289 | 0.9362 | 0.9425 | 0.9478 |  |  |
| 249         | 0.9094                    | 0.9198 | 0.9285 | 0.9359 | 0.9422 | 0.9476 |  |  |
| 250         | 0.9089                    | 0.9194 | 0.9281 | 0.9355 | 0.9419 | 0.9473 |  |  |
| 251         | 0.9084                    | 0.9190 | 0.9278 | 0.9352 | 0.9416 | 0.9470 |  |  |
| 252         | 0.9079                    | 0.9185 | 0.9274 | 0.9349 | 0.9412 | 0.946  |  |  |
| 253         | 0.9075                    | 0.9181 | 0.9270 | 0.9346 | 0.9409 | 0.946  |  |  |
| 254         | 0.9070                    | 0.9177 | 0.9266 | 0.9342 | 0.9406 | 0.9462 |  |  |
| 255         | 0.9065                    | 0.9173 | 0.9263 | 0.9339 | 0.9403 | 0.9459 |  |  |
| 256         | 0.9060                    | 0.9168 | 0.9259 | 0.9335 | 0.9400 | 0.9450 |  |  |
| 257         | 0.9055                    | 0.9164 | 0.9255 | 0.9332 | 0.9397 | 0.9453 |  |  |
| 258         | 0.9050                    | 0.9160 | 0.9251 | 0.9328 | 0.9394 | 0.9450 |  |  |
| 259         | 0.9045                    | 0.9156 | 0.9247 | 0.9325 | 0.9391 | 0.9448 |  |  |
| 260         | 0.9040                    | 0.9151 | 0.9243 | 0.9321 | 0.9388 | 0.944  |  |  |
| 261         | 0.9036                    | 0.9147 | 0.9240 | 0.9318 | 0.9385 | 0.9442 |  |  |
| 262         | 0.9031                    | 0.9142 | 0.9236 | 0.9314 | 0.9382 | 0.9439 |  |  |
| 263         | 0.9026                    | 0.9138 | 0.9232 | 0.9311 | 0.9379 | 0.943  |  |  |
| 264         | 0.9021                    | 0.9134 | 0.9228 | 0.9308 | 0.9375 | 0.9434 |  |  |
| 265         | 0.9016                    | 0.9130 | 0.9224 | 0.9305 | 0.9372 | 0.943  |  |  |
| 266         | 0.9011                    | 0.9125 | 0.9220 | 0.9301 | 0.9369 | 0.9428 |  |  |
| 267         | 0.9007                    | 0.9121 | 0.9217 | 0.9298 | 0.9366 | 0.9426 |  |  |
| 268         | 0.9002                    | 0.9117 | 0.9213 | 0.9294 | 0.9363 | 0.9423 |  |  |
| 269         | 0.8997                    | 0.9113 | 0.9209 | 0.9291 | 0.9360 | 0.9420 |  |  |
| 270         | 0.8992                    | 0.9108 | 0.9205 | 0.9287 | 0.9357 | 0.941  |  |  |
| 271         | 0.8987                    | 0.9104 | 0.9202 | 0.9284 | 0.9354 | 0.9414 |  |  |
| 272         | 0.8982                    | 0.9100 | 0.9198 | 0.9280 | 0.9351 | 0.9411 |  |  |
| 273         | 0.8977                    | 0.9096 | 0.9194 | 0.9277 | 0.9348 | 0.9409 |  |  |

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| <b>CORRECTION FACTORS</b> (to determine volume at 60 °F) |                           |        |        |        |        |        |  |
|--|---------------------------|--------|--------|--------|--------|--------|--|
| Temperature  | Specific Gravity at 60 °F |        |        |        |        |        |  |
| ° <b>F</b>   | 0.800                     | 0.850  | 0.900  | 0.950  | 1.000  | 1.050  |  |
| 274  | 0.8972                    | 0.9091 | 0.9190 | 0.9274 | 0.9345 | 0.9406 |  |
| 275  | 0.8968                    | 0.9087 | 0.9186 | 0.9271 | 0.9342 | 0.9403 |  |
| 276  | 0.8963                    | 0.9082 | 0.9182 | 0.9267 | 0.9339 | 0.9400 |  |
| 277  | 0.8958                    | 0.9078 | 0.9179 | 0.9264 | 0.9336 | 0.9398 |  |
| 278  | 0.8953                    | 0.9074 | 0.9175 | 0.9260 | 0.9332 | 0.9395 |  |
| 279  | 0.8948                    | 0.9070 | 0.9171 | 0.9257 | 0.9329 | 0.9392 |  |
| 280  | 0.8943                    | 0.9065 | 0.9167 | 0.9253 | 0.9326 | 0.9389 |  |
| 281  | 0.8939                    | 0.9061 | 0.9163 | 0.9250 | 0.9323 | 0.9387 |  |
| 282  | 0.8934                    | 0.9057 | 0.9159 | 0.9246 | 0.9320 | 0.9384 |  |
| 283  | 0.8929                    | 0.9053 | 0.9156 | 0.9243 | 0.9317 | 0.9381 |  |
| 284  | 0.8924                    | 0.9048 | 0.9152 | 0.9239 | 0.9314 | 0.9378 |  |
| 285  | 0.8919                    | 0.9044 | 0.9148 | 0.9236 | 0.9311 | 0.9375 |  |
| 286  | 0.8914                    | 0.9040 | 0.9144 | 0.9233 | 0.9308 | 0.9372 |  |
| 287  | 0.8909                    | 0.9036 | 0.9141 | 0.9230 | 0.9305 | 0.9370 |  |
| 288  | 0.8904                    | 0.9031 | 0.9137 | 0.9226 | 0.9302 | 0.9367 |  |
| 289  | 0.8900                    | 0.9027 | 0.9133 | 0.9223 | 0.9299 | 0.9364 |  |
| 290  | 0.8895                    | 0.9022 | 0.9129 | 0.9219 | 0.9295 | 0.9361 |  |
| 291  | 0.8890                    | 0.9018 | 0.9125 | 0.9216 | 0.9292 | 0.9359 |  |
| 292  | 0.8885                    | 0.9014 | 0.9121 | 0.9212 | 0.9289 | 0.9356 |  |
| 293  | 0.8880                    | 0.9010 | 0.9118 | 0.9209 | 0.9286 | 0.9353 |  |
| 294  | 0.8875                    | 0.9005 | 0.9114 | 0.9205 | 0.9283 | 0.9350 |  |
| 295  | 0.8870                    | 0.9001 | 0.9110 | 0.9202 | 0.9280 | 0.9348 |  |
| 296  | 0.8864                    | 0.8997 | 0.9106 | 0.9198 | 0.9277 | 0.9345 |  |
| 297  | 0.8860                    | 0.8993 | 0.9102 | 0.9195 | 0.9274 | 0.9342 |  |
| 298  | 0.8856                    | 0.8988 | 0.9098 | 0.9192 | 0.9271 | 0.9339 |  |
| 299  | 0.8851                    | 0.8984 | 0.9095 | 0.9189 | 0.9268 | 0.9336 |  |
| 300  | 0.8846                    | 0.8979 | 0.9091 | 0.9185 | 0.9265 | 0.9333 |  |
| 301  | 0.8841                    | 0.8975 | 0.9087 | 0.9182 | 0.9262 | 0.9331 |  |
| 302  | 0.8836                    | 0.8971 | 0.9083 | 0.9178 | 0.9258 | 0.9328 |  |
| 303  | 0.8831                    | 0.8967 | 0.9079 | 0.9175 | 0.9255 | 0.9325 |  |
| 304  | 0.8826                    | 0.8962 | 0.9075 | 0.9171 | 0.9252 | 0.9322 |  |
| 305  | 0.8821                    | 0.8958 | 0.9072 | 0.9168 | 0.9249 | 0.9320 |  |
| 306  | 0.8816                    | 0.8953 | 0.9068 | 0.9164 | 0.9246 | 0.9317 |  |
| 307  | 0.8812                    | 0.8949 | 0.9064 | 0.9161 | 0.9243 | 0.9314 |  |
| 308  | 0.8807                    | 0.8945 | 0.9060 | 0.9157 | 0.9240 | 0.9311 |  |
| 309  | 0.8802                    | 0.8941 | 0.9056 | 0.9154 | 0.9237 | 0.9308 |  |
| 310  | 0.8797                    | 0.8936 | 0.9052 | 0.9150 | 0.9234 | 0.9305 |  |
| 311  | 0.8792                    | 0.8932 | 0.9049 | 0.9147 | 0.9231 | 0.9303 |  |
| 312  | 0.8787                    | 0.8928 | 0.9045 | 0.9144 | 0.9228 | 0.9300 |  |

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| Temperature Specific Gravity at 60 °F |        |        |        |        |        |        |
|---------------------------------------|--------|--------|--------|--------|--------|--------|
| °F                                    | 0.800  | 0.850  | 0.900  | 0.950  | 1.000  | 1.050  |
| 313                                   | 0.8782 | 0.8924 | 0.9041 | 0.9141 | 0.9225 | 0.9297 |
| 314                                   | 0.8777 | 0.8919 | 0.9037 | 0.9137 | 0.9221 | 0.9294 |
| 315                                   | 0.8772 | 0.8915 | 0.9033 | 0.9134 | 0.9218 | 0.9292 |
| 316                                   | 0.8767 | 0.8910 | 0.9029 | 0.9130 | 0.9215 | 0.9289 |
| 317                                   | 0.8763 | 0.8906 | 0.9026 | 0.9127 | 0.9212 | 0.9286 |
| 318                                   | 0.8758 | 0.8902 | 0.9022 | 0.9123 | 0.9209 | 0.9283 |
| 319                                   | 0.8753 | 0.8898 | 0.9018 | 0.9120 | 0.9206 | 0.9281 |
| 320                                   | 0.8748 | 0.8893 | 0.9014 | 0.9116 | 0.9203 | 0.9278 |
| 321                                   | 0.8743 | 0.8889 | 0.9010 | 0.9113 | 0.9200 | 0.9275 |
| 322                                   | 0.8738 | 0.8884 | 0.9006 | 0.9109 | 0.9197 | 0.9272 |
| 323                                   | 0.8733 | 0.8880 | 0.9003 | 0.9106 | 0.9194 | 0.9269 |
| 324                                   | 0.8728 | 0.8876 | 0.8999 | 0.9102 | 0.9191 | 0.9266 |
| 325                                   | 0.8723 | 0.8872 | 0.8995 | 0.9099 | 0.9188 | 0.9264 |
| 326                                   | 0.8718 | 0.8867 | 0.8991 | 0.9096 | 0.9184 | 0.9261 |
| 327                                   | 0.8714 | 0.8863 | 0.8987 | 0.9093 | 0.9181 | 0.9258 |
| 328                                   | 0.8709 | 0.8858 | 0.8983 | 0.9089 | 0.9178 | 0.9255 |
| 329                                   | 0.8704 | 0.8854 | 0.8980 | 0.9086 | 0.9175 | 0.9253 |
| 330                                   | 0.8699 | 0.8850 | 0.8976 | 0.9082 | 0.9172 | 0.9250 |
| 331                                   | 0.8694 | 0.8846 | 0.8972 | 0.9079 | 0.9169 | 0.9247 |
| 332                                   | 0.8689 | 0.8841 | 0.8968 | 0.9075 | 0.9166 | 0.9244 |
| 333                                   | 0.8684 | 0.8837 | 0.8964 | 0.9072 | 0.9163 | 0.9241 |
| 334                                   | 0.8679 | 0.8833 | 0.8960 | 0.9068 | 0.9160 | 0.9238 |
| 335                                   | 0.8674 | 0.8829 | 0.8957 | 0.9065 | 0.9157 | 0.9236 |
| 336                                   | 0.8669 | 0.8824 | 0.8953 | 0.9061 | 0.9154 | 0.9233 |
| 337                                   | 0.8664 | 0.8820 | 0.8949 | 0.9058 | 0.9151 | 0.9230 |
| 338                                   | 0.8659 | 0.8815 | 0.8945 | 0.9054 | 0.9147 | 0.9227 |
| 339                                   | 0.8654 | 0.8811 | 0.8941 | 0.9051 | 0.9144 | 0.9225 |
| 340                                   | 0.8649 | 0.8807 | 0.8937 | 0.9047 | 0.9141 | 0.9222 |
| 341                                   | 0.8645 | 0.8803 | 0.8934 | 0.9044 | 0.9138 | 0.9219 |
| 342                                   | 0.8640 | 0.8798 | 0.8930 | 0.9041 | 0.9135 | 0.9216 |
| 343                                   | 0.8635 | 0.8794 | 0.8926 | 0.9038 | 0.9132 | 0.9213 |
| 344                                   | 0.8630 | 0.8789 | 0.8922 | 0.9034 | 0.9129 | 0.9210 |
| 345                                   | 0.8625 | 0.8785 | 0.8918 | 0.9031 | 0.9126 | 0.9208 |
| 346                                   | 0.8620 | 0.8780 | 0.8914 | 0.9027 | 0.9123 | 0.9205 |
| 347                                   | 0.8615 | 0.8776 | 0.8911 | 0.9024 | 0.9120 | 0.9202 |
| 348                                   | 0.8610 | 0.8772 | 0.8907 | 0.9020 | 0.9116 | 0.9199 |
| 349                                   | 0.8605 | 0.8768 | 0.8903 | 0.9017 | 0.9113 | 0.9197 |
| 350                                   | 0.8600 | 0.8763 | 0.8899 | 0.9013 | 0.9110 | 0.9194 |
| 351                                   | 0.8595 | 0.8759 | 0.8895 | 0.9010 | 0.9107 | 0.9191 |

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|             | CORREC | TION FACTO | ORS (to detern | nine volume at | 60 °F) |        |
|-------------|--------|------------|----------------|----------------|--------|--------|
| Temperature |        |            | Specific Gra   | avity at 60 °F |        |        |
| ° <b>F</b>  | 0.800  | 0.850      | 0.900          | 0.950          | 1.000  | 1.050  |
| 352         | 0.8590 | 0.8754     | 0.8891         | 0.9006         | 0.9104 | 0.9188 |
| 353         | 0.8585 | 0.8750     | 0.8887         | 0.9003         | 0.9101 | 0.9185 |
| 354         | 0.8580 | 0.8746     | 0.8883         | 0.8999         | 0.9098 | 0.9182 |
| 355         | 0.8575 | 0.8742     | 0.8880         | 0.8996         | 0.9095 | 0.9180 |
| 356         | 0.8570 | 0.8737     | 0.8876         | 0.8992         | 0.9092 | 0.9177 |
| 357         | 0.8565 | 0.8733     | 0.8872         | 0.8989         | 0.9089 | 0.9174 |
| 358         | 0.8560 | 0.8728     | 0.8868         | 0.8985         | 0.9085 | 0.9171 |
| 359         | 0.8555 | 0.8724     | 0.8864         | 0.8982         | 0.9082 | 0.9169 |
| 360         | 0.8550 | 0.8720     | 0.8860         | 0.8979         | 0.9079 | 0.9166 |
| 361         | 4.6980 | 0.8716     | 0.8857         | 0.8976         | 0.9076 | 0.9163 |
| 362         | 8.5410 | 0.8711     | 0.8853         | 0.8972         | 0.9073 | 0.9160 |
| 363         | 4.6971 | 0.8707     | 0.8849         | 0.8969         | 0.9070 | 0.9157 |
| 364         | 0.8531 | 0.8702     | 0.8845         | 0.8965         | 0.9067 | 0.9154 |
| 365         | 0.8526 | 0.8698     | 0.8841         | 0.8962         | 0.9064 | 0.9152 |
| 366         | 0.8521 | 0.8693     | 0.8837         | 0.8958         | 0.9061 | 0.9149 |
| 367         | 0.8516 | 0.8689     | 0.8833         | 0.8955         | 0.9058 | 0.9146 |
| 368         | 0.8511 | 0.8685     | 0.8829         | 0.8951         | 0.9054 | 0.9143 |
| 369         | 0.8506 | 0.8681     | 0.8826         | 0.8948         | 0.9051 | 0.9141 |
| 370         | 0.8501 | 0.8676     | 0.8822         | 0.8944         | 0.9048 | 0.9138 |
| 371         | 0.8496 | 0.8672     | 0.8818         | 0.8941         | 0.9045 | 0.9135 |
| 372         | 0.8491 | 0.8667     | 0.8814         | 0.8937         | 0.9042 | 0.9132 |
| 372         | 0.8486 | 0.8663     | 0.8810         | 0.8934         | 0.9039 | 0.9129 |
| 374         | 0.8481 | 0.8659     | 0.8806         | 0.8930         | 0.9036 | 0.9126 |
| 375         | 0.8476 | 0.8655     | 0.8802         | 0.8927         | 0.9033 | 0.9124 |
| 376         | 0.8471 | 0.8650     | 0.8798         | 0.8923         | 0.9030 | 0.9121 |
| 377         | 0.8466 | 0.8646     | 0.8795         | 0.8920         | 0.9027 | 0.9118 |
| 378         | 0.8461 | 0.8641     | 0.8791         | 0.8916         | 0.9023 | 0.9115 |
| 379         | 0.8456 | 0.8637     | 0.8787         | 0.8913         | 0.9020 | 0.9112 |
| 380         | 0.8451 | 0.8632     | 0.8783         | 0.8910         | 0.9017 | 0.9109 |
| 381         | 0.8446 | 0.8628     | 0.8779         | 0.8907         | 0.9014 | 0.9107 |
| 382         | 0.8441 | 0.8624     | 0.8775         | 0.8903         | 0.9011 | 0.9104 |
| 383         | 0.8436 | 0.8620     | 0.8771         | 0.8900         | 0.9008 | 0.9101 |
| 384         | 0.8431 | 0.8615     | 0.8767         | 0.8896         | 0.9005 | 0.9098 |
| 385         | 0.8426 | 0.8611     | 0.8764         | 0.8893         | 0.9002 | 0.9096 |
| 386         | 0.8421 | 0.8606     | 0.8760         | 0.8889         | 0.8999 | 0.9093 |
| 387         | 0.8416 | 0.8602     | 0.8756         | 0.8886         | 0.8996 | 0.9090 |
| 388         | 0.8411 | 0.8597     | 0.8752         | 0.8882         | 0.8992 | 0.9087 |
| 389         | 0.8406 | 0.8593     | 0.8748         | 0.8879         | 0.8989 | 0.9084 |
| 390         | 0.8401 | 0.8589     | 0.8744         | 0.8875         | 0.8986 | 0.9081 |

| <b>Femperature</b> |        |        | Specific Gra | avity at 60 °F |        |        |
|--------------------|--------|--------|--------------|----------------|--------|--------|
| °F                 | 0.800  | 0.850  | 0.900        | 0.950          | 1.000  | 1.050  |
| 391                | 0.8396 | 0.8585 | 0.8740       | 0.8872         | 0.8983 | 0.9079 |
| 392                | 0.8391 | 0.8580 | 0.8736       | 0.8868         | 0.8980 | 0.9076 |
| 393                | 0.8386 | 0.8576 | 0.8733       | 0.8865         | 0.8977 | 0.9073 |
| 394                | 0.8381 | 0.8571 | 0.8729       | 0.8861         | 0.8974 | 0.9070 |
| 395                | 0.8376 | 0.8567 | 0.8725       | 0.8858         | 0.8971 | 0.9067 |
| 396                | 0.8371 | 0.8562 | 0.8721       | 0.8854         | 0.8967 | 0.9064 |
| 397                | 0.8366 | 0.8558 | 0.8717       | 0.8851         | 0.8964 | 0.9062 |
| 398                | 0.8361 | 0.8553 | 0.8713       | 0.8847         | 0.8961 | 0.9059 |
| 399                | 0.8356 | 0.8549 | 0.8709       | 0.8844         | 0.8958 | 0.9056 |
| 400                | 0.8351 | 0.8545 | 0.8705       | 0.8840         | 0.8955 | 0.9053 |
| 401                | 0.8346 | 0.8541 | 0.8702       | 0.8837         | 0.8952 | 0.9051 |
| 402                | 0.8341 | 0.8536 | 0.8698       | 0.8833         | 0.8949 | 0.9048 |
| 403                | 0.8336 | 0.8532 | 0.8694       | 0.8830         | 0.8946 | 0.9045 |
| 404                | 0.8331 | 0.8527 | 0.8690       | 0.8827         | 0.8943 | 0.9042 |
| 405                | 0.8326 | 0.8523 | 0.8686       | 0.8824         | 0.8940 | 0.9039 |
| 406                | 0.8321 | 0.8518 | 0.8682       | 0.8820         | 0.8936 | 0.9036 |
| 407                | 0.8316 | 0.8514 | 0.8678       | 0.8817         | 0.8933 | 0.9034 |
| 408                | 0.8311 | 0.8509 | 0.8674       | 0.8813         | 0.8930 | 0.9031 |
| 409                | 0.8306 | 0.8505 | 0.8670       | 0.8810         | 0.8927 | 0.9028 |
| 410                | 0.8301 | 0.8501 | 0.8666       | 0.8806         | 0.8924 | 0.9025 |
| 411                | 0.8296 | 0.8497 | 0.8663       | 0.8803         | 0.8921 | 0.9022 |
| 412                | 0.8290 | 0.8492 | 0.8659       | 0.8799         | 0.8918 | 0.9019 |
| 413                | 0.8285 | 0.8488 | 0.8655       | 0.8796         | 0.8915 | 0.9017 |
| 414                | 0.8280 | 0.8483 | 0.8651       | 0.8792         | 0.8911 | 0.9014 |
| 415                | 0.8275 | 0.8479 | 0.8647       | 0.8789         | 0.8908 | 0.9011 |
| 416                | 0.8270 | 0.8474 | 0.8643       | 0.8785         | 0.8905 | 0.9008 |
| 417                | 0.8265 | 0.8470 | 0.8639       | 0.8782         | 0.8902 | 0.9006 |
| 418                | 0.8260 | 0.8465 | 0.8635       | 0.8778         | 0.8899 | 0.9003 |
| 419                | 0.8255 | 0.8461 | 0.8631       | 0.8775         | 0.8896 | 0.9000 |
| 420                | 0.8250 | 0.8457 | 0.8627       | 0.8771         | 0.8893 | 0.8997 |
| 421                | 0.8245 | 0.8453 | 0.8624       | 0.8768         | 0.8890 | 0.8994 |
| 422                | 0.8240 | 0.8448 | 0.8620       | 0.8764         | 0.8886 | 0.8991 |
| 423                | 0.8235 | 0.8444 | 0.8616       | 0.8761         | 0.8883 | 0.8989 |
| 424                | 0.8230 | 0.8439 | 0.8612       | 0.8757         | 0.8880 | 0.8986 |
| 425                | 0.8225 | 0.8435 | 0.8608       | 0.8754         | 0.8877 | 0.8983 |
| 426                | 0.8220 | 0.8430 | 0.8604       | 0.8750         | 0.8874 | 0.8980 |
| 427                | 0.8215 | 0.8426 | 0.8600       | 0.8747         | 0.8871 | 0.8977 |
| 428                | 0.8209 | 0.8421 | 0.8596       | 0.8743         | 0.8868 | 0.8974 |
| 429                | 0.8204 | 0.8417 | 0.8592       | 0.8740         | 0.8865 | 0.8972 |

| Temperature |        |        | Specific Gra | vity at 60 °F |        |        |
|-------------|--------|--------|--------------|---------------|--------|--------|
| ° <b>F</b>  | 0.800  | 0.850  | 0.900        | 0.950         | 1.000  | 1.050  |
| 430         | 0.8199 | 0.8412 | 0.8588       | 0.8736        | 0.8861 | 0.8969 |
| 431         | 0.8194 | 0.8408 | 0.8585       | 0.8733        | 0.8858 | 0.8966 |
| 432         | 0.8189 | 0.8403 | 0.8581       | 0.8729        | 0.8855 | 0.8963 |
| 433         | 0.8184 | 0.8399 | 0.8577       | 0.8726        | 0.8852 | 0.8960 |
| 434         | 0.8179 | 0.8395 | 0.8573       | 0.8722        | 0.8849 | 0.8957 |
| 435         | 0.8174 | 0.8391 | 0.8569       | 0.8719        | 0.8846 | 0.8955 |
| 436         | 0.8169 | 0.8386 | 0.8565       | 0.8715        | 0.8843 | 0.8952 |
| 437         | 0.8164 | 0.8382 | 0.8561       | 0.8712        | 0.8840 | 0.8949 |
| 438         | 0.8159 | 0.8377 | 0.8557       | 0.8708        | 0.8836 | 0.8946 |

The following formulas are used to calculate the correction factors in the table above:

$$Volume_{Corrected} = Volume_{Measured} \times \frac{1}{\left[\left(\frac{p_{1}^{2} - p_{2}^{2}}{2 \times p_{1} \times p_{2}}\right) + 1\right]}$$

where  $p_1 = Specific Gravity @ 60 °F$ 

and  $p_2 = Specific Gravity @ Temperature_{Measured in °F}$ 

 $= \sqrt{p_1^2 - [0.000611 \times (Temperature_{Measured in °F} - 60 °F)]}$ 

Reference: Perry's Chemical Engineers' Handbook, 6<sup>th</sup> edition, 1984, McGraw – Hill, R660.28P or 660.2

### FIELD SCREEN TEST PROCEDURE FOR EMULSIFIED ASPHALT

- Scope: This method provides a field procedure for determining whether emulsified asphalt has uniform particle size and distribution and does not have deleterious material large enough to plug and/or contaminate equipment (distributor filters, spray nozzles, etc). This procedure is adopted from AASHTO R 66. This procedure is NOT the Sieve Test included in AASHTO T 59.
- Use: This procedure is used to evaluate emulsified asphalt in accordance with *WYDOT* Standard Specifications Section 804.3, and upon delivery for acceptance or rejection of tanker(s) before use per *WYDOT Standard Specifications* Section 113.2.

This test is performed to ensure emulsions are "smooth and homogeneous throughout." The owner of the distributor is responsible for ensuring the emulsion is acceptable for each load of emulsion delivered.

Reference

| Documents: | AASHTO M 140<br>AASHTO M 208<br>AASHTO R 66<br>WYDOT 113.2 | Standard Specification for Emulsified Asphalt<br>Standard Specification for Cationic Emulsified Asphalt<br>Standard Practice for Sampling Asphalt Materials<br>WYDOT Standard Specifications Acceptance of Asphalt<br>Materials |
|------------|--|---|
|            | WYDOT 804.3<br>WYDOT E-224                                 | Waterials<br>WYDOT Standard Specifications Section Emulsified<br>Asphalt<br>Pay Adjustment for Emulsified Asphalt   |
| Apparatus: | 1  | hare screen mesh with <sup>1</sup> / <sub>8</sub> inch square openings hers such as, 5 gallon capacity, etc., for testing and cleanup   |

- 3. Gloves, insulated, vinyl coated, 10 inch gauntlet
- 4. Aluminum 12 inch square pan, 2 inch deep with 8-inch diameter hole centered in bottom of pan
- Precautions: 1. Use gloves for handling the apparatus and hot emulsified asphalt.
  - 2. Ensure the screen mesh is clean and dry before use.

- 3. Do not re-use screen mesh. Emulsified asphalt hardens such that apparatus cannot be cleaned completely to avoid accumulation buildup affecting future testing.
- Procedure: 1. Upon delivery of each load to project, check the temperature of the emulsified asphalt to ensure it complies with appropriate specifications. Place one large container under the sampling valve, open the valve and allow a minimum of two gallons of emulsified asphalt to pour into the five gallon container. This is to ensure that any possible residue is flushed out of the valve/port and only representative material is used during the test.
  - 2. Momentarily close the valve and place another large container under the valve port. Place a clean, unused piece of screen mesh with <sup>1</sup>/<sub>8</sub> inch openings into the square pan and position it under the valve/port. Reopen the valve/port and allow one gallon sample of emulsified asphalt to flow through the piece of screen mesh and hole in pan into the container below and close the valve.
    - Note: If the one gallon sample of emulsified asphalt is obtained through the fill port on the top of the tanker, then the sampling cup/ladle, etc., must be dipped down far enough into the emulsified asphalt to avoid any contamination, such as foam floating at the top of the emulsified asphalt in the tanker.
  - 3. Examine the piece of screen mesh. Emulsion may stick to the screen mesh due to cooling effects. Determine if emulsion is acceptable as follows:
    - a. Using a vinyl coated glove, press down lightly on each particle on the screen mesh to distinguish between bubbles and 'true sieve particles' versus other solid contaminants (DO NOT force particles through the screen mesh).

'True sieve particles' appear as round beads (bb's) and are an agglomeration of the dispersed phase of emulsion (see picture below showing emulsion particle size distribution viewed under a microscope). AASHTO specifications allow 0.1 percent by weight maximum of sieve particles (larger than 0.85 millimeter in size). Sieve particles, when pressed down lightly, will flatten out smoothly on the screen or push through because they are soft and pliable.

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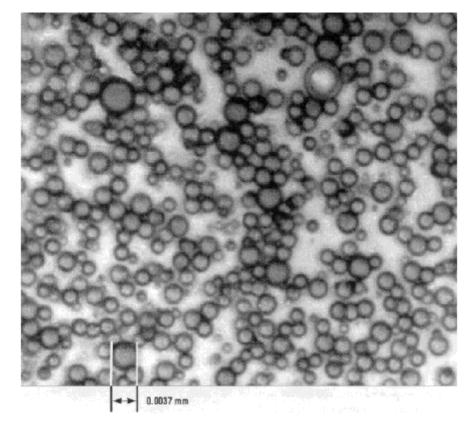


Figure 2.6-1 Relative Sizes and Distribution of Asphalt Particles in an Emulsion

- b. Are solid contaminants retained on the screen mesh? These would include irregular shaped particles of un-milled or un-dissolved polymer, rigid asphalt coke or chunks, heavy/thick skin/films of latex, melted rubber, etc.
  - 1. NO Accept emulsified asphalt
  - 2. YES RETEST by repeating Steps 1, 2, & 3 above.
    - Retest: a. NO Accept b. YES - REJECT
- 4. Pour all unused emulsified asphalt back into the tanker during and after testing. Discard used screen mesh after one use.
- 5. Dispose of all waste in appropriate manner. Clean asphalt from square pan.
- 6. Report test result (Accept or Reject) on Form E-224 (see attached).

# Form E-224 (Rev. 10-17) Sheet WYOMING DEPARTMENT OF TRANSPORTATION PAY ADJUSTMENT FOR EMULSIFIED ASPHALT

| Signatures                         | Computed By: Technician's Name | Checked By: Technician's Name      | Engineer: Engineer's Name        |
|------------------------------------|--------------------------------|------------------------------------|----------------------------------|
| Project Number: ERP Project Number | Project Name: Name of Project  | Resident Engineer: Engineer's Name | Engineer's Town: Engineer's Town |

|          |            | Refinery Acceptance Sample         | tance Sample | FIELD        | TRUD      | (1)                | (2)      | (2)       | (4)                       | (2)                             | PAY  |                              |
|----------|------------|------------------------------------|--------------|--------------|-----------|--------------------|----------|-----------|---------------------------|---------------------------------|--|------------------------------|
| DATE     | ASPHALT    |                                    |              | SCREEN       | CHECK     |                    | Quantity |           | CONTRACTOR'S PERCENT ADJ. | PERCENT ADJ.                    | ADJUSTMENT   | REMARKS                      |
| RCEIVED  | TYPE/GRADE | RECEIVED TYPE/GRADE BILL OF-LADING | *            | Accept       | SAMPLE    | TONS               | TONS     | NET       | COST                      | (see Lab                        | (3) x (4) x  |                              |
|          |            | NUMBER                             | REPORT       | or<br>Reject | (FCS-EA#) | RECEIVED           | ¥0ID     | (1) - (2) | (F.O.H. Refmer y)         | Test Report)                    | $1 - 1 \times \{ (5) / 100 \} \}$  |                              |
| C5/01/18 | CSS-1      | 5-0340*2                           | 16-029       | Accept       |           | E.74C              |          | 6 740     | \$,46.00                  | 000                             | \$0.00   | Transferred from =1±1018     |
| 16/07/16 | CSE-1      | 5334262                            | 16-143       | Accept       |           | 21.880             |          | 21.880    | \$*46.00                  | 6.30                            | (216372)   | No refnery sample to Lab     |
| C5/2C/18 | CSS-1H     | 5334437                            | 16-016       | Accept       |           | 24,290             |          | 24.290    | \$:46.00                  | 000                             | \$0.00   |                              |
| C5/27/4B | CRS-2      | 5134538                            | 18-025       | Accept       |           | 34,930             | 1E.740   | 24.190    | \$^46.00                  | C.30                            | \$0.00   | Void and used for county joo |
| C5/3C/16 | CR5-2      | 5334626                            | 16-028       | Accept       |           | 40,130             |          | 4C.13C    | \$ 46,00                  | 00101                           | (\$585.90)   |                              |
| C6/02/18 | CR5-2      | 5334582                            |              | Reject       |           |                    |          |           | \$*46.00                  | C.30                            |  |                              |
| C6/04/16 | CR5-2      | \$134775                           |              | Reject       |           |                    |          |           | \$*46.00                  | C.30                            |  |                              |
| 005/16   | CRS-2      | 5334654                            | 16-052       | Accept       | F         | 36.720             |          | 3£.72C    | \$*46.00                  | 000                             | \$0.00   |                              |
| C6/0E/1B | CRS-2      | 5335162                            | 16-059       | Accept       | 54        | 13,860             |          | 15.860    | \$* 46,00                 | (C.3)                           | \$0.00   |                              |
| C7/14/16 | CRS-2      | 5336981                            | 16-162       | Accept       |           | 34.310             |          | 34.310    | \$ 46.00                  | 25.00                           | (\$1,25232)  |                              |
| C7/15/18 | CRS-2      | 5136982                            |              | Reject       |           |                    |          |           | \$'46.00                  | 0.0                             |  |                              |
| C7/17/16 | CRS-2      | 5337100                            | 16-242       | Accept       |           | 40.530             |          | 40,530    | \$ 46.00                  | 1<br>1<br>1<br>1                | (\$ 295.87)  | No refinery sample to Lab    |
| C7/2E/18 | C3S-2P     | 5 337831                           | 16-201       | Accept       |           | 24.760             |          | 24.760    | \$1, 90,00                | C.30                            | \$0.0C   |                              |
| C8/01/16 | CRS-2P     | 5.137928                           |              | Accept.      |           | 37.720             |          | 37.72C    | \$~ 90.00                 | 000                             | \$0.00   | Vvaiding for ab report       |
| C8/01/16 | C35-2P     | 5 337929                           |              | Reject       | 5 = 10    |                    |          |           | \$`30,00                  | C.30                            |  |                              |
| C8/04/16 | C3S-2P     | 5 33 60 4 4                        |              | Accept       |           | 35.780             |          | 36.780    | \$. 90.00                 | C.30                            | \$0.0C   | Waiting for ab report        |
| C8/05/16 | HFRS-2P    | 2335587                            |              | Reject       |           |                    |          |           | \$225,00                  | 00'0                            |  |                              |
| CB/IC/IB | HFRS-2P    | 5135372                            |              | Accept       | 9         | 23.940             |          | 25.94C    | \$225.00                  | C.0                             | \$0.0C   | Vvaiting for abireport       |
|          |            |                                    |              |              |           | Colored allowed as | Part and | · The way |                           | and the second of the second of | State of the second sec |                              |

\*\*If no test report has been received in the field from the Laboratory within approximately 60 days after receiving a load of material, send a legible copy of the Bill-Of-Lading to the Laboratory with a memorandum requesting the status of the test.

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Date: XX/XX/XX Date: XX/XX/XX Date: XX/XX/XX

### CHIP SEAL AGGREGATE / EMULSION COMPATIBILITY TEST

Scope: This procedure describes the method for determining compatibility of aggregate and emulsified asphalt for chip seals and establishes information to report prior to sealing operations. Compatibility is defined as the ability of aggregate to allow sufficient coating by emulsion residue and resist coating loss from adverse water exposure.

Ensure laboratories performing compatibility testing meet requirements of *WYDOT Standard Specifications* for applicable AASHTO test methods.

Use: Contractor performs compatibility testing prior to sealing operations. Submit test data on WYDOT Form T-180 to Resident Engineer (see blank form this section).

# Apparatus: 1. Containers for mixing, having rounded corners, such as seamless tin cans, with capacity to easily hold 100 grams of aggregate.

- 2. Balance, with minimum capacity of 95 grams, accurate to 0.1 gram.
- 3. Spatula, steel, with stiff blade approximately 25 mm wide by 100 mm long.
- 4. Beaker, glass, 800 milliliter (mL).
  - Piece of aluminum window screen, cut in circle to match bottom, inside diameter of 800 mL beaker.
- 6. Heat source, either hot plate or Bunsen burner, capable of maintaining 200  $^{\circ}F \pm 10 \ ^{\circ}F$ .
- 7. Thermometer, stem, range 180 °F to 220 °F.
- 8. Brown Kraft paper, 50 lb weight, square sheet; 12 inch x 12 inch, 18 inch x 18 inch

### Reference

5.

| AASHTO R 66<br>AASHTO T 2 | Standard Practice for Sampling Asphalt Materials<br>Sampling of Aggregates   |
|---------------------------|--|
| AASHTO T 11               | Materials Finer than 75 $\mu$ m (No. 200) Sieve in Mineral   |
|                           | Aggregate  |
| AASHTO T 27               | Sieve Analysis of Fine and Coarse Aggregates   |
| AASHTO T 59               | Testing Emulsified Asphalts  |
| WYDOT 409                 | WYDOT Standard Specifications  |
| WYDOT 803.1               | WYDOT Standard Specifications  |
| WYDOT 803.8               | WYDOT Standard Specifications  |
| WYDOT 803.9               | WYDOT Standard Specifications  |
| WYDOT 804.1               | WYDOT Standard Specifications  |
| WYDOT 804.3               | WYDOT Standard Specifications  |
| WYDOT 814.1.1             | WYDOT Standard Specifications  |
| WYDOT T-180               | Chip Seal Aggregate / Emulsion Compatibility Test  |
|                           | AASHTO T 2<br>AASHTO T 11<br>AASHTO T 27<br>AASHTO T 59<br>WYDOT 409<br>WYDOT 803.1<br>WYDOT 803.8<br>WYDOT 803.9<br>WYDOT 804.1<br>WYDOT 804.3<br>WYDOT 814.1.1 |

- Procedure: 1. Obtain approximately  $100 \pm 5$  grams of clean, oven-dried (no surface moisture) aggregate as required by project specifications. For example, if project requires gradation Type B for chip seal aggregate, obtain aggregate sample from project source(s) that is well-graded from coarse to fine in accordance with Table 803.8-1, Gradation Requirements: Chip Seal, 2010 *WYDOT Standard Specifications*.
  - 2. Obtain emulsion of same type as required by project specifications; thoroughly heat emulsion to  $140 \pm 5$  °F; stir for 5 minutes or until uniform in consistency.
  - 3. Weigh  $100 \pm 5$  grams of aggregate into a clean mixing container; record weight as aggregate, **A**, in grams, on Form T-180.
  - 4. Add 1% water to aggregate (by weight of dry aggregate); mix until water is absorbed; record weight as water, **W**, in grams, on Form T-180.
  - 5. Determine quantity of emulsion to add to aggregate to achieve blend of 7% emulsion with 93% aggregate using the following equation:

 $E_{7\%} = (A \div 0.93) - A$ 

Where:  $\mathbf{A}$  = Aggregate dry weight, grams (Step 3)  $\mathbf{E}_{7\%}$  = Emulsion weight (7% blend), grams

- 6. Add calculated quantity of emulsion (Step 5) to aggregate; thoroughly and vigorously mix/blend emulsion and aggregate to maximize coating of aggregate, but not more than 5 minutes  $\pm$  15 seconds.
- 7. After completely mixing aggregate and emulsion, empty container onto 18 inch x 18 inch square sheet of brown Kraft paper; spread out sample so all coated aggregate surfaces are clearly visible.
- 8. Let coated aggregate cure at room temperature (60  $^{\circ}$ F to 80  $^{\circ}$ F) for 24 hours.
- 9. Measure gross weight of coated aggregate & sheet (nearest gram); record as aggregate weight before boiling,  $A_B$ , on Form T-180; visually estimate percent coating (nearest 5%).
- 10. Record as percent coating before boiling,  $P_B(1)$ , on Form T-180 (the digit 1 denotes 1% water added to aggregate before emulsion coating).

- 11. If  $P_B(1) \ge 85\%$ , proceed with boiling sample (Step 14); otherwise obtain new aggregate sample (per Step 1), repeat Steps 2 through 9 *except add* 2% *water* (*Step 4*).
- 12. Record percent coating before boiling as,  $P_B(2)$ , on Form T-180 (the digit 2 denotes 2% water added to aggregate before emulsion coating).
- 13. If  $P_B(2) \ge 85\%$ , proceed with boiling sample (Step 14); otherwise record aggregate/emulsion combination as "Not Compatible" on Form T-180.
- 14. Place circular piece of aluminum window screen on bottom of 800 mL beaker to serve as a spacer to allow boiling water to contact full surface area of all coated aggregates (including surfaces at bottom of beaker).
- 15. Add 600 mL of water into beaker.
- 16. Determine "mild boil" temperature,  $T_B$ , for water using the following equation (elevation adjusted):

 $\mathbf{T}_{\mathbf{B}} = (-0.002 \text{ x } \mathbf{E}) + 205.1$ 

Where:  $T_B$  = Temperature, nearest degree F E = Elevation of lab above sea level, nearest 10 feet

- 17. Heat water in beaker to temperature  $T_B \pm 5$  °F (from Step 16); verify temperature using stem thermometer inserted into water while heating.
- 18. Add entire coated aggregate sample (Step 9) to boiling water in beaker; measure weight of used 18 inch x 18 inch sample sheet and residue (nearest gram); record as sample sheet & residue weight before boiling,  $S_B$ , on Form T-180.
- 19. Adjust/add heat to achieve  $T_B \pm 5$  °F again (verify using stem thermometer); record as temperature of water,  $T_W$ , on Form T-180; leave coated aggregate sample in boiling water for 5 minutes  $\pm$  15 seconds; record boiling time as,  $B_T$ , on Form T-180.
- 20. Drain water from beaker; let coated aggregate cool to room temperature (60 °F to 80 °F); measure weight of clean 12 inch x 12 inch square sheet of brown Kraft paper; record as sample sheet weight after boiling,  $S_A$ , on Form T-180; empty beaker contents onto sample sheet; spread out sample so all coated aggregate surfaces are clearly visible.

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- 21. Measure gross weight of coated aggregate & sheet (nearest gram); record as aggregate weight after boiling,  $A_A$ , on Form T-180; visually estimate percent coating (nearest 5%).
- 22. Record as percent coating after boiling,  $P_A(x)$ , on Form T-180 (where digit x denotes percent water added to aggregate before emulsion coating).
- 23. Determine percent coating retained after boiling,  $P_R(x)$ , using the following equation:

$$P_{R}(x) = (P_{A}(x) \div P_{B}(x)) \times 100\%$$

Where:

- **x** = percent water added to aggregate to achieve 85% minimum emulsion coating before boiling
- $\mathbf{P}_{\mathbf{R}}(\mathbf{x})$  = Percent coating retained after boiling, nearest 1%
- $P_A(x)$  = Percent coating after boiling, nearest 5%
- $P_B(x)$  = Percent coating before boiling, nearest 5%
- 24. Record percent coating retained after boiling as,  $P_R(x)$ , on Form T-180.
- 25. If  $P_R(x) \ge 80\%$ , record aggregate/emulsion combination as "Compatible" on Form T-180; if  $P_R(x) < 80\%$ , record aggregate/emulsion combination as "Not Compatible" on Form T-180.
- General: Provide materials for aggregate/emulsion combination(s) as follows:
  - Aggregate– Conform to requirements of Subsection 803.1, General; 803.8, Aggregate for Chip Seal, and Subsection 803.9, Aggregate for Blotter.

Emulsified Asphalt– Conform to requirements of Subsection 804.3, Emulsified Asphalt.

- Water Conform to requirements of Subsection 814.1.1, General.
- Report: All test information on WYDOT Form T-180 (see blank form this section) including the following:

Aggregate;

Source location (e.g., Granite Canyon Quarry, Underpass Pit, etc) Gradation type (B, C, D, E, K, or S) Gradation data (% Passing, sieve size) Dry sample weight, A Weight (coated) before boiling,  $A_B$ Weight, sample sheet & residue, before boiling,  $S_B$ Weight, sample sheet, after boiling,  $S_A$ Weight (coated) after boiling,  $A_A$ 

Coating (emulsion residue); Percent before boiling, P<sub>B</sub> Percent after boiling, P<sub>A</sub> Percent retained after boiling, P<sub>R</sub>

Water;

Source location (e.g., City of Cheyenne, etc) Weight added to aggregate (1%, 2%), W Temperature (boiling, elevation adjusted), T<sub>B</sub> Temperature (boiling water), T<sub>W</sub> Boiling time, B<sub>T</sub>

Emulsified Asphalt;

Emulsion supplier Emulsion type/grade (e.g., CRS-2P) Modifier type (latex, solid) Blend sample weight, E<sub>7%</sub>

Aggregate/Emulsion Compatibility Aggregate moisture, % (to achieve 85% coating before boiling and 80% coating retained after boiling)

#### Contractor will:

Provide all information required by Form T-180 to laboratory (e.g., emulsion supplier) performing compatibility testing. This information includes WYDOT project number, project location, name of WYDOT resident engineer, name of aggregate source, aggregate sample gradation type and data, date when aggregate was sampled, company that tested and graded the aggregate, contractor name, address, name of contact, and phone number.

Testing Laboratory will:

Perform compatibility testing, record all data on Form T-180, sign, print name, and date the completed Form T-180 at bottom right, and submit to contractor for their review, signature, printed name and date (bottom left).

Contractor must submit completed, signed and dated Form T-180 to WYDOT Resident Engineer at least three working days prior to chip sealing operations.

T-180 (Rev: 09-16)



#### WYOMING DEPARTMENT OF TRANSPORTATION CHIP SEAL AGGREGATE / EMULSION COMPATIBILITY TEST

| Project No(s).:                  | ERP Project Number         | Contractor Name:   | Company Name                            |
|----------------------------------|----------------------------|--------------------|---|
| Project Location(s):             | On The Plans               | Street/PO Address: | Company address                         |
| Resident Engineer.               | Resident Engineer Nome     | City, State Zip:   | >>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>>> |
| Aggregate Source (quarry, pit,)  | : Pit or Quarry Name       | Contact Name:      | Joe President                           |
| Aggregate Gradation Type (B, C   | , D, E, K or S): Per plans | Phone:             | ###-###-####                            |
| Aggregate Sampled (Date)         | MM/DD/YR                   | Testing Lab Name:  | Company Name                            |
| Aggregate Tested & Graded by     | Company Name               | Street/PO Address: | Address                                 |
| Water Source (City of Cheyenne,) | Name of Water source       | City, State Zip:   | City                                    |
| Emulsion Type/Grade (CRS-2P,)    | Per Plans                  | Contact Name:      | Joe Tester                              |
| Emulsion Modifier (latex, solid) | Per plans                  | Phone:             | ###-###-####                            |
|                                  |                            | Lab Elevation      | (nearest 10 feet): 6830                 |

| Test Property   | Aggregate                | Sample                   |   |  |  |
|---|--------------------------|--------------------------|---|--|--|
| Aggregate Gradation   | Add 1% water             | Add 2% water             | Comments                                      |  |  |
| Sieve Size (Subsection 803.8)   | % Pase                   | sing                     |   |  |  |
| 1 inch  |                          | 89                       | · · · · · · · · · · · · · · · · · · ·         |  |  |
| % inch  |                          |                          | 5.0   |  |  |
| ½ inch  | 100                      | 100                      |   |  |  |
| % inch  | 94                       | 92                       | 3/8 " Max Nominal max.                        |  |  |
| No. 4   | 7                        | 5                        |   |  |  |
| No. 8   | 4                        | 3                        | /   |  |  |
| No. 200   | 1                        | 1                        |   |  |  |
| Total Aggregate Dry Weight, A   | 101 grams                | 104 grams                |   |  |  |
| Water weight, W   | 1 grams                  | 2 grams                  | = [ A ÷ 100 ] x ( % water ), nearest gram     |  |  |
| Emulsion weight (blend 7:93), E <sub>7%</sub>                           | 8 grams                  | 8 grams                  | = [ A ÷ 0.93 ] - A, nearest gram              |  |  |
| Weight (coated) before boiling, ${\rm A}_{\rm B}$                       | 124 grams                | 126 grams                | coated aggregate & sheet, nearest gram        |  |  |
| Estimated coating before boiling, $P_{\rm B}(x)$                        | 80 %, P <sub>B</sub> (1) | 90 %, P <sub>B</sub> (2) | Visual estimate, nearest 5%                   |  |  |
| Minimum coating before boiling<br>( Is P <sub>B</sub> (x) ≥ 85% ? )     | Not Compatible           | YES                      | Minimum 85% required                          |  |  |
| Temperature (boiling, elev. adjusted), ${\rm T_{\rm B}}$                | 191                      | ۴                        | = [-0.002 x Elev. ] + 205.1, nearest °F       |  |  |
| Weight, sheet & residue, before boiling, $\mathbf{S}_{\mathrm{B}}$      | grams                    | 20 grams                 | 18" x 18" sheet & residue, nearest gram       |  |  |
| Temperature (water), T <sub>w</sub>                                     | °F                       | 193 °F                   | T <sub>B</sub> ±5 °F required                 |  |  |
| Boiling time, B <sub>T</sub>  | (min : sec)              | 5:03 (min : sec)         | 5 minutes ±15 seconds required                |  |  |
| Weight, sheet, after boiling, $S_{\rm A}$                               | grams                    | 7 grams                  | 12" x 12" sheet (clean), nearest gram         |  |  |
| Weight (coated) after boiling, $A_{\!\scriptscriptstyle A}$             | grams                    | 115 grams                | coated aggregate & sheet, nearest gram        |  |  |
| Estimated coating after boiling, $P_A(x)$                               | %, P <sub>A</sub> (1)    | 80 %, P <sub>A</sub> (2) | Visual estimate, nearest 5%                   |  |  |
| Coating retained after boiling, $P_{\rm R}(x)$                          | %, P <sub>R</sub> (1)    | 89 %, P <sub>R</sub> (2) | = [ $P_A(x) \div P_B(x)$ ] x 100%, nearest 1% |  |  |
| Aggregate / Emulsion Compatibility<br>( Is P <sub>R</sub> (x) ≥ 80% ? ) |                          | YES                      | Minimum 80% required                          |  |  |

Reviewed By (Contractor Representative):

Tested By (Laboratory Representative):

Signature: Frint Name:

Date:

Print Name: Date:

Signature:

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#### FIELD PROCEDURE FOR SAMPLING HOT POURED ELASTIC SEALANT AND HOT POURED CRACK SURFACING

- Scope: Submit samples to the Materials Program according to the requirements described below for all hot-poured elastic sealant and hot-poured crack surfacing (each different type or grade) supplied for road construction or maintenance projects. Referenced Forms with example data follow in this section.
  - Note: DO NOT submit samples (only certifications) as per *WYDOT Standard Specifications* 403.4.5.1 if material is incidental to other bid items or project quantity is equal to or less than the following;

Hot Poured Elastic Sealant - 180,000 ft, 450 ft<sup>3</sup>, 45,000 lb Hot Poured Crack Surfacing - 450 ft<sup>3</sup>

- Use: Applicable to obtaining and submitting hot poured elastic sealant and hot poured crack surfacing samples as per *WYDOT Standard Specifications* 403.4.5.2 or applicable supplementary specifications.
- Apparatus: 1. Sample Containers Silicon release coated (lined) boxes, furnished by the contractor. Fold sides together properly so silicon release coating forms the inside of box.
  - a. For elastic sealant; use 5 lb boxes
  - b. For crack surfacing; use 15 lb boxes
  - 2. Heat resistant gloves (sample temperatures exceed 150 °F)
  - 3. Tape packing or strap

| Documents: | WYDOT 403.4.5.1 | WYDOT Standard Specifications                         |
|------------|-----------------|---|
|            | WYDOT 403.4.5.2 | WYDOT Standard Specifications                         |
|            | WYDOT E-222     | Pay Adjustment for Hot Poured Elastic Sealant         |
|            | WYDOT E-225     | Pay Adjustment for Hot Poured Crack Surfacing         |
|            | WYDOT T-122     | Sample Transmittal Hot Poured Elastic Sealant / Crack |
|            |                 | Sealant   |
|            | WYDOT T-128     | Construction Test Requirements                        |

#### WYDOT 870.0 (Rev. 10-17) Samples: Each sample requires the following documentation:

- 1. Sample Transmittal Form T-122, "Hot Poured Elastic Sealant/Crack Surfacing"
- 2. Weigh ticket/information (production run, batch or lot number, etc.)
- 3. Certificate of Compliance (COC)
- 4. Bill of Lading (BOL) or shipping manifest

Note: BOL must include all appropriate information.

Procedures: The WYDOT inspector will observe sampling. If anything is questionable, record in field diary.

The WYDOT inspector will include documentation noted above for all cartons, pallets, etc. Submit documentation when not sampled.

Wait until each lot is complete before submitting samples and documentation to the Materials Program. A 'standard' lot is three sublots, but may have five sublots maximum depending on circumstances. When 'partial' lots (two samples or less) occur, submit 'as-is' for testing (lots have minimum of 3 sublots).

- 1. Hot-Poured Elastic Sealant
  - a. Sample 10 lb; use two 5 lb containers
  - b. Point of Acceptance the contractor, in the presence of WYDOT representative, will obtain the sample directly from the <u>applicator</u> <u>nozzle during installation of the sealant</u>. Take the random sample any time during sealing operations after initial startup. Allow the equipment to stabilize for temperature and agitation/mixing.
  - c. Frequency one sample per sublot as follows:
    - 1. length 120,000 ft
    - 2. volume-  $300 \text{ ft}^3$
    - 3. mass 30,000 lb per sublot
  - d. Identification
    - 1. Identify hot-poured elastic sealant samples using designation from Form T-128 (Q-HPES) and number them in the order they are obtained. Example: Q-HPES #1, Q-HPES #2, Q-HPES #3, etc.
    - 2. The WYDOT inspector will mark both sample boxes with the Lot and Sublot numbers and tape them together. Example: Lot 1- Sublot 2 is L1-SL2, etc.

- 3. The WYDOT inspector will include required Form T-122 and any other information with each sample and comments, if any, about sampling. Only one set of documentation is required for each pair of boxes. Maintain proper chain-ofcustody (i.e., the correct pair of boxes with the correct documentation) prior to shipment to the Materials Program.
- e. Other record receipt, payment, etc., information on Form E-222
- 2. Hot-Poured Crack Surfacing
  - a. Sample 30 lb; use two 15 lb containers
  - b. Point of Acceptance the contractor, in the presence of WYDOT representative, will obtain the sample directly from the <u>melter-applicator machine discharge chute during installation of the surfacing material</u>. Take the random sample any time during surfacing operations after initial startup (allow equipment to stabilize for temperature and agitation/mixing).
  - c. Frequency one sample per  $300 \text{ ft}^3$ . This represents one sublot for one lot
  - d. Identification
    - 1. The WYDOT inspector will identify hot-poured crack surfacing samples using designation from Form T-128 (Q-HPCS) and number them in the order they are obtained. Example: Q-HPCS #1, Q-HPCS #2, Q-HPCS #3, etc.
    - 2. The WYDOT inspector will mark both sample boxes with the Lot and Sublot numbers and tape them together. Example: Lot 1- Sublot 2 is L1-SL2, etc.
    - 3. The WYDOT inspector will include required Form T-122 and any other information with each sample and comments, if any, about sampling. Only one set of documentation is required for each pair of boxes. Maintain proper chain-ofcustody (i.e., the correct pair of boxes with the correct documentation) prior to shipment to the Materials Program.
  - e. Other record receipt, payment, etc., information on Form E-225



#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY SAMPLE TRANSMITTAL CRACK SEALANT / CRACK SURFACING

| LAB USE ONLY:  |
|--|
| LAB NO:  |
| DATE RECEIVED:   |
| Project No.(s): ERP Project Number   |
| Engineer: Resident Engineer City: Engineer City State: WY                        |
| Sampled Date: MM/DD/YY   |
| Source (Manufacturer/Supplier): Manufactures Name City: Mfgr's City State: ST    |
| AASHTO Type: M-324 Type I: M-324 Type IV: Other:                                 |
| Quantity Represented: Weight:(LB) Length:(FT) Volume:(CF)                        |
| Manufacturer's Production Run/Batch/Lot #s: <u>As Required</u>                   |
| Check Sample, Field #s: As Required  |
| WYDOT Lot #: Lot # Sublot #: <u>#</u> of <u>#</u> Total                          |
| ALL SAMPLES SHALL BE OBTAINED FROM THE APPLICATOR NOZZLE UNLESS NOTED OTHERWISE. |
| Remarks:   |
|  |
|  |
|  |
|  |
|  |
|  |
| Submitted By: Field Sampler  |

| Form E-222<br>(Rev. 10-17)   | Sheet 1<br>of 1           |  | Date: XX/XX/XX<br>Date: XX/XX/XX       |                        |                      | Check If Final Report | ]          |                                | TMENT                           | (13) x (4) x (Weather, Kettle<br>temperature, etc.) |                       |                 | 2.6/ 40 (Air) 350 (Kettle)<br>2.85 45° (Air) 350° (Kettle) |              |          | (\$80.39) 45° (Air) 360° (Kettle) | Т            |              | (\$104.73) 45° (Air) 360° (Kettle) | (\$102.25) 45° (Air) 360° (Kettle) |          |          |          |            |          |          | (\$59.32) 45° (Air) 360° (Kettle) | (\$297.49)  |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
|--|---------------------------|--|--|------------------------|----------------------|-----------------------|------------|--------------------------------|---------------------------------|---|-----------------------|-----------------|--|--------------|----------|-----------------------------------|--------------|--------------|------------------------------------|------------------------------------|----------|----------|----------|------------|----------|----------|-----------------------------------|-------------|--------|---|---|--|--|--|---|---|---|---|---|---|---|---|------------|--|
|  | F                         |  | r ar                                   | T                      |                      | ume                   |            | PAY                            |                                 | ( [3] X   | - fel 1               | \$166.37        | \$130.65   | \$174.66     | (\$85    | 985)<br>(\$                       | (\$83        | (\$43        | (\$10-                             | (\$102                             | (\$97    | (\$61    | (\$106   | (\$112.13) | (\$102   | (\$54    |                                   |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| <b>TION</b>  | EALA                      |  |  |                        |                      | O volume              |            | (2)                            | CONTRACT PAY FACTOR             | (see Lab<br>Benorf)                                 | (Tropan               | 103             | 103  | 103          | 0.98     | 0.98                              | 0.98<br>0.98 | 86:0         | 0.98                               | 0.98                               | 0.98     | 0.98     | 0.98     | 0.98       | 0.98     | 86.0     | 0.98                              | SHEET TOTAL |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| ORTA   | STIC S                    |  |  |                        |                      | • Mass                | CHOOSE ONE | (4)                            | CONTRACT                        | PRICE   | (e) .                 | \$0.65<br>** :- | \$0.65   | \$0.65       | \$0.65   | \$0.65                            | \$0.65       | \$0.65       | \$0.65                             | \$0.65                             | \$0.65   | \$0.65   | \$0.65   | \$0.65     | \$0.65   | \$0.65   | \$0.65                            | HS          |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| YOMING DEPARTMENT OF TRANSPORTATION<br>PAY ADJUSTMENT FOR HOT POURED ELASTIC SEALANT |                           |  |  |                        |                      |                       | -F         |                                | (2)                             | птү   | NET MASS<br>(1) - (2) | 9               | 8532   | 01/9<br>01/9 | 8957     | 6583                              | 6184         | 0/01<br>6456 | 3374                               | 8056                               | 7865     | 7492     | 4736     | 8356       | 8625     | 7866     | 4218                              | 4563        | 119621 |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| F TF   | POUF                      |  |  |                        |                      | Otength               |            | (Z)                            | FIELD QUANTITY                  | diov<br>diov  | 1                     |                 |  |              |          |                                   | 75           |              |                                    |                                    |          |          |          |            |          |          |                                   | SHEET TOTAL |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| MENT OF<br>FOR HOT F<br>Signatures<br>Computed By:                                   |                           |  | Checked By:<br>Environ                 | Engineer               |                      |                       | (1)        | H                              | INSTALLED                       | 1   | 8532                  | 01/9            | 8957   | 6583         | 6184     | 10/0                              | 3374         | 8056         | 7865                               | 7492                               | 4738     | 8356     | 8625     | 7866       | 4218     | 4563     | SHEET                             |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| ARTMI  | IENT FO                   | Ö  | σ                                      | σ                      |                      |                       |            |                                | FIELD ACCEPTANCE QUALITY SAMPLE | **LAB<br>REPORT                                     |                       |                 | 11-012   |              |          | 11-013                            |              |              |                                    |                                    | 11-013   |          |          |            | 11-013   |          |                                   |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| DEP  | NSTM                      |  |  | Ĩ                      |                      |                       |            | RI                             | INCE QUAI                       | Q-HPES  |                       |                 | m  |              |          | 4                                 |              |              |                                    |                                    | ы        |          |          |            | 6        |          |                                   |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| NG   | ADJI                      |  |  |                        |                      |                       |            |                                |                                 |   |                       |                 |  |              |          |                                   |              |              |                                    |                                    |          |          |          |            | ACCEPTA  | SUBLOT   | ,                                 | m 1         | " n    | 3 | 1 |  |  |  | 2 | 2 | 2 | 2 | 2 | m | 9 | e | <b>6</b> 0 |  |
| IMO  | РАҮ                       |  |  |                        | Other                |                       |            |                                |                                 |   | . ~1<br>1             | LoT             |  | ei a         |          | 1                                 | 1            | ~ ~          | <u>л</u> сл                        | ~                                  | 2        | ~        | N        | ~          | ~        | ~        | 61                                | 61          | 2      |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| λ  |                           | ****                                     |  |                        |                      | ≥                     |            | ELASTIC SEALANT - DAILY REPORT | SUPPLIER                        | PRODUCTION<br>RUN OR<br>BATCH                       | DAICH                 | 6037            | 6037<br>6037   | 6037         | 6191     | 6191                              | 191          | 6249         | 6249                               | 6249                               | 6249     | 6372     | 6372     | 6372       | 6372     | 6372     | 6372                              |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
|  |                           | Project Number: #######<br>Project Name: | Resident Engineer:<br>Engineer's Town: | /Supplier:             | STM - Wyoming Modifi | 🗆 D6690 Type IV       |            | E                              | presented                       | ENDING  |                       | 69              | 12.9   | 15.0         | 0/1      | 19.7                              | 242          | 25.0         | 28.3                               | 30.0                               | 32.5     | 34.0     | 36.0     | 37.1       | 39.0     | 41.2     | 42.9                              |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
|  |                           | Projec<br>Proje                          | Resident<br>Fnoinee                    | Manufacturer/Supplier: | ¥                    | □ D66:                |            |                                | Section Represented             | Beginning<br>Milepost                               |                       | 6.4             | 10.0   | 129          | 15.0     | 17.0                              | 210          | 24.2         | 25.0                               | 28.3                               | 30.0     | 32.5     | 34.0     | 36.0       | 37.1     | 39.0     | 41.2                              |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |
| 1  | Contraction of the second |  |  | Ma                     | TYPE:                |                       |            |                                |                                 | DATE  |                       | 12/16/16        | 12/11/716<br>12/18/16                                      | 12/19/16     | 01/16/16 | 01/07/16                          | 01/09/16     | 91/10/10     | 01/13/16                           | 01/14/16                           | 01/15/16 | 01/16/16 | 01/17/16 | 01/18/16   | 01/19/16 | 01/20/16 | 01/21/16                          |             |        |   |   |  |  |  |   |   |   |   |   |   |   |   |            |  |

"If no test report has been received in the field from the Laboratory within approximately 80 days after sending in all samples for a complete lot, send legible copies of all T-122 Forms, "Sample Transmittal, Hot Poured Elastic Seatant / Crack Surfacing", to Laboratory with a memorandum requesting status of report.

WYDOT 870.0 (Rev. 10-17)



# Form E-225 (Rev. 10-17) Sheet WYOMING DEPARTMENT OF TRANSPORTATION PAY ADJUSTMENT FOR HOT POURED CRACK SURFACING

| Signatures             | Computed By:  | Checked By:        | Engineer:        |  |
|------------------------|---------------|--------------------|------------------|--|
| Project Number: ###### | Project Name: | Resident Engineer: | Engineer's Town: |  |

Date: XX/XX/XX Date: XX/XX/XX

Frocuct Name:

Manuracturer/Supplier.

pof

8

Theoretical Density (TD) =

Date: XX/XX/XX

đ

| n J                   |                                |                                 | KEMARKS<br>(Weather, Melter | Temperature, etc.)                  |            |  |    |                 |   |  |       |        |   |    |  |                  |
|-----------------------|--------------------------------|---------------------------------|-----------------------------|-------------------------------------|------------|--|----|-----------------|---|--|-------|--------|---|----|--|------------------|
| Check If Final Report |                                | 1                               | -10.00                      | [(5) - (3)] x (6)                   | \$1,288.89 |  |    |                 |   |  |       |        |   |    |  | \$1,288.89       |
| Chec                  | (9)                            |                                 | CONTRACT                    | (\$)                                | \$ 100.30  |  |    |                 |   |  |       |        |   |    |  | SHEET TOTAL      |
|                       | (2)                            |                                 |                             | vaLume<br>[(1) - [2)] / (4)         | 234        |  |    |                 |   |  |       |        |   |    |  | SHE              |
|                       | (4)                            |                                 | ACTUAL                      | DENSITY                             | 85.C       |  |    |                 | - |  |       |        | 1 |    |  | <del>ل</del> ة م |
|                       | (3)                            |                                 | THEORETICAL                 | VOLUME [(1) - (2)] / TD             | 221        |  |    |                 |   |  |       |        |   |    |  | 221              |
|                       | (3)                            |                                 | ass                         | dio<br>a                            | 100        |  | Π  |                 |   |  |       |        |   |    |  | TAL              |
|                       | (1)                            |                                 | Weight or Mass              | INSTALLED VOID<br>Ib Ib             | 20002      |  |    | 10 ož           |   |  |       |        |   |    |  | SHEET TOTAL      |
|                       |                                | FIELD ACCEPTANCE QUALITY SAMPLE | 1778 T-111                  | " LAB<br>REPORT                     | 2015-13    |  | 0. |                 | 4 |  | <br>6 |        | £ | 10 |  |                  |
|                       |                                | NCE QUAI                        |                             | Q-HPCS                              | 1          |  |    | н. — ж<br>Та ал |   |  |       | A      |   |    |  |                  |
|                       | EPORT                          | ACCEPTA                         |                             | LOT SUBLOT Q.HPCS                   | 1          |  |    |                 |   |  |       |        |   |    |  |                  |
|                       | DAILY R                        |                                 |                             |                                     | 1          |  |    |                 |   |  |       |        |   |    |  |                  |
|                       | CRACK SURFACING - DAILY REPORT |                                 | PRODUCTION                  | RUN OR<br>BATCH                     | 1          |  |    |                 | 0 |  |       |        |   |    |  |                  |
|                       | CRAC                           | ROUTE LOCATION                  |                             | system milepost<br>Number Beg - End | 5-4        |  |    |                 |   |  |       | 5<br>0 |   |    |  |                  |
|                       |                                | ROUTEI                          |                             | SYSTEM<br>NUMBER                    | AL 12      |  |    |                 |   |  |       |        |   |    |  |                  |
|                       |                                |                                 |                             | UAIE                                | 5/15/2015  |  |    |                 |   |  |       |        |   |    |  | 28               |

"If no test report has been received in the field from the Laboratory within approximately 50 days after sending in all samples for a complete lot, send legible copies of all T-122 Forms, "Sample Transmittal, Hot Poured Elastic SealantiCrack Surfacing", to the Laboratory with a memorandum requesting the status of the test.

#### DEFORMED AND PLAIN BILLET-STEEL BARS FOR CONCRETE REINFORCEMENT

Scope: This section covers deformed and plain billet-steel concrete reinforcement bars in cut lengths or coils, or deformed and plain carbon-steel bars; ASTM A615 *Standard Specification for Deformed and Plain Carbon-Steel Bars for Concrete Reinforcement* and AASHTO M 31 *Deformed and Plain Carbon-Steel Bars for Concrete Reinforcement*. The standard sizes and dimensions of deformed bars and their number designations are listed in a table in this section.

A deformed bar is a steel bar with protrusions; a bar that is intended for use as reinforcement in reinforced concrete construction. The nominal dimensions of a deformed bar are equivalent to those of a plain round bar having the same weight per foot as the deformed bar.

Use: This section describes the designation numbers, grades, and nominal dimensions of deformed and plain carbon-steel concrete reinforcement bars, and lists the minimum yield and tensile strength.

*WYDOT Standard Specifications* section 811.1.2 Reinforcing Steel Bars requires reinforcing steel bars in accordance with ASTM A615 and for epoxy-coated steel bars in accordance with ASTM A775.

#### Reference

| Documents: | AASHTO M 31   | Standard Specification for Deformed and      | Plain |
|------------|---------------|--|-------|
|            |               | Carbon-Steel Bars for Concrete Reinforcement |       |
|            | ASTM A615     | Standard Specification for Deformed and      | Plain |
|            |               | Carbon-Steel Bars for Concrete Reinforcement |       |
|            | WYDOT 811.1.2 | WYDOT Standard Specifications                |       |
|            | WYDOT 130.0   | Miscellaneous Items - Sample Size            |       |
|            | WYDOT T-128   | Construction Test Requirements               |       |

Minimum Yield Strength:

| 40,000 lb/in <sup>2</sup>  |               | Grade 40 |
|----------------------------|---------------|----------|
| 60,000 lb/in <sup>2</sup>  |               | Grade 60 |
| 75,000 lb/in <sup>2</sup>  |               | Grade 75 |
| *80,000 lb/in <sup>2</sup> | designated as | Grade 80 |

Minimum Tensile Strength:

| 60,000 lb/in <sup>2</sup>   |               | Grade 40 |
|-----------------------------|---------------|----------|
| 90,000 lb/in <sup>2</sup>   |               | Grade 60 |
| 100,000 lb/in <sup>2</sup>  |               | Grade 75 |
| *105,000 lb/in <sup>2</sup> | designated as | Grade 80 |

Bars are classified in three grades in AASHTO M 31. \*Bars are classified in four grades in ASTM A615, adding Grade 80. Bar numbers are based on the number of eighths of an inch included in the nominal diameter of the bar.

Following is a table with currently used bars, USA designation.

Note: For ductility properties (elongation and bending), test provisions of the nearest smaller nominal diameter deformed bar size apply.

| Deforme   | <b>USA Bars</b><br>Deformed Bar Designation Numbers, Nominal Masses, Nominal Dimensions, Deformation Requirements |                  |                                   |                   |                                   |                              |  |  |  |  |  |  |  |
|---|---|------------------|-----------------------------------|-------------------|-----------------------------------|------------------------------|--|--|--|--|--|--|--|
| Bar No.   | Mass,<br>Nominal  |                  | Dimensions,<br>Nominal            |                   | Deformation<br>Requirements, inch |                              |  |  |  |  |  |  |  |
| Diameter,<br><sup>1</sup> / <sub>8</sub> inch ± | Weight<br>lb/ft   | Diameter<br>Inch | X-Sect<br>Area<br>in <sup>2</sup> | Perimeter<br>Inch | Maximum<br>Average<br>Spacing     | Minimum<br>Average<br>Height | Maximum<br>Gap<br>(Chord of<br>12.5% of<br>Nominal<br>Perimeter) |  |  |  |  |  |  |
| 3   | 0.376   | 0.375            | 0.11                              | 1.178             | 0.262                             | 0.015                        | 0.143  |  |  |  |  |  |  |
| 4   | 0.668   | 0.500            | 0.20                              | 1.571             | 0.350                             | 0.020                        | 0.191  |  |  |  |  |  |  |
| 5   | 1.043   | 0.625            | 0.31                              | 1.963             | 0.437                             | 0.028                        | 0.239  |  |  |  |  |  |  |
| 6   | 1.502   | 0.750            | 0.44                              | 2.356             | 0.525                             | 0.038                        | 0.286  |  |  |  |  |  |  |
| 7   | 2.044   | 0.875            | 0.60                              | 2.749             | 0.612                             | 0.044                        | 0.334  |  |  |  |  |  |  |
| 8   | 2.670   | 1.000            | 0.79                              | 3.142             | 0.700                             | 0.050                        | 0.383  |  |  |  |  |  |  |
| 9   | 3.400   | 1.128            | 1.00                              | 3.544             | 0.790                             | 0.056                        | 0.431  |  |  |  |  |  |  |
| 10  | 4.303   | 1.270            | 1.27                              | 3.990             | 0.889                             | 0.064                        | 0.487  |  |  |  |  |  |  |
| 11  | 5.313   | 1.410            | 1.56                              | 4.430             | 0.987                             | 0.071                        | 0.540  |  |  |  |  |  |  |
| 14  | 7.650   | 1.693            | 2.25                              | 5.320             | 1.185                             | 0.085                        | 0.648  |  |  |  |  |  |  |
| 18  | 13.60   | 2.257            | 4.00                              | 7.090             | 1.580                             | 0.102                        | 0.864  |  |  |  |  |  |  |

Sample size requirements for miscellaneous items are shown in WYDOT 130.0. Submit samples as per the plans or as required on WYDOT Form T-128.

#### ALKALI SAMPLING AND PRELIMINARY PIPE SELECTION

| Scope:                  | Alkali samples are soil samples taken from drainage channels that are traversed<br>by an existing or proposed roadway.            |  |  |  |  |  |
|-------------------------|---|--|--|--|--|--|
| Apparatus:              | <ol> <li>Clean canvas sample sacks</li> <li>Shovel</li> <li>Form T-120 <i>Sample Transmittal</i> with envelope</li> </ol>         |  |  |  |  |  |
| Use:                    | Alkali samples are tested to determine the potential of the soil to cause damage to metallic and/or concrete drainage structures. |  |  |  |  |  |
| Reference<br>Documents: | WYDOT T-120 Sample Transmittal  |  |  |  |  |  |
| Sampling                |   |  |  |  |  |  |

Determination: A minimum of 25 lb of soil is required for each sample.

The sampling may be performed as a separate task or, the sampling may be done at the same time the "Field Photo Annotation" task is performed (this task includes the verification of drainage structure type, size and condition).

For reconstruction projects: Obtain a sample at every drainage channel that will be traversed by the proposed alignment.

For widen and overlay projects: Obtain samples only at those locations where the drainage structure is in fair/poor condition. If the drainage structure is in good condition extend it with the same level of corrosion resistance materials as the existing.

Procedure: Alkali samples are taken by the engineer at all existing or proposed drainage facilities that are less than 48 inches in diameter or width. The Geology Program will take the alkali samples at existing or proposed drainage facilities that are 48 inches or greater unless other arrangements are made by the Programs involved.

Obtain sample at one drainage location only, unless required by the plans or the engineer. Obtain the sample at either the upstream or the downstream end of the existing or proposed drainage structure, whichever is more accessible. Take the sample from the site such that it will represent the soil that will be in contact with the drainage structure; typically taken from the upper 0.5 feet of the soil at the low point within the drainage channel.

Submitted alkali samples to the Materials Program with a Form T-120 that includes the milepost, the station, and the location of the sample as well as the condition of the existing drainage structure (if applicable).

| 8                    | WYOMIN                                   | Materials     | INT OF TRANS        | у                   | Form T-120<br>(Rev. 09-16) |  |
|----------------------|--|---------------|---------------------|---------------------|----------------------------|--|
|                      | Preliminary                              | Geol 🔽 Geol   | ogy 🔽 Co            | nstruction          |                            |  |
|                      |  |               |                     |                     |                            |  |
| Project Number       | 12                                       |               |                     | #:                  |                            |  |
|                      | : Resident Eng                           | ineer         |                     | At: Engineer's Tow  | 'n                         |  |
| Soils                | N.                                       | 20-40-5       |                     | on: As Per Plans    |                            |  |
|                      | Name of Pit                              |               |                     | ty: County of Pit o |                            |  |
| Date Sampled         | Date Sampled: Date Received: / ## / ## / |               |                     |                     |                            |  |
| ,<br>✓ Aggregat      | e  |               | e Distribution      |                     | Geology                    |  |
|                      |  | Concrete      | Chemistry           |                     | Geology                    |  |
|                      |  |               |                     |                     | Multiple Samples           |  |
| Sample Number(s)     |  |               | \$ #: <u>14</u>     | TH #:_7             | l of                       |  |
| Location (Belt, Stoc |  |               | At: (Sta., kp., M.F |                     |                            |  |
| Vertical Limits      | 40. VASC                                 |               | To: <u>10</u>       | )' 6"               |                            |  |
| Horizontal Limits    |  |               | To:                 |                     |                            |  |
| Qty. Represented     |  |               |                     |                     |                            |  |
|                      |  | Fo            | r Use As :          |                     |                            |  |
| Profile              |  | BSE           | ] PMP, Grd.         | Conc. Coars         | e Aggregate                |  |
| Borrow               | $\checkmark$                             | CB, Grd.      |                     | Conc. Med. /        | \ggregate                  |  |
| Topping              |  | РМВ           | ] PMWC, Type        | Conc. Fine A        | ggregate                   |  |
| Alkali               |  | СТВ           | ] ССА, Туре         | Conc. Cylind        | ers                        |  |
| Check Curve          | e 🗌                                      | Filler        | ] Maint. Type       | Conc. Beam          | 5                          |  |
| Final Emb.           |  | Drain Gra∨el  | Check Design        | Port. Cemen         | t, Type                    |  |
| Other                |  |               |                     | Туре                |                            |  |
|                      |  | Geosynthetics | (Geogrid/Geotext    | ile)                |                            |  |
| Product Name         |  |               | Manufacturer        |                     |                            |  |
| Remarks: Sand & G    | ravel                                    |               |                     |                     |                            |  |
|                      |  |               |                     |                     |                            |  |
|                      |  |               |                     |                     |                            |  |
|                      |  |               |                     |                     |                            |  |
|                      |  |               |                     |                     |                            |  |
|                      |  |               |                     |                     |                            |  |

**Printed** Name

Signature

#### **DETERMING DELAMINATION IN BRIDGE DECKS BY CHAIN DRAG METHOD**

- Scope: This procedure is technically equivalent, but not identical, to ASTM D 4580. This test method describes the procedure for surveying concrete bridge decks and other concrete pavements by chain drag method to locate delaminations in the concrete.
- Use: This procedure is not intended for use on bridge decks that have been overlaid with bituminous mixtures or on frozen concrete. This procedure may be used on bridge decks that have been overlaid with concrete pavement, however, areas indicated to be delaminated may have a lack of bond between the overlay and the underlying bridge deck.
- Apparatus: The chain drag apparatus consists of four segments of 1 inch link chain 1. of 1/4 inch diameter steel approximately 18 inch long. These are attached to two 10 inch pieces of 3/4 inch type L copper tubing (two segments of chain attached to each piece) which are joined together by a <sup>3</sup>/<sub>4</sub> inch copper tee. A 3 ft piece of the same copper tubing is attached to the copper tee to form a handle with the completed apparatus forming a T. See Figure 1.
  - Measuring tape and marking paint to establish a grid system on the bridge 2. deck and to outline the delaminated areas.
  - 3. A bridge deck layout/map. Field notes can be prepared in advance with the dimensions of the deck, skew angles, and a 5 ft grid matching the grid on the deck.

Reference

Documents:

ASTM D 4580 Standard Practice for Measuring Delaminations in Concrete Bridge Decks by Sounding

Procedure: 1. Bridge Deck Layout

> Construct a grid system on the deck surface by establishing the center of the bridge deck and placing a mark at 5 ft intervals from centerline to curb on each side of the deck at each abutment. Any distance less than 5 ft should be next to each curb. This forms the transverse part of the grid. Mark a scale down the centerline of the deck in 5 ft intervals to establish the longitudinal part of the grid.

2. **Test Procedure** 

> Drag the chains over the deck surface either longitudinally or transversely. Delaminated areas are those where a dull or hollow sound from the chain dragging operation is heard. When a delamination is

heard, mark the limit of the delamination with marking paint or a lumber crayon. Continue chain dragging and marking the delamination until the limits are found in all directions.

3. Plotting

Transfer the outlines of the delaminations marked on the deck to the map by drawing the outlines from the deck to the corresponding location on the map. A tape measure can be used to measure the lines that are between the 5 ft grid marks. Determine the total area contained in the individual delaminated areas. Divide the total delaminated area by the total bridge deck area and multiply by 100 to yield the percent of delaminated area.

 $\frac{\text{Delaminated Area}}{\text{Total Bridge Deck Area}} \ge 100 = \% \text{ Delaminated}$ 

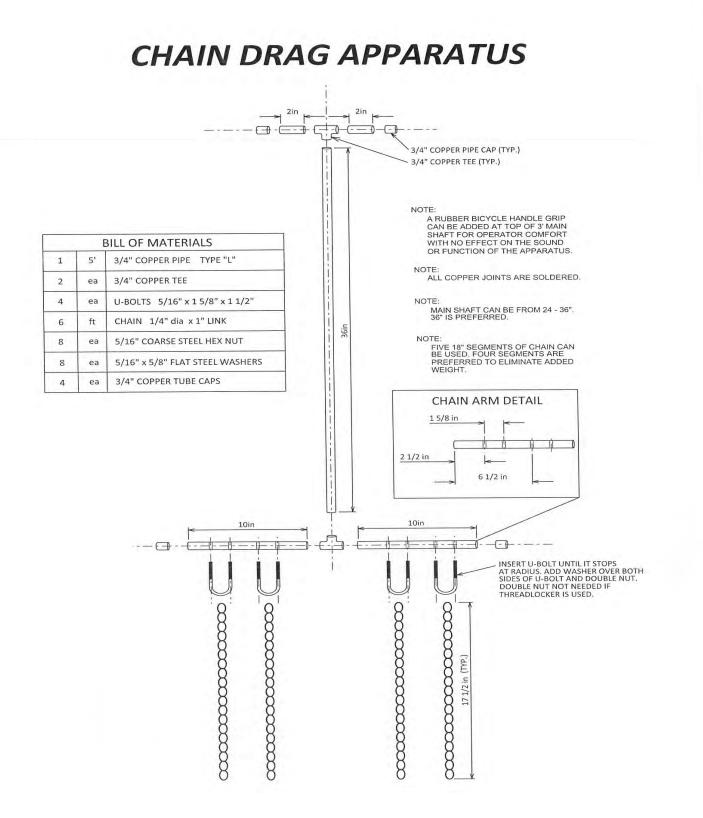
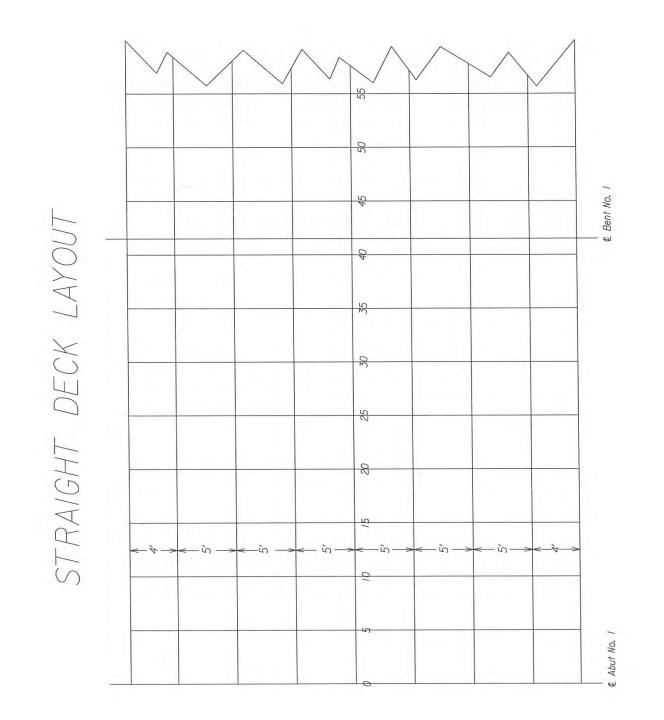
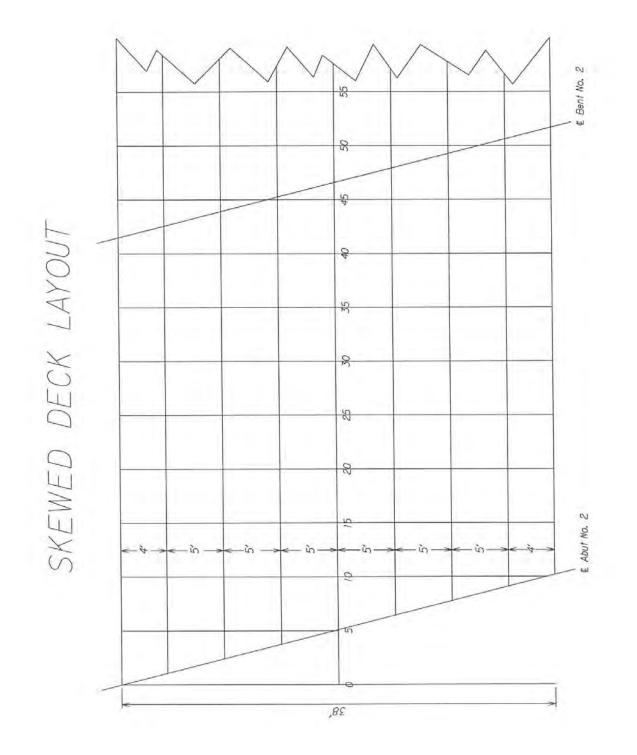


Figure 1.





5

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# MTM Forms (Rev. 10-18) WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING MANUAL

FORMS

| Last<br>Revised | Form #  | MTM Section #                                  | Form TITLE  |
|-----------------|---------|--|---|
| 09-16           | E-45    | 471.0  | Concrete Mix Design   |
| 09-16           | E-46    | 414.0  | Hot Plant Mix Job Mix Formula   |
| 09-16           | E-46A   | 414.0  | Hot Plant Mix Job Mix Formula (Non-QCQA)                                |
| 09-16           | E-46M   | 430.0  | Microsurfacing Mix Design (Include JMF)                                 |
| CMS             | E-56    | 421.0  | Asphalt and Lime Report (Created in CMS Module)                         |
| CMS             | E-119   | 126.0  | Pay Adjustment for Density (Created in CMS Module)                      |
| CMS             | E-120   | 814.0  | Pay Adjustment for Aggregate Gradation (Created in CMS Module)          |
| 10-17           | E-120E  | 421.0  | Pay Adjustment for Asphalt Content                                      |
| 10-17           | E-221   | 840.0  | Pay Adjustment for Performance Graded Asphalt Binder                    |
| 10-17           | E-222   | 870.0  | Pay Adjustment for Hot Poured Elastic Sealant                           |
| 10-17           | E-224   | 840.0  | Pay Adjustment for Emulsified Asphalt                                   |
| 10-17           | E-225   | 870.0  | Pay Adjustment for Hot Poured Crack Surfacing                           |
| CMS             | E-229   | N/A  | Pay Adjustment for QC/QA Structural Concrete Level of Control 1         |
| CMS             | E-230   | N/A  | Pay Adjustment for QC/QA Structural Concrete Level of Control 2 & 3     |
| CMS             | E-231   | N/A  | Pay Adjustment for Portland Cement Concrete Pavement                    |
| 09-16           | T-100   | 471.0  | Report of Tests on Concrete Mix Designs (Provided by Materials Program) |
| 09-16           | T-100PE | 472.0  | Portland Cement Concrete Pavement Mix Design                            |
| 09-16           | T-100SE | 472.0  | Structural Concrete Pavement Mix Design                                 |
| 09-16           | T-101   | 816.0  | Report of Field Tests on Concrete Aggregate                             |
| 09-16           | T-102   | 814.0, 816.0                                   | Report of Field Tests on Surfacing Materials                            |
| 09-16           | T-107W  | 837.0  | Report of Test on Aggregate   |
| 10-18           | T-108   | 415.0  | Asphalt Base / Pavement Density Report                                  |
| 10-18           | T-109   | 483.0  | Concrete Placing Report   |
| 09-16           | T-112   | 210.0, 212.0,<br>213.0, 214.0,<br>216.0, 301.0 | Soil Compaction Worksheet   |
| 09-16           | T-113   | 213.0, 215.0,<br>221.0                         | Weekly Report for Compaction of Embankment/Crushed Base/Other           |
| 09-16           | T-120   | 123.0, 1010.0                                  | Sample Transmittal  |
| 10-17           | T-121   | 840.0  | Sample Transmittal Asphalt  |
| 09-16           | T-122   | 870.0  | Sample Transmittal Crack Sealant / Crack Surfacing                      |
| 11-12           | T-128   | 107.0  | Construction Test Requirements (Provided by Materials Program)          |
| 03-00           | T-131   | 107.0  | Manufactured Products Received (Provided by Materials Program)          |
| 11-16           | T-132   | 107.0  | Engineer's Verification of Specification Compliance                     |
| 09-16           | T-140   | 210.0, 213.0,                                  | Plotting Worksheet  |
|                 |         | 214.0, 216.0                                   |   |
| 09-16           | T-158   | 414.0  | Bituminous Pavement Mix Design  |
| 10-18           | T-158F  | 414.0  | Mix Verification of Plant Produced Bituminous Plant Mix Pavement        |
| 09-16           | T-159   | 817.0  | Flat & Elongated and Fractured Faces                                    |
| CMS             | T-165AG | 126.0  | Correlation of Aggregate Gradations (Created in CMS Module)             |
| CMS             | T-165CD | 423.0  | Correlation of Core Densities (Created in CMS Module)                   |

MTM Forms (Rev. 10-18)



#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING MANUAL FORMS

| Last<br>Revised | Form #   | MTM Section #          | Form TITLE   |
|-----------------|----------|------------------------|--|
| 10-18           | T-166    | 803.0, 814.0,<br>816.0 | Aggregate Analysis   |
| 09-16           | T-168    | 108.0                  | Certification of Materials (Re-order # FR-6140)                    |
| 09-16           | T-180    | 850.0                  | Chip Seal Aggregate / Emulsion Compatibility Test                  |
| 10-17           | T-211    | 230.0                  | Macrotexture Report  |
| 10-18           | T-302    | 211.0                  | Standardization of Sand Worksheet                                  |
| 09-16           | T-312    | 800.0                  | Density Random Number Selection Worksheet                          |
| 09-16           | T-313    | 801.0                  | Balance Verification Worksheet                                     |
| 09-16           | T-480    | 481.0                  | Equipment Calibration, Verification, Maintenance and Checking Form |
| 09-16           | T-481    | 481.0                  | Report of Calibration Verification                                 |
| 10-18           | T-515IPV | 401.0                  | High Speed Inertial Profiler Worksheet                             |
| 10-18           | T-515M   | 403.0                  | Smoothness Assessment Report                                       |
| 10-18           | T-515SR  | 402.0, 403.0           | Smoothness Testing Summary Report                                  |
|                 |          |                        |  |
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|                 |          |                        |  |

Please note all MTM Forms are now accessible on the Materials Program's (MP's) FTP site. Click on any form in the Forms Table of Contents and you will be directed to the FTP site to make a form selection.

Forms created in CMS Module are no longer available on the MP's FTP site.

#### WYOMING DEPARTMENT OF TRANSPORTATION PAY ADJUSTMENT FOR ASPHALT CONCRETE



Form E-120E (Rev. 10-18)

Sheet 1

| Date:       E-56       Content<br>Number       Material<br>(%) from<br>E-56       Material<br>Produced<br>This Date       Asphalt<br>Content Pay<br>Factor       Leveling       Mainline       Approach       Wearing Crs       0         6/2/2017       1       4.21       1572.73       REJECT       1563.45       Item Bid Price (\$)       0         6/3/2017       2       5.42       2484.86       1.00       2189.42       Item Side Price (\$)       0         6/4/2017       3       5.27       2415.27       1.00       2310.22       Item Side Price (\$)       0         6/5/2017       4       5.27       1595.28       1.00       1475.54       Item Side Price (\$)       0         6/8/2017       5       5.00       1500.00       0.95       22.26       528.06       Item Side Price (\$)   | (2) x (3)<br>REJECT<br>\$0.00  |
|---|--|
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $   | 5<br>Pay<br>Adjustment \$<br>0.67 x [ (1) - 1.0 ] x<br>(2) x (3)<br>REJECT<br>\$0.00 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$   | 5<br>Pay<br>Adjustment \$<br>0.67 x [ (1) - 1.0 ] x<br>(2) x (3)<br>REJECT<br>\$0.00 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$   | Pay<br>Adjustment \$<br>0.67 x [ (1) - 1.0 ] x<br>(2) x (3)<br>REJECT<br>\$0.00      |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $   | Pay<br>Adjustment \$<br>0.67 x [ (1) - 1.0 ] x<br>(2) x (3)<br>REJECT<br>\$0.00      |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $   | Adjustment \$ 0.67 x [ (1) - 1.0 ] x (2) x (3) REJECT \$0.00                         |
| Date:E-56<br>NumberContent<br>(%) from<br>E-56Material<br>Produced<br>This DateAsphalt<br>Content Pay<br>FactorLevelingMainlineApproachWearing Crs<br>Wearing Crs0 $6/2/2017$ 14.211572.73REJECT $1563.45$ <td< td=""><td>Adjustment \$ 0.67 x [ (1) - 1.0 ] x (2) x (3) REJECT \$0.00</td></td<>   | Adjustment \$ 0.67 x [ (1) - 1.0 ] x (2) x (3) REJECT \$0.00                         |
| Date:         Number $\binom{\%}{100}$ from<br>E-56         Produced<br>This Date         Content Pay<br>Factor         Leveling         Mainline         Approach         Wearing Crs $\binom{Wainline}{100}$ Mapproach         Wearing Crs $\binom{Wainline}{100}$ Mapproach         Wearing Crs $\binom{Wainline}{100}$ Mapproach         Wearing Crs $\binom{Wainline}{100}$ Mapproach         Wearing Crs $\binom{Wainline}{100}$ Approach         Wearing Crs $\binom{Wainline}{100}$ Mapproach         Mapproach | (2) x (3)<br>REJECT<br>\$0.00  |
| E-56This DateFactorFactorItem Bid Price (\$)(2)\$ 20.00\$ 35.00\$ 50.006/2/201714.211572.73REJECT1563.456/3/201725.422484.861.00 $2189.42$ 6/4/201735.272415.271.00 $2310.22$ </td <td>(2) x (3)<br/>REJECT<br/>\$0.00</td>   | (2) x (3)<br>REJECT<br>\$0.00  |
| 6/2/2017       1       4.21       1572.73       REJECT       1563.45       50.00       \$ 50.00         6/3/2017       2       5.42       2484.86       1.00       2189.42       4  | <b>REJECT</b><br>\$0.00  |
| 6/3/2017       2       5.42       2484.86       1.00       2189.42  | \$0.00   |
| 6/4/2017       3       5.27       2415.27       1.00       2310.22  |  |
| 6/5/2017       4       5.27       1595.28       1.00       1475.54  | +  |
| 6/8/2017       5       5.00       1500.00       0.95       22.26       528.06            6/9/2017       6       5.04       1505.56       0.95       1467.73             6/10/2017       7       5.71       2554.94       0.80       2508.89             6/11/2017       8       5.37       2600.53       1.00       2535.88             6/12/2017       9       5.41       2471.07       1.00       2406.36   | \$0.00   |
| 6/9/2017         6         5.04         1505.56         0.95         1467.73              6/10/2017         7         5.71         2554.94         0.80         2508.89  <  | \$0.00   |
| 6/10/2017       7       5.71       2554.94       0.80       2508.89            6/11/2017       8       5.37       2600.53       1.00       2535.88             6/12/2017       9       5.41       2471.07       1.00       2406.36  | (\$14.91)  |
| 6/11/2017         8         5.37         2600.53         1.00         2535.88             6/12/2017         9         5.41         2471.07         1.00         2406.36   | (\$1,720.91)   |
| 6/12/2017         9         5.41         2471.07         1.00         2406.36   | (\$11,766.69)  |
|   | \$0.00   |
| 6/15/2017         10         5.26         3008.76         1.00         2745.85  | \$0.00   |
|   | \$0.00   |
| 6/16/2017 11 5.39 2744.07 1.00 2723.23  | \$0.00   |
| 6/17/2017         12         5.65         2391.54         0.85         2106.27         111.68   | (\$7,970.00)   |
| 6/18/2017 13 4.78 650.12 <b>REJECT</b> 575.88 49.72   | \$0.00   |
| 6/19/2017 14 5.81 1623.50 <b>REJECT</b> 1528.40   | REJECT   |
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| Sheet Totals:         7560.89         19126.55         161.40   | (\$21,472.52)  |
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#### WYOMING DEPARTMENT OF TRANSPORTATION MATERIALS TESTING LABORATORY

E-229 (Rev. 03-17)

# QC/QA STRUCTURAL CONCRETE LEVEL OF CONTROL 1

| Project No.:    | N345093                                   | Date:            | 5/17/2018              |
|-----------------|---|------------------|------------------------|
| Road:           | Lovell - Cowley Road (Sage Creek Section) | Pumped:          | No                     |
| Engineer:       | Michael Miller, P.E.                      | Location:        | Sage Creek Bridge Deck |
| Concrete Class: | A   | Pumped Concrete: | No                     |
| Tested By:      | Wayne A Riley                             | WMTC Number:     | 4667                   |
| Tested By:      |   | WMTC Number:     |                        |

|                     | Sublot 1  | Sublot 2  | Sublot 3  | Sublot 4  | Sublot 5 | Sublot 6 | Sublot 7 |
|---------------------|-----------|-----------|-----------|-----------|----------|----------|----------|
| Cylinder 1          | 7450.0000 | 7080.0000 | 6940.0000 | 6570.0000 |          |          |          |
| Cylinder 2          | 7290.0000 | 6690.0000 | 7190.0000 | 6400.0000 |          |          |          |
| Cylinder 3          | 7350.0000 | 7020.0000 | 7060.0000 | 6470.0000 |          |          |          |
| Average Strength    | 7363      | 6930      | 7063      | 6480      |          |          |          |
| Strength Pay Factor | 1.00      | 1.00      | 1.00      | 1.00      |          |          |          |

| Air Content | 6.1 | 6.0 | 6.1 | 6.8 | 0.0 | 0.0 | 0.0 |
|-------------|-----|-----|-----|-----|-----|-----|-----|
| ACn         | 4.2 | 4.2 | 4.2 | 4.2 |     |     |     |

| Lot Number        | 2    |
|-------------------|------|
| Number of sublots | 4    |
| Design Strength   | 3750 |
| Average Strength  | 6959 |

| Strength Pay Factor | 1.00 |
|---------------------|------|
| Air Pay Factor      | 1.00 |
| Overall Pay Factor  | 1.00 |
| Override            |      |

|             | Destant No   |                             | Quantita | 1.1  |            |                |
|-------------|--------------|-----------------------------|----------|------|------------|----------------|
| Item Number | Project No.  | Pour Description / Location | Quantity | Unit | Unit Price | Pay Adjustment |
| 513.00005   | NHPP-N345093 | Sage Creek Bridge Deck      | 100.0000 | CY   | \$556.50   | \$0.00         |

Remarks



### MATERIALS TESTING LABORATORY QC/QA STRUCTURAL CONCRETE LEVEL OF CONTROL 2

E-230 (Rev. 03-17)

| Project No.: | N345093                          |          |                |       |          | Date:         | 9/28/2017              |            |                |  |
|--------------|----------------------------------|----------|----------------|-------|----------|---------------|------------------------|------------|----------------|--|
| Road:        | Lovell - Cowley Road (           | Sage Cre | eek Sec        | tion) |          | Pumped:       | Yes                    |            |                |  |
| Engineer:    | Michael Miller, P.E.             |          |                |       |          | Location:     | Location: bent #2 Rt   |            |                |  |
| Tested By:   | Wayne A Riley                    |          |                |       | ١        | WMTC Number:  | 4667                   |            |                |  |
| Tested By:   | Shannon Armstrong                |          |                | _     | ١        | WMTC Number:  | 9581                   |            |                |  |
|              | Test Set Number                  |          |                |       | Design S | trength       | 3750                   |            |                |  |
|              |                                  |          |                |       |          | Average of    | -                      | 6323       |                |  |
|              | Cylinder 2 632<br>Cylinder 3 623 |          | 0.0000         |       | F        | Strength Pa   | av Factor              | 1.00       |                |  |
|              |                                  |          | 0000           |       |          |               | ,                      |            |                |  |
|              |                                  |          | 0.0000<br>8000 |       |          | ACn           |                        | 4.70       |                |  |
|              |                                  |          |                |       |          | Air Content F | Air Content Pay Factor |            |                |  |
|              |                                  |          |                |       |          |               |                        |            |                |  |
|              | Overall Pay Facto                |          | actor          | 1.00  |          | Override      |                        |            |                |  |
|              |                                  |          |                | •     |          |               |                        |            |                |  |
| Pour [       | Description / Location           |          | lte            | m #   |          | Project       | Quantity               | Unit Price | Pay Adjustment |  |
| Bent #2      | Rt Sage Creek Bridg              | ge       | 506.0          | 01048 | NH       | IPP-N345093   | 21.0000                | \$580.00   | \$0.00         |  |

Comments:



Lot #:

1

## MATERIALS TESTING LABORATORY Portland Cement Concrete Pavement Air, Strength and Thickness Pay Factors

E-231 (Rev. 03-17)

| Project No.: | 0901091  | Date:        | 6/12/2017      |  |
|--------------|--|--------------|----------------|--|
| Road:        | Sheridan Marginal (North Sheridan Interchange) |              |                |  |
| Engineer:    | Jerry Buckley, P.E.                            | Location:    | N. Main Street |  |
| Tested By:   | Frankie R Horsley Jr                           | WMTC Number: | 7626           |  |
| Tested By:   |  | WMTC Number: |                |  |
|              |  |              |                |  |
|              |  |              |                |  |

#### Design Flexural Strength 650 psi Design Thickness 9.00 in

| Sublot<br>Number | 28 Day Compressive Strengths (psi) |      |         | Correlation<br>Constant | Flexural<br>Strength | Air   | Thickness |      |
|------------------|------------------------------------|------|---------|-------------------------|----------------------|-------|-----------|------|
|                  | 1                                  | 2    | 3       | Average                 | Cc                   | (psi) |           |      |
| 1                | 6530                               | 6700 | 6600    | 6610                    | 9.00                 | 732   | 6.5       | 9.00 |
| 2                | 5720                               | 5950 | 5770    | 5813                    | 8.98                 | 685   | 6.3       | 9.00 |
| 3                | 6020                               | 6030 | 6360    | 6137                    | 8.98                 | 703   | 5.0       | 9.75 |
|                  |                                    |      | Average | 6187                    |                      | 707   | 5.9       | 9.3  |

| Air<br>(PFa) | Strength<br>(PFs) | Thickness<br>(PFt) | Overall PF | Override |
|--------------|-------------------|--------------------|------------|----------|
| 1.00         | 1.00              | 1.02               | 1.02       |          |
|              | PFs+PFt-1         |                    |            |          |
|              | 1.02              |                    |            |          |

| Item Number | Project           | Quantity      | Unit Price | Pay Adjustment |
|-------------|-------------------|---------------|------------|----------------|
| 414.01040   | SIB-NHPPI-0901091 | 5312.00<br>00 | \$55.04    | \$5,847.45     |

#### Remarks

Sta.2087+50 to 2079+00 LT 16.5 ft wide Center Lane Sta.2087+50 to 2079+00 RT 16.5 ft wide Center Lane Sta.2078+15 to 2069+00 LT 24.5 with C&G